

**MODEL 8201
MODULATION ANALYZER
INSTRUCTION MANUAL**

BOONTON

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DATE 4/92**

IMPORTANT NOTICE

DECEMBER 28, 1994

INSTRUCTION MANUAL-ADDENDUM: MODEL 8201

Instruction manual addenda are issued to adapt the manual to changes and improvements made after its printing. Please review the following pages and insert into your manual and discard the old pages.

Thank you for selecting Boonton Electronics for your Test and Measurement needs.

SECTION 7, TABLE 7-2, page 7-28

Change U4 Part number to 534366000

SECTION 8, FIGURE 8-23, page 8-27

Change U4 to SN74F00

IMPORTANT NOTICE

MARCH 6, 1995

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Page 4-3 Figure 4-2: RF Circuits Block Diagram.

Replace CR11 with a wire.

Page 6-12

On line number 23 change "2 volts" to "4.5 volts" and omit text ", or open CR11".

Page 7-5 Table 7-2: Model 8201 Parts List.

Change Reference Designator "CR6-16" to "CR6-9,12-16" and change the quantity on that line to "9".

Add the following information for CR10:

DIODE HSCH1001 (1N6263)	28480	HSCH-10001	1	530174000
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Page 7-7 Table 7-2: Model 8201 Parts List.

Change the information for R72 as follows:

RES MF 110K 1% 1/4W	19701	5043ED110K0F	1	341504000
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Page 8-10 Figure 8-6: RF Board A2A1, Parts Location.

Replace CR11 with a wire.

Page 8-11 Figure 8-8: RF Board A2A1, Schematic Diagram.

Replace CR11 with a wire. Omit reference designator "CR11" and the value "1N914".

Change the value of CR10 to "1N6263".

Change the value of R72 to "110K".

IMPORTANT NOTICE

DECEMBER 1, 1995

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Page 1-6 Table 1-1 General Information

Add the following:

Ventilation Requirements:

1 1/2 inch clearance after installation, top, side, and rear

Temperature:

Non-Operating: -40 to 75 degrees C

Altitude:

Operating: 10,000 FT

Non-Operating: 15,000 FT

Humidity:

95% (non-condensing)

Battery Type:

Refer to page 7-25

Installation Category:

Designed for IEC Installation (overvoltage) Category 2

CE MARK: Declares Conformity to European Community (EC) Council Directives :
89/336/EEC//93/68/EEC, 73/23/EEC//93/68/EEC & Standards : EN55011,
EN50082-1, EN61010-1

Page 2-1 Line Voltage Select Chart

Change 3/4ATD & 3/8 ATD to 3/4A T & 3/8A T

IMPORTANT NOTICE

February 27, 2008

OPERATION AND MAINTENANCE MANUAL-ADDENDUM: MODEL 8201

Operation and Instruction manual addenda are issued to adapt the manual to changes and improvements made after this printing. Please review the following text and retain with your manual for future reference. These changes will be applied in the next printing of the manual.

Thank you for selecting BOONTON ELECTRONICS for your Test and Measurement needs.

Page 7-2 “**A1 PWA ‘8201’ MOTHER ”**

REFERENCE: 224270000

REMOVE C11.

Page 7-2 “**A1 PWA ‘8201’ MOTHER ”**

REFERENCE: 205045000

ADD REFERENCE DESIGNATOR C26 WITH C15.

CHANGE QUANTITY FROM 1 TO 2.

Page 7-3 “**A1 PWA ‘8201’ MOTHER ”**

REFERENCE: 341246000

ADD REFERENCE DESIGNATOR R21 WITH R5.

CHANGE QUANTITY FROM 1 TO 2.

Page 8-4 “**Figure 8-2. Mother Board A1, Parts Location.**”

REPLACE WITH DRAWING 082519B

Page 8-5 “**Figure 8-3. MotherBoard A1, Schematic Diagram Sheet 1.**”

REPLACE WITH DRAWING 83136230A REV. C

DRAWING 83136230A REV. C INCLUDES THE FOLLOWING CHANGES;

- 1) REMOVE C11
- 2) ADD 301 OHM RESISTOR FROM AR2 PIN1 TO CATHODE OF CR7
- 3) ADD 270 pF CAPACITOR FROM AR2 PIN 1 TO AR2 PIN 2

SAFETY SUMMARY

The following general safety precautions must be observed during all phases of operation and maintenance of this instrument. Failure to comply with these precautions or with specific warnings elsewhere in this manual violates safety standards of design, manufacture, and intended use of the instrument. Boonton Electronics assumes no liability for the customer's failure to comply with these requirements.

THE INSTRUMENT MUST BE GROUNDED

To minimize shock hazard the instrument chassis and cabinet must be connected to an electrical ground. The instrument is equipped with a three conductor, three prong power cable. The power cable must either be plugged into an approved three-contact electrical outlet or used with a three-contact to a two-contact adapter with the (green) grounding wire firmly connected to an electrical ground at the power outlet.

DO NOT OPERATE THE INSTRUMENT IN AN EXPLOSIVE ATMOSPHERE

Do not operate the instrument in the presence of flammable gases or fumes.

KEEP AWAY FROM LIVE CIRCUITS

Operating personnel must not remove instrument covers. Component replacement and internal adjustments must be made by qualified maintenance personnel. Do not replace components with the power cable connected. Under certain conditions dangerous voltages may exist even though the power cable was removed; therefore, always disconnect power and discharge circuits before touching them.

DO NOT SERVICE OR ADJUST ALONE

Do not attempt internal service or adjustment unless another person, capable of rendering first aid and resuscitation, is present.

DO NOT SUBSTITUTE PARTS OR MODIFY INSTRUMENT

Do not install substitute parts or perform any unauthorized modification of the instrument. Return the instrument to Boonton Electronics for repair to ensure that the safety features are maintained.

SAFETY SYMBOLS

This safety requirement symbol (located on the rear panel) has been adopted by the International Electrotechnical Commission, Document 66 (Central Office) 3, paragraph 5.3, which directs that the instrument be so labeled if, for the correct use of the instrument, it is necessary to refer to the instruction manual. In this case it is recommended that reference be made to the instruction manual when connecting the instrument to the proper power source. Verify that the correct fuse is installed for the power available, and that the switch on the rear panel is set to the applicable operating voltage.



The CAUTION sign denotes a hazard. It calls attention to an operation procedure, practice, or the like, which, if not correctly performed or adhered to, could result in damage to or destruction of part or all of the equipment. Do not proceed beyond the CAUTION sign until the indicated conditions are fully understood and met.

The WARNING sign denotes a hazard. It calls attention to an operation procedure, practice, or the like, which, if not correctly performed or adhered to, could result in injury or loss of life. Do not proceed beyond a WARNING sign until the indicated conditions are fully understood and met.

Indicates dangerous voltages.

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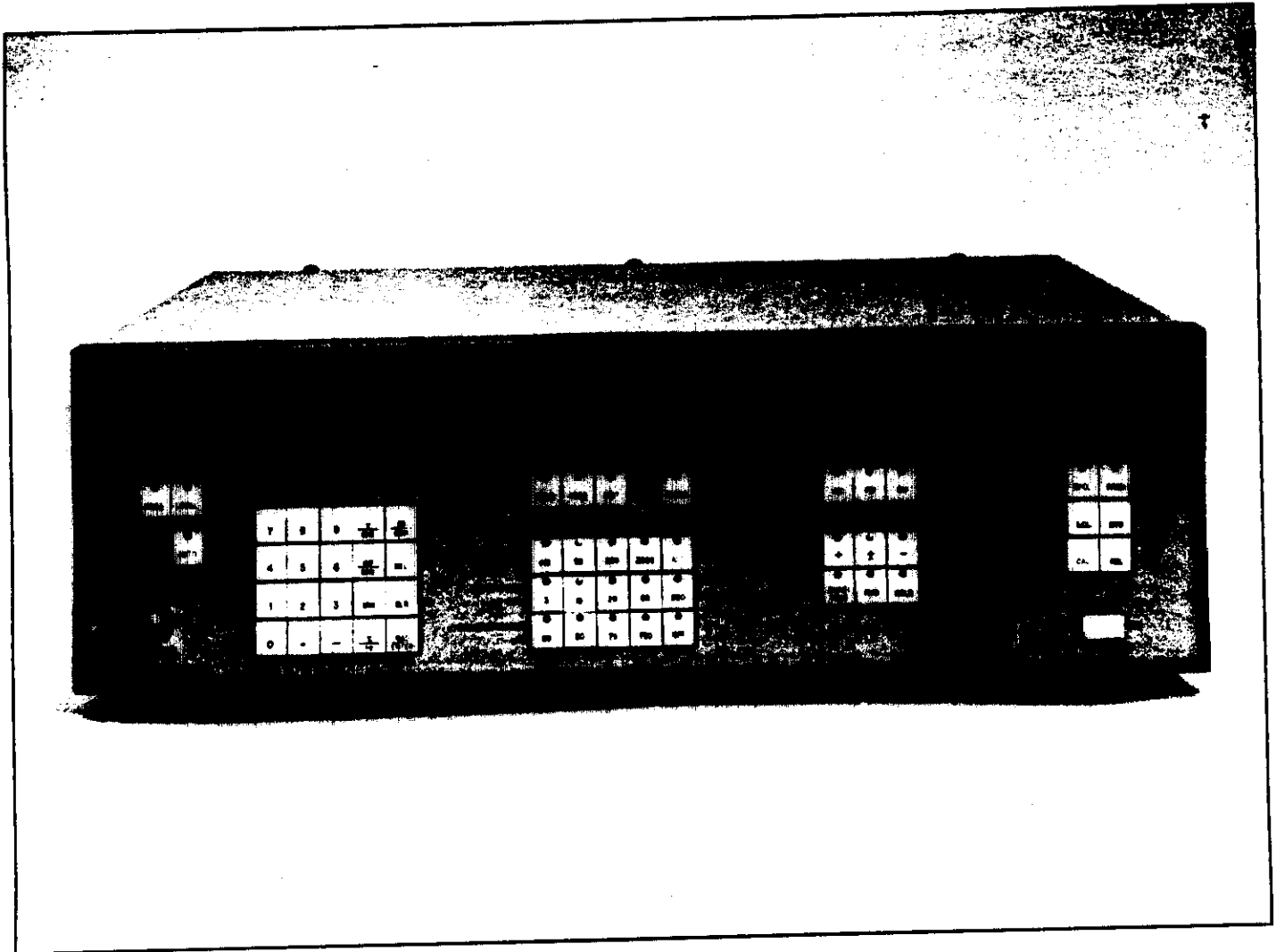
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8201 Modulation Analyzer

SECTION I

GENERAL INFORMATION

1-1. INTRODUCTION.

1-2. This manual provides general information, installation information, operating instructions, theory of operation, performance tests, maintenance instructions, a parts list and schematic diagrams for the Model 8201 Modulation Analyzer. The Model 8201 is manufactured by Boonton Electronics Corporation, Randolph, New Jersey.

1-3. DESCRIPTION.

1-4. The Model 8201 is a versatile, precision, solid-state instrument with features and performance characteristics especially suitable for laboratory and industrial applications. It covers a frequency range of 100 kHz to 2.5 GHz. Human engineering considerations have been emphasized in both the mechanical and electrical design of the Model 8201. The result is a modulation analyzer that is easy and convenient to use, despite its flexibility. Among the outstanding features are:

Automatic tuning and leveling. The Model 8201 can automatically acquire the largest signal present at the input connector and adjust its local oscillator and measurement channel gain to provide a calibrated display of amplitude modulation (AM), frequency modulation (FM), or phase modulation (PM). Additionally, the operator can select the display of carrier level in millivolts or dBm. This may be accomplished using the front panel keys or remotely via the IEEE-488 bus.

Separate displays of all major functions. The Model 8201 has four separate displays to present simultaneously carrier frequency or level, audio frequency, distortion percent, or distortion SINAD, modulation AM, FM, or PM, and program number or SPCL function. Continuous display of IEEE-488 bus status is also presented.

Internal Distortion Analyzer. The Model 8201 includes a fully automatic audio distortion analyzer. The results can be displayed in percent or dB SINAD.

Low Residual Modulation. The exceptionally low modulation residuals provide excellent measurement accuracy with low noise sources. Direct residual measurements are possible using the Model 8201 with internal true rms detectors. In addition, active peak detectors insure exceptional baseband detection linearity so that residuals may be easily discounted for enhanced measurement accuracy.

1-5. The features described in the preceding paragraphs, together with those described in Table 1-1, make the Model 8201 particularly useful for design, production line, and field testing of AM, FM, and PM transmitters and signal generators. Because of its flexibility, the Model 8201 is also a good modulation analyzer for laboratory applications.

1-6. OPTIONS.

-01 **Avionics Calibration.** Additional tests are made to insure the augmented avionics AM specifications. (Table 1-1)

-02 **Rear panel RF IN connector.** The RF IN connector is installed on the rear panel of the Model 8201.

-03 **CCITT filter.** A CCITT bandpass filter is added to the baseband processing circuits.

-05 **Power Reference.** A 50 MHz, 0 dBm calibrator is added to the rear panel of the Model 8201.

-07 **Audio loop-thru.** Circuitry is added to the baseband processing circuits to permit the use of custom external filters.

-08 **CCIR filter.** A CCIR bandpass filter is added to the baseband processing circuits.

-09 **C-MESSAGE filter.** A C-MESSAGE bandpass filter is added to the baseband processing circuits.

1-7. Inquiries regarding special applications of the Model 8201 to specific customer requirements are invited. Direct such inquiries to the Applications Engineering Department of Boonton Electronics Corporation.

1-8. PERFORMANCE SPECIFICATIONS.

1-9. Performance specifications for the Model 8201 are listed in Table 1-1.

1-10. OUTLINE DIMENSIONS.

1-11. Outline dimensions of the Model 8201 are shown in Figure 1-1.

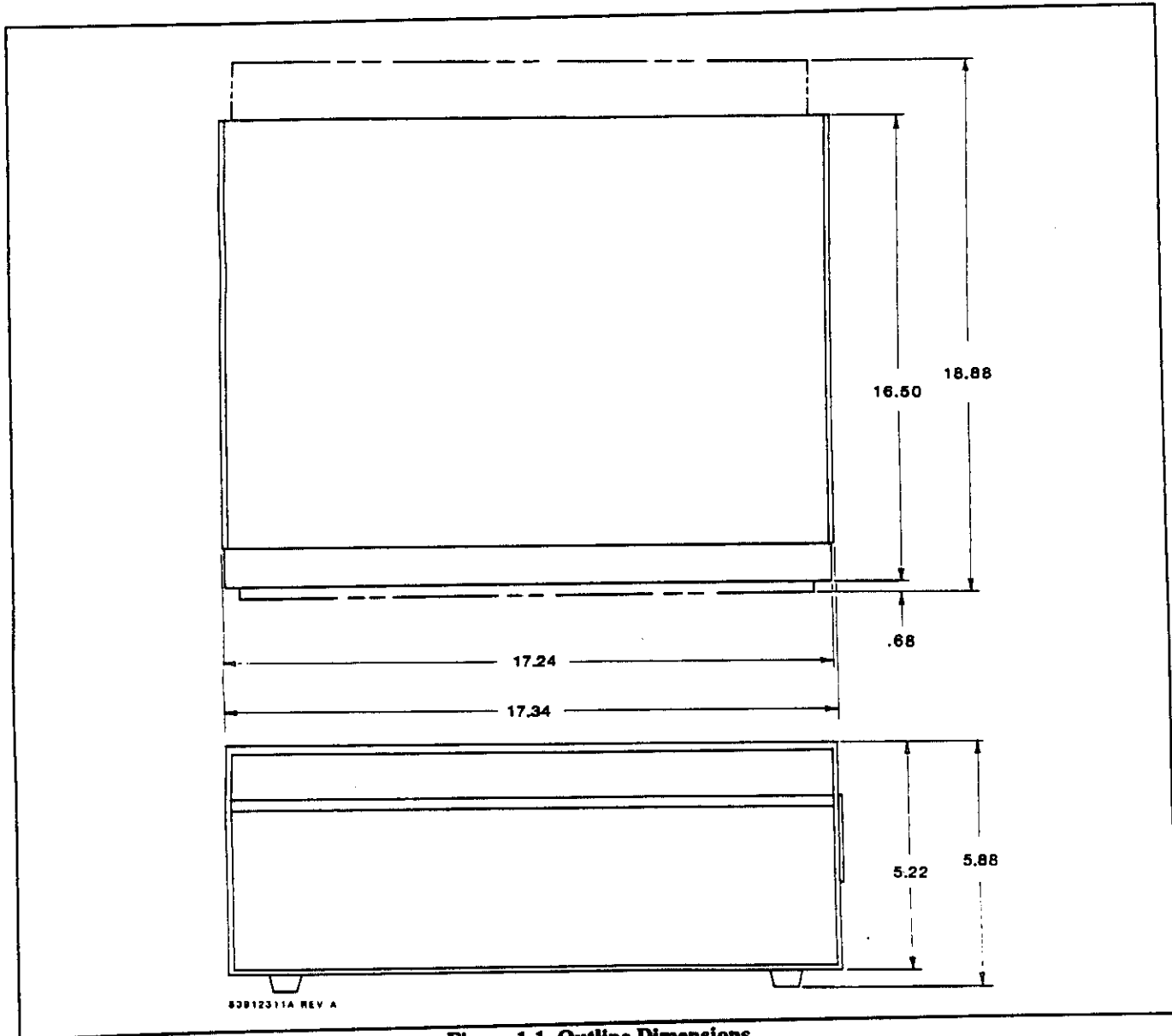


Figure 1-1. Outline Dimensions.

TABLE 1-1. PERFORMANCE SPECIFICATIONS.

RF INPUT	
Frequency Range	: 100 kHz to 2.5 GHz
Tuning (8)	: Automatic, typical acquisition time one second, or manual from keyboard or IEEE-488 bus.
Sensitivity	: 10 mV, Frequency Range: 100 kHz to 520 MHz. : 15 mV, Frequency Range: 520 MHz to 1000 MHz. : 28 mV, Frequency Range: 1000 MHz to 1500 MHz. : 50 mV, Frequency Range: 1500 MHz to 2500 MHz.
Maximum Input (8)	: 1 watt (7 V rms, +30 dBm)
Maximum Safe Input (8)	: 40 Vdc, 35 Vac (25 W for source SWR < 4)
Level Set (8)	: Automatic, typical acquisition time one second for levels up to 7 V, or manual from keyboard or IEEE-488 bus.
Input Impedance	: 50 ohms nominal.
VSWR	: < 1.50, Frequency Range: 100 kHz to 2.0 GHz. : < 1.80, Frequency Range: 2.0 GHz to 2.5 GHz.
FREQUENCY MODULATION	
Measurement	: + peak, -peak, peak average, quasi-peak, and rms.
Rates	: 20 Hz to 15 kHz, Frequency Range: 0.2 to 0.5 MHz. : 20 Hz to 50 kHz, Frequency Range: 0.5 MHz to 10 MHz. : 20 Hz to 220 kHz, Frequency Range: 10 MHz to 2.5 GHz.
Range(6)	: 0 to carrier(kHz)/10 kHz peak, Frequency Range: 0.2 to 0.5 MHz. : 0 to 150 kHz peak, Frequency Range: 0.5 to 10 MHz. : 0 to 500 kHz peak, Frequency Range: 10 MHz to 2.5 GHz.
Resolution(7)	: 1 Hz, 0.000 to 5.000 kHz deviation. : 10 Hz, 5.00 to 50.00 kHz deviation. : 100 Hz, 50.0 to 500.0 kHz deviation.
Accuracy(1) (2)	: 1% of reading, 30 Hz to 5 kHz rates, Frequency Range: 0.2 to 0.5 MHz. : 2% of reading, 5 kHz to 7.5 kHz, Frequency Range: 0.2 to 0.5 MHz. : 1% of reading, 30 Hz to 15 kHz, Frequency Range: 0.5 to 10 MHz. : 2% of reading, 15 kHz to 30 kHz, Frequency Range: 0.5 to 10 MHz. : 1% of reading, 30 Hz to 100 kHz, Frequency Range: 0.01 to 2.5 GHz. : 2% of reading, 100 kHz to 150 kHz, Frequency Range: 0.01 to 2.5 GHz.
Distortion	: < 0.1% for deviations < 30 kHz, Frequency Range: 0.2 to 0.5 MHz. : < 0.1% for deviations < 75 kHz, Frequency Range: 0.5 to 10 MHz. : < 0.1% for deviations < 100kHz, Frequency Range: 0.01 to 2.5 GHz.
Residual FM (3 kHz low-pass)	: < 15 Hz RMS at 2000 MHz carrier, decreasing linearly with frequency. : < 1 Hz RMS at 100 MHz.(floor)
Residual FM (15 kHz low-pass)	: < 30 Hz RMS at 2000 MHz carrier, decreasing linearly with frequency. : < 2 Hz RMS at 100 MHz.(floor)
Incidental FM	: < 20 Hz peak deviation at 50% AM, 30 Hz to 3 kHz measurement bandwidth.

TABLE 1-1. PERFORMANCE SPECIFICATIONS CONTINUED.

AMPLITUDE MODULATION	
Measurement	: + peak, -peak, peak average, quasi-peak, and rms.
Rates	: 20 Hz to 15 kHz, Frequency Range: 0.1 to 0.5 MHz. : 20 Hz to 50 kHz, Frequency Range: 0.5 to 10 MHz. : 20 Hz to 220 kHz, Frequency Range: 10 MHz to 2.5 GHz.
Range	: 0 to 99.9%.
Resolution	: 0.001% from 0.000 to 5.000% AM. : 0.01% from 5.00 to 50.00% AM. : 0.1% from 50.1 to 99.9% AM.
Accuracy(1) (2)	: 1% of reading, 30 Hz to 5 kHz, Frequency Range: 0.1 to 0.5 MHz. : 2% of reading, 30 Hz to 7.5 kHz, Frequency Range: 0.1 to 0.5 MHz. : 1% of reading, 30 Hz to 15 kHz, Frequency Range: 0.5 to 10 MHz. : 2% of reading, 30 Hz to 30 kHz, Frequency Range: 0.5 to 10 MHz. : 1% of reading, 30 Hz to 100 kHz, Frequency Range: 0.01 to 2.5 GHz. : 2% of reading, 30 Hz to 150 kHz, Frequency Range: 0.01 to 2.5 GHz.
Distortion	: < 0.3% for depths up to 90%
Residual AM(3)	: 0.02% RMS, 30 Hz to 3 kHz bandwidth. : 0.05% RMS, 30 Hz to 15 kHz bandwidth.
Incidental AM (3 kHz low-pass)	: < 0.2% AM peak at 5 kHz deviation, Carrier Frequency < 10 MHz. : < 0.2% AM peak at 50 kHz deviation, Carrier Frequency > 10 MHz.
PHASE MODULATION	
Measurement	: + peak, -peak, peak average, quasi-peak, and rms.
Rates	: 100 Hz to 15 kHz, Frequency Range: 0.2 to 0.5 MHz. : 20 Hz to 50 kHz, Frequency Range: 0.5 to 10 MHz. : 20 Hz to 100 kHz, Frequency Range: 10 MHz to 2.5 GHz.
Range(4)	: 0 to CARRIER(kHz)/10 RAD peak, Frequency Range: 0.2 to 0.5 MHz. : 0 to 150 RAD peak, Frequency Range: 0.5 to 10 MHz. : 0 to 500 RAD peak, Frequency Range: 10 MHz to 2.5 GHz.
Resolution(5)	: 0.001 RAD, 0.000 to 5.000 RAD deviation. : 0.01 RAD, 5.00 to 50.00 RAD deviation. : 0.1 RAD, 50.0 to 500.0 RAD deviation.
Accuracy(1) (2)	: 3% of reading, 200 Hz to 7.5 kHz, Frequency Range: 0.2 to 0.5 MHz. : 3% of reading, 200 Hz to 30 kHz, Frequency Range: 0.5 MHz to 2.5 GHz.

TABLE 1-1. PERFORMANCE SPECIFICATIONS CONTINUED.

Distortion	: < 0.1% for deviations < 30 RAD, Frequency Range: 0.2 to 0.5 MHz. : < 0.1% for deviations < 75 RAD, Frequency Range: 0.5 to 10 MHz. : < 0.1% for deviations < 100 RAD, Frequency Range: 0.01 to 2.5 GHz.
Residual PM	: < 0.1 RAD RMS at 2 GHz decreasing linearly with frequency. : < 0.005 RAD RMS at 100 MHz. (floor)
Incidental PM	: < 0.02 RAD peak at 50 % AM, 30 Hz to 3 kHz bandwidth.
CARRIER FREQUENCY	
Range	: 100 kHz to 2.5 GHz.
Resolution	: 10 Hz, Frf < 1000 MHz. : 100 Hz, Frf > 1000 MHz.
Accuracy	: reference accuracy \pm 3 digits.
Reference	: 10.0000 MHz, 1 X 10 ⁻⁶ /year aging. : 1 X 10 ⁻⁶ /degree C temperature influence, from 0 to 50 degrees C.
CARRIER LEVEL	
Range*	: -47.0 (-27.0) to + 30.0 dBm, Frequency Range: 0.1 to 520 MHz. : -37.0 (-17.0) to + 30.0 dBm, Frequency Range: 520 to 1500 MHz. : -33.0 (-13.0) to + 30.0 dBm, Frequency Range: 1500 to 2500 MHz. * With carrier frequency set. () values in automatic mode.
Frequency Range	: 100 kHz to 2500 MHz.
Resolution	: 0.01 dB or 0.1 millivolts.
Accuracy	: \pm 1 dB, Frequency Range: 0.1 to 520 MHz. : \pm 2.0 dB, Frequency Range: 520 to 1500 MHz. : \pm 3.0 dB, Frequency Range: 1500 to 2500 MHz.
AUDIO FREQUENCY	
Range	: 10 Hz to 220 kHz.
Resolution	: 0.1 Hz from 10 Hz to 1 kHz. : 1 Hz from 1 kHz to 10 kHz. : 10 Hz from 10 kHz to 100 kHz. : 100 Hz above 100 kHz.
Accuracy	: reference accuracy \pm 1 count.

TABLE 1-1. PERFORMANCE SPECIFICATIONS CONTINUED.

AUDIO DISTORTION/SINAD	
Frequency Range	: 20 Hz to 20 kHz.
Tuning	: Automatic if modulation frequency is within range, or manual from keyboard or IEEE-488 bus.
Distortion Range	: 0.01 TO 100% THD or 0 to 80 dB SINAD.
Resolution	: 0.01%, Range: 0.01 TO 9.99%. : 0.1%, Range: 10.0 TO 99.9%. : 0.01 dB, Range: 0 TO 80 dB SINAD.
Accuracy	: $\pm 10\%$ or ± 1 dB SINAD. Residual modulation must be accounted for in distortion measurements.
Residual Distortion	: < 0.1 % or 60 dB SINAD.
AUDIO FILTERS	
High-pass	: < 10 Hz gaussian, less than 10 % droop with 5 Hz square wave.(8) : 30, 300 and 3000 Hz, 3-pole Butterworth.
Low-pass	: 3 and 15 kHz, 3-pole Butterworth. : 20 kHz, 3-pole Bessel. : 50 and 220 kHz, 7-pole Butterworth.
De-emphasis	: 25, 50, 75, and 750 μ s.
Accuracy	: $\pm 4\%$ 3 dB corner and time constant.
AM CALIBRATOR	
	: internal, 50.00% depth, 0.1% accuracy.
FM CALIBRATOR	
	: internal, 125.0 kHz deviation, 0.1% accuracy.
PM CALIBRATOR	
	: internal, 136.3 RAD deviation, 1% accuracy.
GENERAL	
Power Requirements	: 100, 120, 220, or 240 volts, $\pm 10\%$, 50-400 Hz, single phase, approx. 65 VA.
Operating Temperature	: 0 to 55 degrees C.
Dimensions	: 17.25 inches (43.8 cm) wide, 5.75 inches (14.6 cm) high, 18.75 inches (47.6 cm) deep
Weight	: 28 lbs (12.7 kg)
Accessories Included	: rack mounting hardware.

TABLE 1-1. PERFORMANCE SPECIFICATIONS CONTINUED.

SUPPLEMENTAL SPECIFICATIONS	
AF OUT (8)	: Uncalibrated, approx. 1 V into 600 ohms at 5000 counts on display. Source impedance 600 ohms.
IF OUT (8)	: Approximately 0 dBm into 50 ohms. : Frequency 1.21 MHz nominal for carriers from 10 to 2500 MHz, 346 kHz for carriers from 2 to 10 MHz, and 100 kHz to 2 MHz for carriers below 2 MHz. : Source impedance 50 ohms.
AM OUT (8)	: DC coupled, 0.02 volts peak-to-peak per 1% AM depth. Source impedance 600 ohms.
FM OUT (8)	: DC coupled, 2 volts peak-to-peak per ± 100 kHz deviation. Source impedance 600 ohms.
DIST OUT (8)	: Uncalibrated, approximately 1 V rms into 600 ohms at 5000 counts on display. Source impedance 600 ohms.
REF IN (8)	: TTL compatible for external timebase. Switching is automatic.
IEEE-488 (8)	: Complies with IEEE-488-1978. Implements AH1, SH1, T6, TE0, L4, LE0, SR1, RL1, PF0, DC1, DT1, C0, and E1.
Stereo Separation (8)	: > 48 dB, 50 Hz to 15 kHz, < 10 to 220 kHz bandwidth.
AVIONICS AM CALIBRATION (optional)	
Accuracy	: $\pm 0.7\%$, 20 to 40% AM, at 30 Hz to 3 kHz rates, < 10 to 15 kHz filters.
Flatness	: $\pm 0.4\%$ for constant AM between 20 and 40%, and 90 and 150 Hz rates.
POWER REFERENCE (optional)	
Frequency	: 50 MHz, $\pm 1\%$.
Power Accuracy	: 0.7% initial accuracy. : $\pm 1.2\%$ over 1 year.
CCITT FILTER (optional)	
	: bandpass filter, CCITT recommendation P.53.

TABLE 1-1. PERFORMANCE SPECIFICATIONS CONTINUED.

CCIR FILTER (optional)

: bandpass filter, CCIR recommendation 468-3(DIN 45404).

C-MSG FILTER (optional)

: bandpass filter, Bell System Technical Reference 41009.

AUDIO LOOP THRU (optional)**Frequency range** : < 10 Hz to > 220 kHz.**Input impedance** : 1 Megohm, shunted by approximately 50 pF.**Output impedance** : 600 ohms**NOTES**

- (1) Peak residuals must be accounted for.
- (2) For rms add $\pm 1\%$ of reading.
- (3) For quasi-peak add $\pm 6\%$ of reading, 20 Hz to 20 kHz.
Level > 100 millivolts, carrier frequency < 520 MHz.
Above 520 MHz, residuals increase linearly with frequency.
- (4) Up to 1 kHz modulation rate. Above 1 kHz range decreases linearly with modulation frequency.
- (5) Up to 1 kHz modulation rate. Above 1 kHz resolution is determined by the product of deviation and modulation rate.
- (6) With 750 μ s de-emphasis, and pre-display selected, the deviation is limited to 50 kHz peak.
- (7) Display resolution is ten times greater with 750 μ s de-emphasis, and pre-display selected.
- (8) These specifications are for application purposes and, although typical, are not warranted.

SECTION II INSTALLATION

2-1. INTRODUCTION.

2-2. This section contains the installation instructions for the Model 8201 Modulation Analyzer, and field installable options. Included is information pertinent to unpacking, mounting, power requirements, line voltage selection, cable connections and initial inspection.

2-3. UNPACKING.

2-4. The Model 8201 is shipped complete and is ready to use upon receipt. Unpack the instrument from its shipping container and inspect it for damage. See Figure 2-1. If the contents are incomplete or the instrument shows signs of damage, notify Boonton Electronics and the carrier.

NOTE

Save the packing material and container for possible use in reshipment of the instrument, or for carrier inspection in case of shipping damage.

2-5. MOUNTING.

2-6. For bench mounting, choose a clean, sturdy, uncluttered mounting surface. For rack mounting, the accessory kit supplied with the instrument (08253301A) contains mounting ears, hardware, and instructions for attaching the ears to the Model 8201. The kit also contains line fuses, RF fuses, and an open end wrench for replacing the RF fuses.

CAUTION

Always make certain that the line voltage selector switches are set to the correct positions most nearly corresponding to the voltage of the available AC power source, and that a fuse of the correct rating is installed in the fuse holder before connecting the Model 8201 to any AC power source.

2-7. Set the line voltage selector switches, located on the rear panel, to the appropriate positions as indicated on the LINE VOLTAGE SELECT chart located next to the switches. Check that the line fuse is correct for the selected power source. The correct fuse is:

VAC + -10%	100 120	220 240	50 to 400 Hz
Fuse	3/4 ATD	3/8 ATD	65 VA

2-8. POWER FAIL PROTECTION.

2-9. If the line voltage drops more than 10% below nominal, a power fail protection circuit automatically isolates the internal random access memory. Backup power is provided by a lithium cell rated at 3.0 V and 160 mAh, with a life expectancy of more than five years. Simultaneously, the display is blanked and all internal processes stop. Normal operation resumes when nominal line voltage is restored. All conditions that existed before the loss of power, except the remote mode, will be re-established. If another power failure occurs during the restart process, the Model 8201 will discard the previous setup and perform an initialization restart.

Section 2

2-10. CABLE CONNECTIONS.

2-11. Cable connections required depend on the use of the instrument. Cable connections that may be required include:

- a. **RF IN.** RF input, front panel, 50 ohms nominal impedance. Type N connector.
- b. **AF OUT.** Audio output, front panel, 600 ohms impedance, 1 volt rms at 5000 counts on modulation display. Type BNC connector.
- c. **AM OUT.** AM output, rear panel, 600 ohms source impedance, approximately 0.2 volts per $\pm 10\%$ AM. Type BNC connector.
- d. **FM OUT.** FM output, rear panel, 600 ohms source impedance, approximately 2 volts per ± 100 kHz deviation. Type BNC connector.
- e. **IF OUT.** IF output, rear panel, 50 ohms nominal source impedance, 0 dBm level.
- f. **DIST OUT.** Distortion monitor output, rear panel, 600 ohms nominal impedance.
- g. **EXT REF.** External 10 MHz counter reference, impedance and level requirements are TTL compatible, switching is automatic. BNC connector. 0 dBm level.
- h. **IEEE-488.** Instrument bus connection. Connector compatible with IEEE-488-1975.

2-12. PRELIMINARY CHECK.

2-13. The preliminary check verifies that the Model 8201 is operational and should be performed before the instrument is placed into use.

2-14. Turn the instrument power ON. Wait several seconds then depress the INIT key. The FREQUENCY/LEVEL display will contain the instrument firmware number and the other displays will contain dashes for a period of about three seconds. The FREQUENCY/LEVEL display will then change to indicate self test progress, and finally the 'UNLOC' message will be displayed. Refer to Section 3 for the meaning of any displayed error messages.

2-15. Depress the SPCL key and enter 30 into SPCL/PRGM display using the DATA keypad. Depress the ENTER key to complete the entry. The FREQUENCY/LEVEL display should change to the '-CAL-' message. Observe the operation of the instrument. The Model 8201 is performing an internal calibration of the modulation detectors. As the calibration proceeds, the results of the calibration routines will appear in the modulation display window. The AM detector is calibrated first. The calibration point is 50.00%. If Error 20 appears in the FREQUENCY/LEVEL display window, a calibration fault has occurred and hardware maintenance is required.

2-16. The RMS detector is calibrated next using the AM waveform. Error 23 is a calibration fault. Next comes the FM detector. The nominal indication is 125.0 kHz and error code 21 is the calibration fault. Finally, the PM detector is calibrated. The nominal indication is 136.3 RAD and the error code is 22.

2-17. After the calibration routine completes, the instrument will return to normal operation. If the calibration routine completes properly, the instrument is functional.

2-18. OPTIONAL FILTERS.

2-19. Installation of the optional filters requires that the instrument cover(s) be removed. Refer to Section VI for safety precautions and disassembly details, and Figure 2-2 for filter board assembly details.

2-20. Audio Loop Thru Option -07. Remove all power and signal connections and remove the instrument top and bottom covers. Proceed as follows:

Installation

- Thread W16 (blue) coaxial cable assembly through the AUDIO OUT connector hole in the rear panel of the Model 8201.
- Slide the 3/8 washer and nut over the cable, and secure the BNC connector to the rear panel.
- Thread W17 (yellow) coaxial cable assembly through the AUDIO IN connector hole in the rear panel, and secure as above.
- Route both cables through the large openings in the sheet metal as shown in Figure 2-2.
- Snap the SMC connector on W17 (yellow) onto J1 of Filter option A15.
- Snap the SMC connector on W16 (blue) onto J2 of Filter option A15.
- Dress the two cables toward the left side of the circuit card-cage.
- Move the 2-circuit shunt from pins 8 and 9 to pins 7 and 8 of J3.
- If no other filters are to be installed, place the A15 Option board into the card guides and seat into the XA15 connector on the Motherboard. Note: The A15 option assembly is inserted directly behind the A9 (pink extractors) assembly.

2-21. Options -03, 08, and 09. Remove all power and signal connections and remove the instrument top cover. Proceed as follows:

- Insert the optional filter assembly(ies) into the appropriate mating connectors. Circuit board A15 is marked to indicate the proper location for each of the optional filters.
- Secure the optional filter assembly(ies) to the A15 assembly using two #4-40 machine screws provided.
- Place the A15 Option board into the card guides and seat into the XA15 connector on the Motherboard. Note: The A15 option assembly is inserted directly behind the A9 (pink extractors) assembly.
- Before replacing the top cover, complete performance test 13 to verify optional filter performance, as slight adjustment of the nominal insertion gain may be required.
- Replace the instrument top cover.

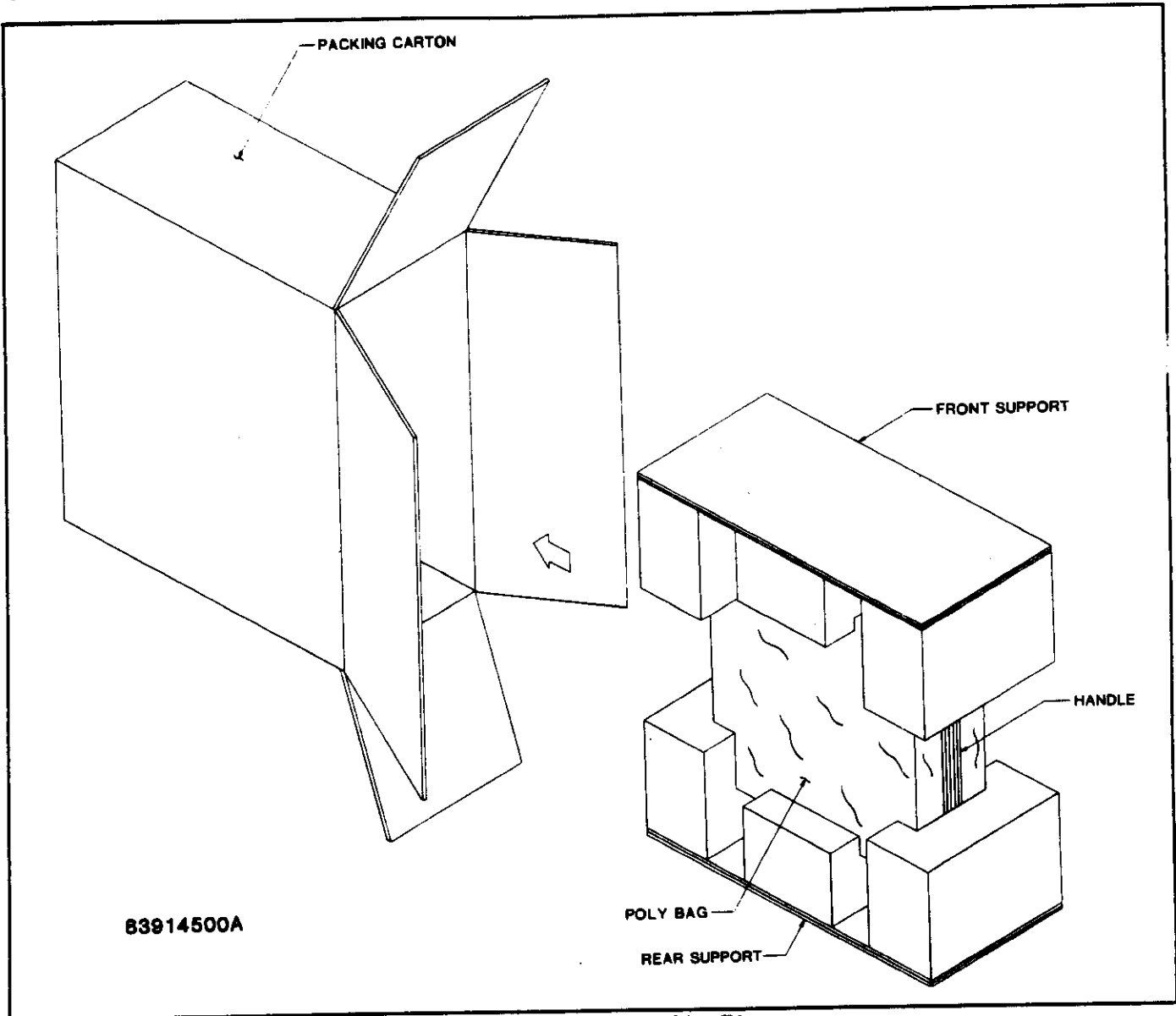


Figure 2-1. Packing and Unpacking Diagram.

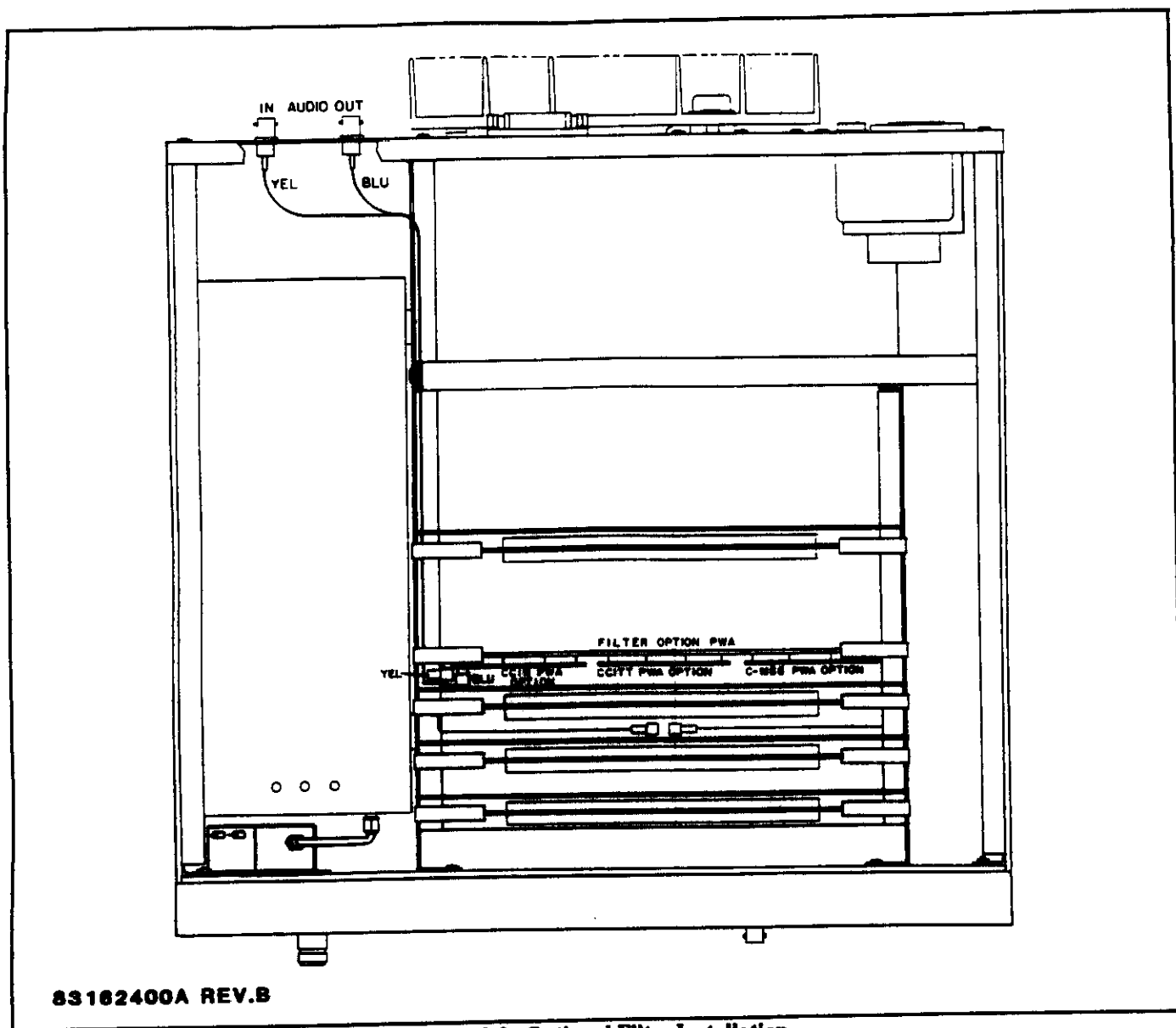


Figure 2-2. Optional Filter Installation.

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SECTION III OPERATION

3-1. INTRODUCTION.

3-2. This section contains complete operating information for the Model 8201 Modulation Analyzer. Included are descriptions of the front and rear panel controls, displays, and connectors, option selections, and instructions for local and remote modes of operation. Additionally, typical measurement situations are described.

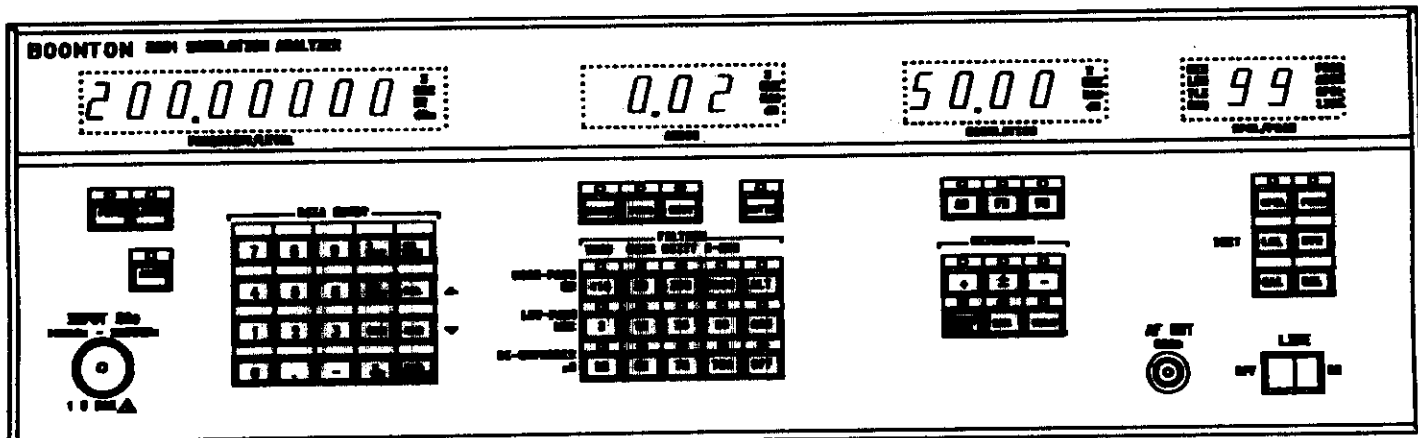
3-3. OPERATING CONTROLS, DISPLAYS, AND CONNECTORS.

3-4. The controls, indicators and connectors used during the operation of the instrument are listed in Table 3-1 and shown in Figures 3-2 and 3-3.

3-5. GETTING STARTED.

3-6. Turn on the instrument and depress the LCL(INIT) key. After a short lamp test, the FREQUENCY/LEVEL display will contain the 8201 firmware reference number and the other displays will contain dashes for about three seconds. The message 'UNLOC' will then appear in the FREQUENCY/LEVEL display window. The audio and modulation displays will contain the [= =] message and the SPCL/PRGM display will contain 99, the initialization program number. Refer to Table 3-7 for the meaning of any reported errors.

3-7. The front panel of the Model 8201 is organized for simple instrument operation. It consists of a display window and a separate keyboard area. The display area contains the FREQUENCY/LEVEL display, the AUDIO display, the MODULATION display, and the SPCL/PRGM display. The keys are organized as function keys, data keypad, and measurement control keys.



83163700A

FIGURE 3-1. Instrument Displays

3-8. DISPLAYS. (Figure 3-1)

3-9. The FREQUENCY/LEVEL display is eight characters wide and displays measurements of carrier level and frequency. Units annunciators are mV and dBm for level, MHz for frequency, and % for ratio. This display is also used for error and status messages.

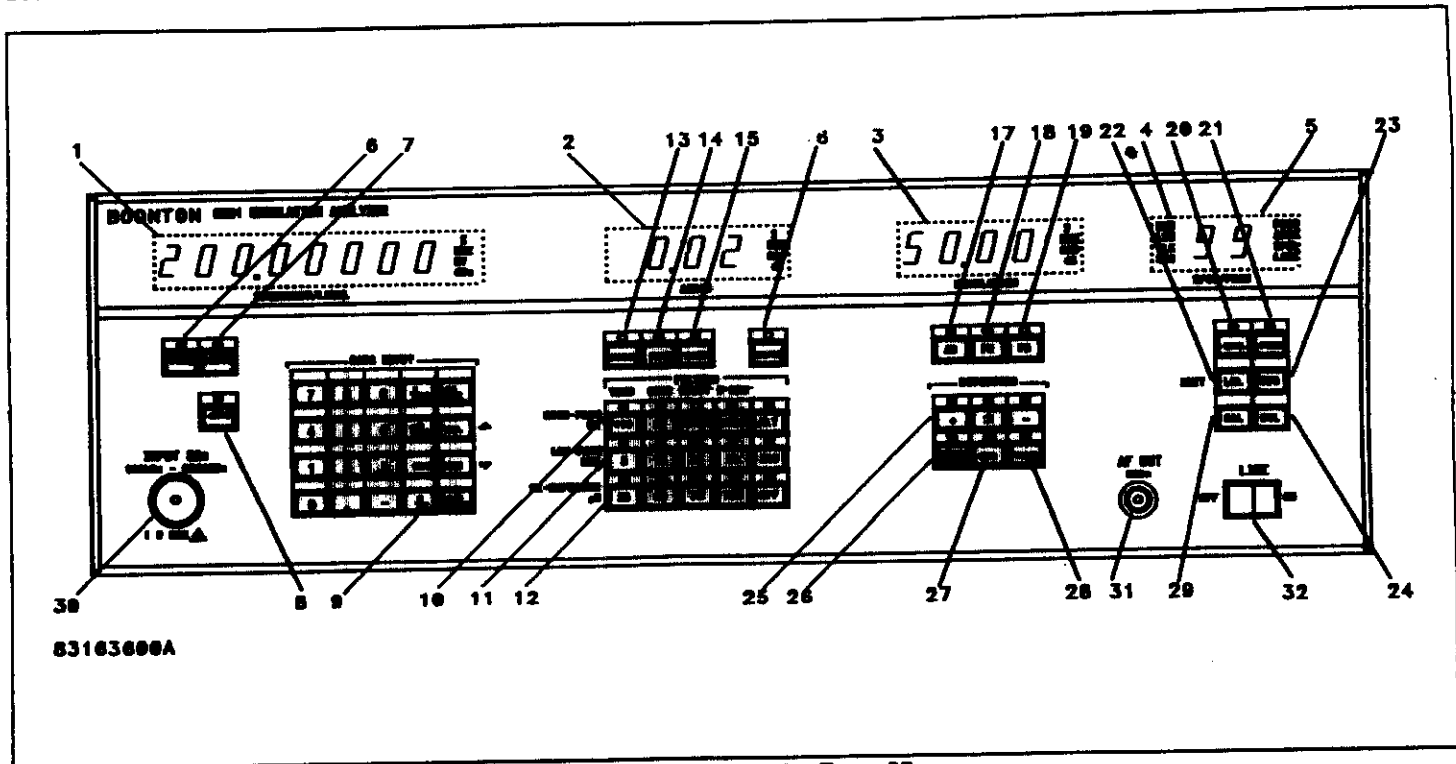


FIGURE 3-2. Model 8201, Front View.

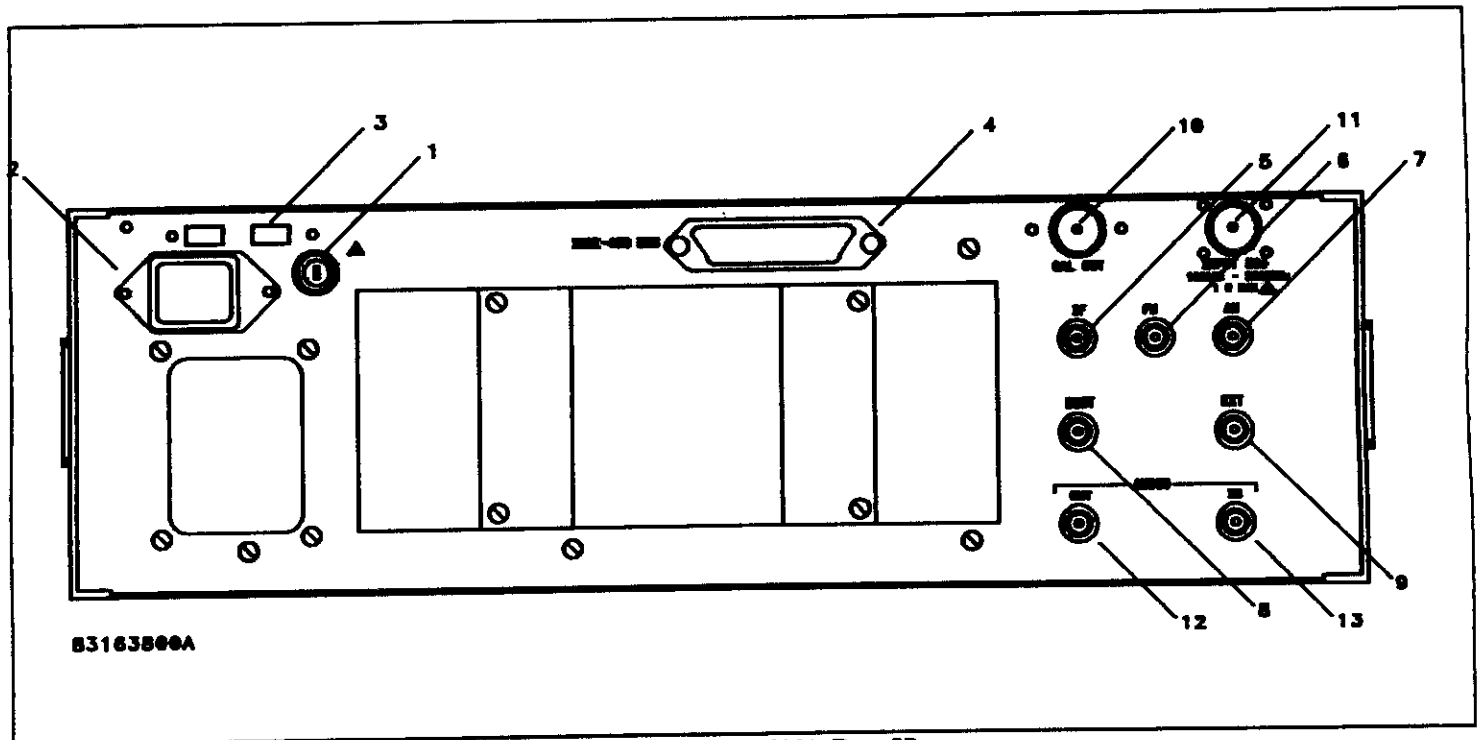


FIGURE 3-3. Model 8201, Rear View.

TABLE 3-1. CONTROLS, DISPLAYS, AND CONNECTORS.

CONTROL, INDICATOR or CONNECTOR	FIGURE and INDEX NO.	FUNCTION
FREQUENCY/LEVEL display	3-2,1	Displays carrier frequency in kHz or MHz, and RF level in dBm or mV. Alternately displays error codes and messages.
AUDIO display	3-2,2	Displays modulation frequency in Hz or kHz and distortion in % or dB SINAD.
MODULATION display	3-2,3	Displays modulation in % AM, kHz FM deviation, and RAD PM deviation. Also displays ratio in % or dB.
BUS Status display	3-2,4	Displays current IEEE-488 bus status; REM (remote enabled), LSN (listener addressed), TLK (talker addressed), and SRQ (service request active).
SPCL/PRGM display	3-2,5	Displays the current program number or selected special function.
FREQ key	3-2,6	Selects carrier frequency as the active function. Use before setting carrier frequency or to activate carrier frequency display.
LEVEL key	3-2,7	Selects carrier level as the active function. Use before setting carrier level or to activate the level display.
AUTO key	3-2,8	Forces the selected function to the measurement mode. Not active for the PRGM and SPCL functions.
DATA ENTRY keys 0 - 9 keys . key - key V/GHz key mV/MHz key kHz key %/Hz key dBm key DEL(↑) key CLR(↓) key RAD/ENTER	3-2,9 3-2,9 3-2,9 3-2,9 3-2,9 3-2,9 3-2,9 3-2,9 3-2,9 3-2,9	Numeric entry keys. Selects decimal point during data entry. Prefix for negative quantity. Selects volts or gigahertz units. Selects millivolts or megahertz units. Selects kilohertz units. Selects percent or Hertz units. Selects decibels referenced to 1 milliwatt. Deletes the last entered digit, or increments parameter. Clears errors or current data entry, or decrements parameter. Selects radians or unitless number termination.

TABLE 3-1. CONTROLS, DISPLAYS, AND CONNECTORS.

CONTROL, INDICATOR or CONNECTOR	FIGURE and INDEX NO.	FUNCTION
High-pass Hz keys < 10/THRU 30/CCIR 300/CCITT 3000/C-MSG ALT	3-2,10 3-2,10 3-2,10 3-2,10 3-2,10	Selects the < 10 Hz high-pass or THRU bandpass filter. Selects the 30 Hz high-pass or CCIR bandpass filter. Selects the 300 Hz high-pass or CCITT bandpass filter. Selects the 3000 Hz high-pass or C-MSG bandpass filter. Toggles filter selection from high-pass to bandpass.
Low-pass kHz keys 3 15 20 50 220	3-2,11 3-2,11 3-2,11 3-2,11 3-2,11	Selects the 3 kHz low-pass filter. Selects the 15 kHz low-pass filter. Selects the 20 kHz low-pass filter. Selects the 50 kHz low-pass filter. Selects the 220 kHz low-pass filter.
De-emphasis uS keys 25 50 75 750 OFF	3-2,12 3-2,12 3-2,12 3-2,12 3-2,12	Selects the 25 us de-emphasis filter. Selects the 50 us de-emphasis filter. Selects the 75 us de-emphasis filter. Selects the 750 us de-emphasis filter. Deselects the de-emphasis filters.
SINAD key	3-2,13	Selects SINAD audio distortion measurement.
FREQ (audio)	3-2,14	Selects audio frequency as the active function. Use before setting audio frequency for SINAD measurements, or to activate the audio frequency display.
DIST key	3-2,15	Selects audio distortion measurement.
RATIO key	3-2,16	Alternate action key. Changes the active display from absolute to relative. Units keys may be used to select displayed units.
AM key	3-2,17	Selects AM modulation as the active function. Use before setting AM modulation reference for subsequent ratio measurement, or to activate the AM modulation display.
FM key	3-2,18	Selects FM modulation as the active function. Use before setting FM modulation reference for subsequent ratio measurement, or to activate the FM modulation display.

TABLE 3-1. CONTROLS, DISPLAYS, AND CONNECTORS.

CONTROL, INDICATOR or CONNECTOR	FIGURE and INDEX NO.	FUNCTION
PM key	3-2,19	Selects PM modulation as the active function. Use before setting PM modulation reference for subsequent ratio measurement, or to activate the PM modulation display.
SPCL key	3-2,20	Selects special function as the active function. Use before selecting special function.
PRGM key	3-2,21	Selects instrument program as the active function. Use before selecting program number for store or recall.
LCL/INIT key	3-2,22	Causes instrument to "go-to-local" if local lockout is not active and remote is active, or initialize when the instrument is in the local state.
STO key	3-2,23	Stores the instrument setup at selected program number.
RCL key	3-2,24	Recalls instrument setup from selected program number.
PEAK keys + key - key ± key	3-2,25 3-2,25 3-2,25	Selects + peak detector for display. Selects - peak detector for display. Selects peak average modulation display. The display is $(+ \text{peak} (+) - \text{peak})/2$.
QUASI-PEAK key	3-2,26	Selects CCIR 386-3 peak detector for display. The display is peak responding, calibrated in rms.
RMS key	3-2,27	Selects a true rms detector for modulation display.
HOLD key	3-2,28	Alternate action key used to display the greater of the current or last modulation reading.
CAL key	3-2,24	Causes the selected function to be calibrated. Active for carrier LEVEL, AM, FM, and PM.

TABLE 3-1. CONTROLS, DISPLAYS, AND CONNECTORS.

CONTROL, INDICATOR or CONNECTOR	FIGURE and INDEX NO.	FUNCTION
RF IN connector	3-2,30	RF input connector, used to apply an external carrier signal.
AF OUT connector	3-2,31	Audio output connector, used to connect the demodulated signal to external test equipment.
LINE switch	3-2,32	Switches the instrument ac power supply ON or OFF.
Fuseholder	3-3,1	Holds fuse for ac line protection.
Line connector	3-3,2	Permits connection of instrument to ac power supply.
Voltage Selector Switch	3-3,3	Permits the selection of various ac power supply voltages.
IEEE-488 bus connector	3-3,4	Provides a means for connecting the Model 8201 to a system control bus.
IF out connector	3-3,5	Provides a means for connecting the intermediate frequency signal to external test equipment.
FM out connector	3-3,6	Provides a means for connecting the demodulated FM signal to external test equipment.
AM out connector	3-3,7	Provides a means for connecting the demodulated AM signal to external test equipment.
DIST out connector	3-3,8	Provides a means for connecting the distortion analyzer signal output to external test equipment.
EXT REF connector	3-3,9	Provides a means for connecting an external 10.00 MHz frequency standard to the internal timebase circuits.

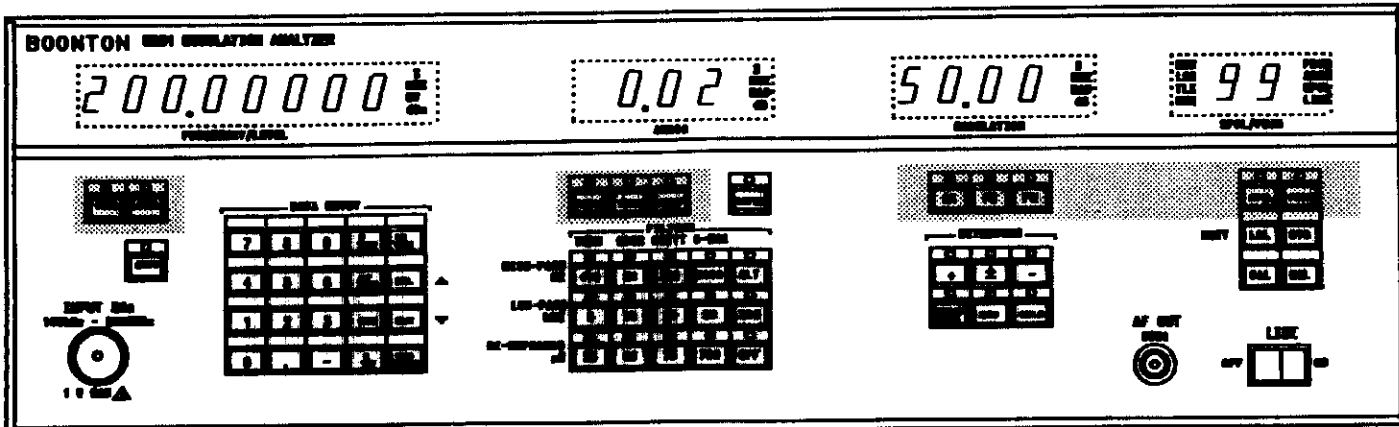
TABLE 3-1. CONTROLS, DISPLAYS, AND CONNECTORS.

CONTROL, INDICATOR or CONNECTOR	FIGURE and INDEX NO.	FUNCTION
Optional: CAL OUT connector	3-3,10	Provides a means for connecting the optional 50 MHz, 0 dBm calibrator to the Model 8201 for level calibration.
RF IN connector	3-3,11	Optional RF input connector, used to apply an external carrier signal.
AUDIO OUT connector	3-3,12	Provides a means for connecting the modulation signal to external filters or processing circuits.
AUDIO IN connector	3-3,13	Provides a means for connecting an external audio signal to the internal baseband processing circuits.

3-10. The AUDIO display is four characters wide and displays the measured audio frequency or distortion. Units annunciators are Hz and kHz for frequency, and percent and dB for distortion.

3-11. The MODULATION display is four characters wide and displays the measured modulation. Units annunciators are percent for AM and ratio, kHz for FM deviation, RAD for PM deviation, and dB for ratio measurements.

3-12. The SPCL/PRGM display is an entry only display which is two characters wide and displays selected special function, or the current instrument program number. Units annunciators are PRGM for program number, SPCL for special function, and ADRS for IEEE-488 bus address. Also included is a LINE annunciator which indicates that ac power is applied.



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FIGURE 3-4. Function Keys.

3-13. To the immediate left of the SPCL/PRGM display is the IEEE-488 status display. This display indicates REM when the Model 8201 is in the remote state, LSN when addressed as a listener, TLK when addressed as a talker, and SRQ when the Model 8201 has activated the IEEE-488 service request line.

3-14. FUNCTION KEYS. (Figure 3-4)

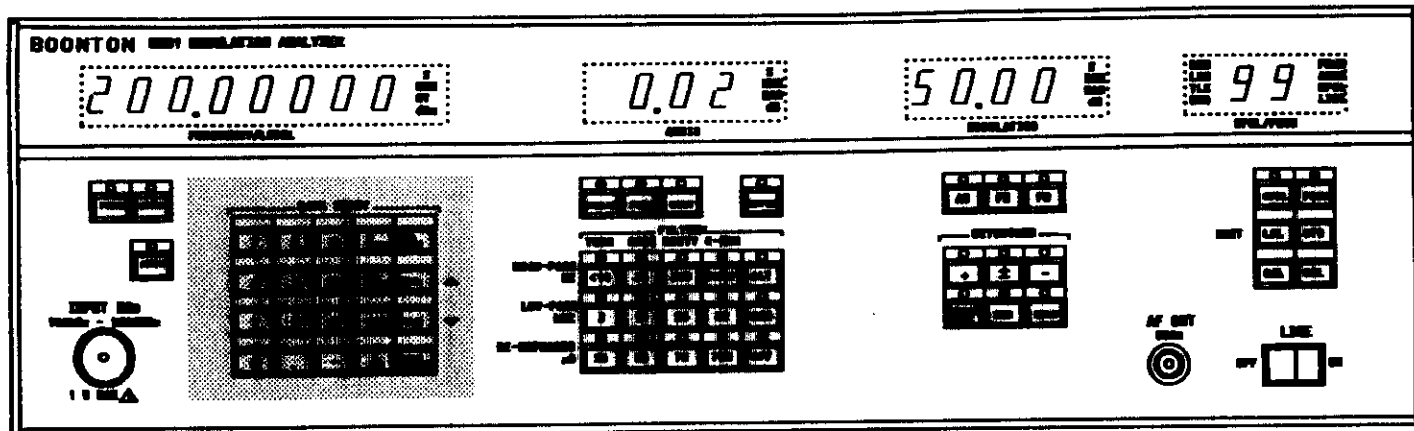
3-15. The top row of illuminated switches are the function keys. These keys are used to select the parameter to be displayed and to enable the data keypad for subsequent data entry. The functions are carrier FREQ, carrier LEVEL, audio SINAD, audio FREQ, audio DIST, AM, FM, PM, SPCL, and PRGM. The LED in the switch of the selected function will be illuminated continuously; the others will be off unless a measurement of that function is in progress. In this case the LED will flash during the measurement interval.

3-16. To select a function depress the desired function key. The units legends associated with that function will appear immediately to the right of the numeric display.

3-17. For example, select the carrier FREQ function and depress the 1 and V/GHZ keys. The display will now contain the number 1000.0000 and the active legend will be MHz.

3-18. Depress the FM function key. The LED in the carrier FREQ key will go out, and the LED in the FM key will illuminate. Depress the 1, 0, and kHz keys. The number 10.00 will now be displayed in the modulation display.

3-19. All other function keys operate in the same manner, except that data cannot be entered when the DIST or SINAD functions are selected.



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FIGURE 3-5. Data keypad.

3-20. DATA KEYPAD. (Figure 3-5)

3-21. Operation of the data keypad is conventional. Select the carrier FREQ function and depress the [8] key. The carrier frequency display will indicate '8 and the units legend will go out. The tick mark (') indicates that the number displayed has not yet been entered. Continue by depressing the [2], [.] , [1] and [5] keys and the MHZ key to enter the number. The display will now indicate 82.15000 MHz.

3-22. Note that it is not necessary to enter any trailing zeroes, nor is it necessary to depress the ENTER key if a units key is used. While this is the most efficient way to enter 82.15 MHz, it is equally valid to enter 82150 kHz, 82150000 Hz, et cetera. If at any time before entry the wrong digit is entered, depress the DEL key to clear the digit, or depress the CLR key to clear all input and restore the previous frequency display.

3-23. The kHz and GHz keys are provided for convenience when entering frequency; however, the display will only indicate in MHz. Similarly, the V key can be used for entering input level; however the display will indicate in millivolts.

3-24. The ENTER key is used for unitless quantities, such as special function and program numbers.

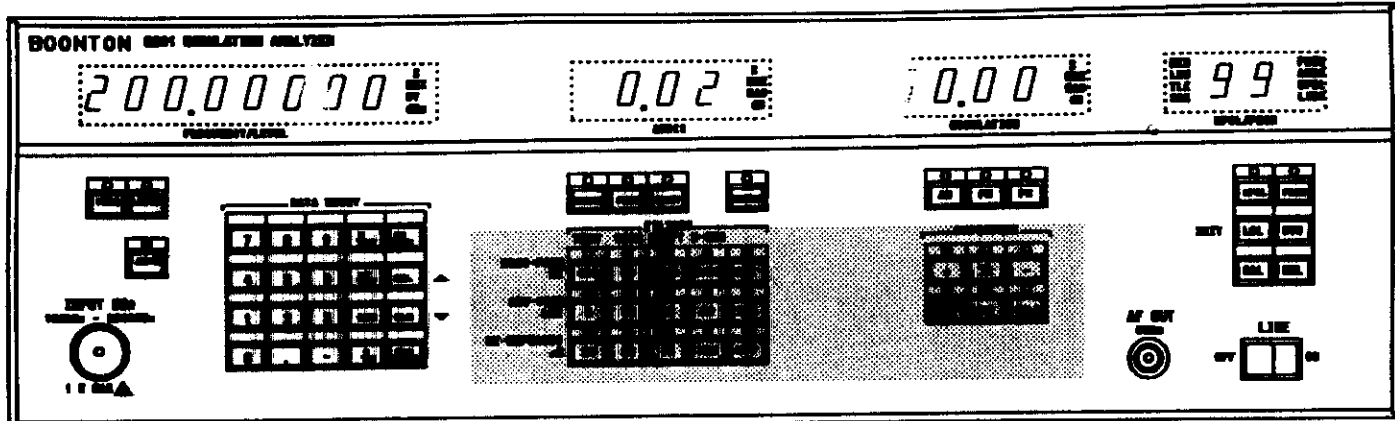
3-25. The CLR key is used to recover from errors. Without changing function, depress the dBm key. The FREQUENCY/LEVEL display will now indicate Error 9 or 11. This means that an inconsistent units key has been depressed to terminate a data entry. Depress the CLR key. The display will return to normal. A list of error codes is presented in Table 3-7, at the end of this section.

3-26. Depress the carrier LEVEL function key, then the 0 and dBm keys. The FREQUENCY/LEVEL display will now indicate 0.00 dBm. Depress the mV/MHz key. The display will change to 223.6 mV. Carrier level may be entered in millivolts, volts, or dBm. The control program will recalculate or rescale numbers as required.

3-27. The DEL and CLR keys are also labeled as up- and down-arrow keys for scrolling through SPCL function menus.

3-28. MEASUREMENT CONTROL KEYS. (Figure 3-6)

3-29. The measurement control keys consist of the groups of switches marked FILTERS and DETECTORS. These keys may be operated at any time and will affect the MODULATION and AUDIO displays. The filter switches are arranged as self-cancelling groups of four and five keys. Depressing any high-pass switch will cause the selected filter to be placed into the measurement channel and cancel any other selected high-pass filter. Similarly, depressing any low-pass filter will cause the selected filter to be placed into the measurement channel and cancel any other selected low-pass filter.



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FIGURE 3-6. Measurement Control Keys.

3-30. The maximum low-pass bandwidth selection is a function of carrier frequency. The control program will automatically adjust the low-pass filter cutoff frequency as required. The carrier breakpoints and low-pass filters are:

Carrier	Filter
< 500 kHz	15 kHz max.
< 10 MHz	50 kHz max.
> 10 MHz	220 kHz max.

3-31. The de-emphasis filters are normally available when measuring FM only. They are selected in the same manner as the high-pass and low-pass filters, but are automatically removed from the measurement channel when AM or PM modulation function is selected. The selected de-emphasis filter will be restored when the FM function is again selected. Additionally, the de-emphasis filters may be placed before or after the modulation display. This is accomplished by selecting SPCL function 7 for pre-display and SPCL function 8 for post-display de-emphasis. SPCL function 9 permits the de-emphasis filters to be selected in the AM measurement function. This is useful for performance verification of the filter 3 dB points.

3-32. The ALT key is active if optional filters are installed in the Model 8201. Optional filters available are:

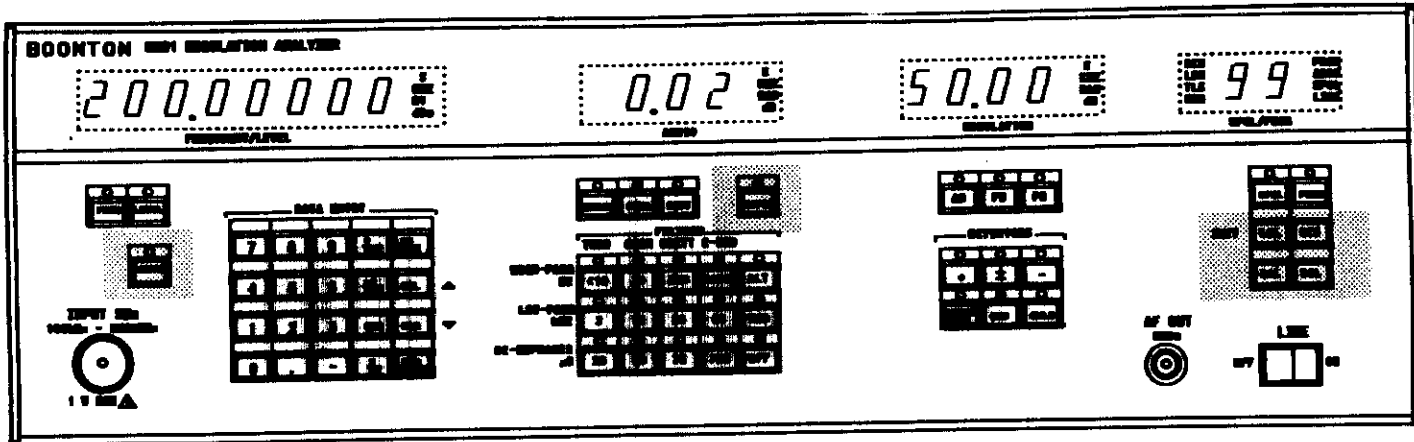
THRU	Permits connection of external filters in the audio path.
CCIR	CCIR recommendation 468-3 bandpass filter.
CCITT	CCITT recommendation P.53 bandpass filter.
C-MSG	Bell System Technical Reference 41009 bandpass filter.

Any or all of these filters can be installed at one time, however, the A15 option board is required with any of the filters. The ALT key will activate the filters marked above the corresponding high-pass key, if the filters are installed. Error 19 will be displayed if an optional filter is not installed and the key is depressed.

3-33. The second group of measurement control keys is the DETECTOR switches. The peak detectors are normally used to measure modulation, however, precision rms detectors are included in the Model 8201. These detectors are used primarily to characterize noise residuals and complex or distorted modulation signals. Two detectors are provided. The normal function of the RMS key is to select an rms calibrated display; however, SPCL function 18 can be executed to change the RMS key to select rms detection calibrated in peak for sinusoidal modulation. This is particularly useful when comparing peak and rms indications of noisy signals. A quasi-peak detector, compatible with CCIR 368-3, is available for use with the CCIR filter option. This detector is always available, whether the optional filter is installed or not.

3-34. The Peak +, -, and \pm keys, the RMS key, and the QUASI-PEAK key are arranged such that only one detector can be selected at a time.

3-35. The HOLD key is used to activate the hold detector mode. It is an alternate action key which can be used with any detector. In operation, as modulation measurements are made, the larger of the current measurement or the previous measurement



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FIGURE 3-7. Other Keys.

becomes the displayed modulation. Depress the HOLD key to activate this mode, then depress the key again to cancel.

3-36. OTHER KEYS. (Figure 3-7)

3-37. The RATIO key is an alternate action key which changes the active display from absolute to relative. In addition, the ratio measurement can be made relative to the current display, or to a set value. Ratio can be displayed in percent, measurement units, or dB by using the %, units, and dB keys in the data keypad.

3-38. The AUTO key is used to resume automatic operation of a particular function. It is active for the carrier FREQ, carrier LEVEL, audio FREQ, AM, FM, and PM functions. When numerical data is entered into a particular function window, the LED in the AUTO key will go out. This indicates that the selected function is not displaying a measured value. To resume measurement, depress the AUTO key. If carrier FREQ is the active function, depressing the AUTO key will always force the Model 8201 to reacquire the carrier signal.

3-39. The LCL(INIT) key is a dual function key. If the Model 8201 is in the local IEEE-488 bus state and the key is depressed an initialization restart occurs. This is similar to a power on reset except that the current instrument status is lost. This does not include bus address or end-of-string selection. If the Model 8201 is remote enabled, and the local lockout bus state is not active, the instrument will return to front panel control.

3-40. The STO and RCL keys are used with the PRGM function key to store and recall one of the 100 possible instrument control settings.

3-41. The CAL key is used to calibrate the active function. It is active for carrier LEVEL, AM, FM, and PM modulation.

3-42. DISPLAYED MESSAGES.

3-43. When the Model 8201 unlocks, the FREQUENCY/LEVEL display will be overwritten with the 'UNLOC' message and the AUDIO and MODULATION displays will be overwritten with the [= =] symbol, which means display out of range. When a valid carrier is acquired, the displays will return to normal.

3-44. The 'IFHI' and 'IFLO' messages appear in the modulation display and indicate that the intermediate frequency level is not within range to make an accurate measurement. SPCL functions 13 and 14 allow the operation of these messages to be modified.

3-45. When the CAL key is depressed, or during the execution of SPCL function 30, the message '-CAL-' is written to the FREQUENCY/LEVEL display to indicate that a calibration sequence is in progress.

3-46. A normal error response is for the word 'Error' to appear in the FREQUENCY/LEVEL display followed by a number indicating the nature of the error. Error codes are tabulated in Table 3-7 along with a description of the error.

3-47. The message 'SELFCHK', followed by a changing digit, appears in the FREQUENCY/LEVEL display at power on, and indicates that a hardware check is in progress. Any error messages displayed indicate a hardware problem. See Table 3-8 for the meaning of any reported errors.

3-48. Other displayed messages are described in detail in the pertinent operation section.

3-49. SPECIAL FUNCTIONS.

3-50. Several of the Model 8201 operating features are internally programmable by selecting a SPCL function. These functions allow the operator to change measurement configuration, as well as change the hardware state of the instrument. Some of the more useful SPCL functions are listed below, the others are included in Table 3-2.

3-51. SPCL 0, CLEAR ALL SPECIALS.

3-52. SPCL function 0 allows the operator to reset any active SPCL functions. The instrument special status is returned to the defaults indicated in Table 3-2.

3-53. SPCL 1-4, MODULATION RANGE SETTINGS.

3-54. SPCL functions 1 through 4 permit the operator to select the modulation display range. This is useful for speeding up measurements where modulation may be removed temporarily, or in situations where the modulation range is known. This feature is also useful when decreased display resolution is desired. SPCL 1 is the default function which is autorange. The others are:

SPCL 2	5.000 full-scale
SPCL 3	50.00 full-scale
SPCL 4	500.0 full-scale

3-55. SPCL 5, ENABLE SLOW PEAK DETECTOR MODE.

3-56. SPCL function 5 is provided to slow the response of the peak detectors for modulation signal frequencies below 200 Hz. The detectors are optimized for signal frequencies greater than 200 Hz for maximum measurement speed. Below 200 Hz additional filtering is required.

3-57. SPCL 6, DISABLE SLOW DETECTOR MODE.

3-58. SPCL function 6 allows the operator to cancel SPCL 5. This is the default setting.

3-59. SPCL 7, SET PRE-DISPLAY DE-EMPHASIS.

3-60. SPCL function 7 allows the operator to change the de-emphasis filter location from post-display to pre-display. This means that the de-emphasis filters will affect the displayed modulation readings as well as the AF OUT signal. This is useful for comparison of receiver de-emphasis networks to the precision network used in the Model 8201.

3-61. SPCL 8, SET POST-DISPLAY DE-EMPHASIS.

3-62. SPCL function 8 allows the operator to change the de-emphasis filter location from pre-display to post-display. This means that the de-emphasis filters will not affect the displayed modulation readings, but will affect the AF OUT signal. This is the default setting for the de-emphasis filters.

TABLE 3-2. SPECIAL FUNCTIONS.

SPECIAL FUNCTION	PURPOSE
0	Reset all SPCL functions to defaults. Indicated by ♦
1 ♦	Set Modulation Range to AUTO.
2	Set Modulation Range to 5.000 full-scale.
3	Set Modulation Range to 50.00 full-scale.
4	Set Modulation Range to 500.0 full-scale.
5	Set slow peak detector mode.
6 ♦	Cancel slow peak detector mode.
7	Set de-emphasis to Pre-display.
8 ♦	Set de-emphasis to Post-display.
9	Enable de-emphasis for AM measurements.
10 ♦	Disable de-emphasis for AM measurements.
11	Set dB resolution to 0.001 dB for ratio measurements.
12 ♦	Set dB resolution to 0.01 dB for ratio measurements.
13 ♦	Enable IFHI and IFLO messages for FM measurements.
14	Disable IFHI and IFLO messages for FM measurements.
15	Set IEEE-488 end-of-string character.
16	Set IEEE-488 SRQ mask. See text.
17	Set IEEE-488 bus address.
18	Set RMS key to $\sqrt{2}$RMS.
19 ♦	Reset RMS key to RMS.
20	Set 750 uS de-emphasis gain to 1.
21 ♦	Set 750 uS de-emphasis gain to 10.
22	Activate function hold display mode.
23	Toggle fast acquisition mode.
24	Display IF frequency.
25	Display LO frequency.
26	Display calibrator frequency.
27	Reserved.
28	View firmware code.
29	View instrument serial number.
30	Execute complete detector calibration.
31	Enable 8200 error code reporting.
32 ♦	Enable 8201 error code reporting.
33	Activate key test routine.
34	Activate Display test routine.
35	Activate AGC test routine.
36	Activate COUNTER test routine.
37	Activate LOCAL OSCILLATOR test routine.
38	Activate DAC test routine.
39	Activate A/D test routine.
40-49	Reserved.
50-99	ACCESSABLE ONLY WITH A9JP1 INSTALLED. See Section VI.

3-63. SPCL 9-10, SET/RESET DE-EMPHASIS IN AM.

3-64. SPCL function 9-10 alters the operation of the de-emphasis filters such that the filters are active for AM and modulation measurements. This means that the de-emphasis filters will affect AF OUT signal and, optionally, the displayed modulation readings in the modulation measurement mode as well as the FM mode. This is useful for performance testing of de-emphasis time constants. SPCL 10 restores FM only operation.

3-65. SPCL 11, 0.001 DB RESOLUTION FOR LOG MEASUREMENTS.

3-66. SPCL function 11 allows the operator to select a measurement resolution of 0.001 dB for ratio measurements in the dB mode. This function is useful when increased display resolution is desired.

3-67. SPCL 12, 0.01 DB RESOLUTION FOR LOG MEASUREMENTS.

3-68. SPCL function 12 allows the operator to select a display resolution of 0.01 dB for ratio measurements in the dB mode. This is the default resolution for power and log ratio measurement display.

3-69. SPCL 30, MODULATION DETECTOR CALIBRATION.

3-70. SPCL function 30 is the modulation detector calibration program. When executed the -CAL- message will appear in the FREQUENCY/LEVEL display and detector calibration will begin. The calibration routine will take about 80 seconds to complete. The AM detector is calibrated first, followed by the rms detector, the FM detector and finally the PM detector. If calibration errors occur, they will be displayed as the particular detector is being calibrated.

3-71. FRONT PANEL CONNECTORS.

3-72. The Model 8201 is normally supplied with two connectors on the front panel, RF IN, and AF OUT. These connectors are the most often used. Optionally, the RF IN connector can be placed on the rear panel.

3-73. The RF IN connector is the means to apply a test signal to the Model 8201. It is a type N connector which is the preferred connector in this frequency range. The nominal input impedance at the RF IN is 50 ohms (SWR < 1.5). The RF IN connector is designed to accept a fuse, although one is not installed since the Model 8201 is designed to accept inputs of 40 volts dc, or 35 volts ac without damage. A protection circuit automatically disconnects ac inputs exceeding about +32 dBm. The carrier level response is shown in Figure 3-8.

3-74. The AF OUT connector is a type BNC. The signal at this connector is a sample of the recovered modulation. As a result, the amplitude varies with modulation and modulation range settings and the signal is affected by the high-pass and low-pass filters and the de-emphasis networks. The nominal level is 1 volt into 600 ohms at 5000 counts on the modulation display. Source impedance is 600 ohms. Amplitude variations will also occur at the AF OUT connector with carrier level if the AM measurement mode is selected even though the modulation is constant. This happens because the Model 8201 uses a microprocessor controlled discrete AGC system rather than an analog one. The AM indication is not affected since the AM detector level is measured for each displayed AM indication.

3-75. REAR PANEL CONNECTORS.

3-76. The most prominent connector on the rear panel of the Model 8201 is the IEEE-488 connector. This connector provides a means of incorporating the Model 8201 into an automatic test system. Complete instrument operation when connected to the IEEE-488 bus is covered in later paragraphs.

3-77. The connector marked IF OUT is a type BNC connector with a source impedance of 50 ohms which provides a sample of the frequency translated carrier signal. The nominal level is 0 dBm, and the frequency is determined by the carrier frequency as follows:

Carrier	IF Frequency
< 2 MHz	same as carrier
2 to 10 MHz	346 kHz
> 10 MHz	1.211 MHz

Operation

3-78. The connector marked AM OUT is a dc coupled sample of the output of the AM detector. This output is always active and has a small signal bandwidth of 220 kHz, corresponding to the 220 kHz filter setting on the front panel. Additional filtering may be required to use this signal if the carrier frequency is below 10 MHz. The nominal sensitivity is 0.2 volts peak-to-peak for 10% AM. The dc and ac portions of this signal can be used to calculate AM according to the following formula:

$$\%AM = 100\% \times \text{volts ac peak} / (\text{Volts dc} - \text{offset})$$

3-79. The offset in the above equation can be determined by depressing the carrier FREQ and V/MHZ keys and removing the RF IN connection, then noting the dc voltage at the AM OUT connector. Reconnect the carrier signal and measure the ac and dc components. For example:

$$\begin{aligned} \text{offset} &= +7 \text{ millivolts dc} \\ \text{ac volts} &= 0.35 \text{ volts rms} \\ &= 0.5 \text{ volts peak} \\ \text{dc volts} &= 1.008 \text{ volts} \\ \%AM &= 100\% \times 0.5 / (1.008 - .007) = 49.95\% \end{aligned}$$

3-80. The connector marked FM OUT is a dc coupled sample of the output of the FM detector. This output is always active and has a small signal bandwidth of about 220 kHz, corresponding to the 220 kHz filter setting on the front panel. Additional filtering may be required to use this signal if the carrier frequency is below 10 MHz. The nominal sensitivity is 2 volts peak-to-peak for 100 kHz deviation. When the IF frequency is 1.211 MHz, the dc voltage will be approximately -1.3 volts, and at 346 kHz + 7.6 volts. To determine the sensitivity at this connector, apply an unmodulated carrier at about 1 MHz. Note the dc voltage at the FM OUT connector and then change the frequency to 1.5 MHz. The sensitivity is:

$$\text{volts dc @ 1.5 MHz} - \text{volts dc @ 1.0 MHz} / 0.5 \text{ MHz}$$

For example:

$$\begin{aligned} \text{volts dc at 1.5 MHz} &= -4.4 \\ \text{volts dc at 1.0 MHz} &= +0.887 \\ \text{sensitivity} &= [(-4.4) - (0.887)] / 0.5 \\ &= -10.57 \text{ volts/MHz or} \\ &= -1.057 \text{ volts/100kHz} \end{aligned}$$

Note

The sense of the recovered audio signal is reversed for carriers below 2 MHz. The control program automatically reverses the sense of the peak detectors below 2 MHz.

3-81. The connector marked DIST OUT is a sample of the audio signal with the fundamental frequency component removed. The source impedance is 600 ohms. The level is proportional to the distortion indication and is approximately 10 millivolts rms into 600 ohms at 1% distortion. The signal is useful in determining the character of the distortion products of a demodulated signal.

3-82. The connector marked EXT REF provides a means to connect a precision timebase reference to the counter circuits of the Model 8201. This input is TTL compatible, that is, the input circuit is a TTL gate with a termination network. Reference switching from internal to external is automatic when the external signal is present.

3-83. MEASURING AND SETTING CARRIER FREQUENCY.

3-84. The Model 8201 uses a sampling technique to convert frequency. Using this technique it is necessary only that the sampling frequency (and as a result the local oscillator frequency) vary over one octave to convert frequencies over the operating range of the instrument. In practice, more than one octave is covered, but the details of operation remain the same. For any carrier in the operating range of the instrument and any local oscillator frequency, an intermediate frequency signal will be produced which is between zero and one-half of the sampling rate. This signal is used to tune the local oscillator to the correct frequency. The problem is that the harmonic number of the local oscillator creating the intermediate frequency is not known. The relationship between the three different frequencies is:

$F_{rf} = N \times F_{lo} - F_{if}$
 where F_{rf} is the carrier frequency
 F_{lo} is the local oscillator frequency
 F_{if} is the intermediate frequency
 and N is the harmonic number

3-85. The unknown quantity in the equation is N . This can be determined by varying F_{lo} and noting the change in F_{if} . The ratio of the change in F_{if} to the change in F_{lo} is the harmonic number. See Theory of Operation for complete details of the operation of the frequency acquisition circuits.

3-86. When the Model 8201 acquires a carrier signal, the harmonic number is determined as described. The displayed carrier frequency is then calculated from the above expression and displayed.

3-87. To measure carrier frequency, first depress the carrier **FREQ** function key. If the **AUTO** key LED is not illuminated, depress the **AUTO** key. The 'UNLOC' message will appear and then the measured frequency will be displayed. At this point other functions may be selected or the frequency setting can be held by depressing one of the frequency units keys: **V/GHz**, **mV/MHz**, or **kHz**. Depressing **AUTO** again will cause the instrument to reacquire the carrier signal.

3-88. The frequency of operation of the Model 8201 can be established by manual entry using the data keypad. This operation does not imply any form of preselection or filtering, merely that automatic acquisition time can be eliminated. To enter the carrier frequency depress the carrier **FREQ** key and enter the operating frequency using the data keypad. Terminate the number entry with one of the frequency units keys. For example, to set the Model 8201 to operate at 123.5 MHz, depress the [1], [2], [3], [.] and [5] keys, and then the **mV/MHz** key to complete the entry. The **FREQUENCY/LEVEL** display will now contain 125.50000 MHz and the LED in the **AUTO** key will be out.

3-89. Frequency can be entered using any consistent sets of units, as described above. Trailing zeroes are not required and the **CLR** key can be used to abort entry.

3-90. MEASURING AND SETTING CARRIER LEVEL

3-91. The Model 8201 measures carrier level by monitoring the DC output of the AM detector. By knowing the setting of the internal attenuators, this level can be referred to the input connector. Absolute adjustments are made in the displayed value to account for the frequency response of the sampling frequency converter. As a result, it is always necessary for the control program to know the carrier frequency to display the carrier level correctly. The typical frequency corrected response is shown in Fig 3-8.

3-92. To measure carrier level, first set the carrier frequency, as described above, and depress the **LEVEL** key. If the **AUTO** led is not illuminated, depress the **AUTO** key to resume measurement. The **FREQUENCY/LEVEL** display is now indicating carrier level. The units may be in dBm or millivolts. To change displayed units, depress the desired units key and then the **AUTO** key. The action of depressing a units key will override the automatic mode and hold the current level setting. Depressing the **AUTO** key will resume measurement.

3-93. The carrier **LEVEL** measurement can be calibrated by depressing the **CAL** key, with the carrier **LEVEL** function active. To calibrate the measurement, connect the **RF IN** connector to a signal with a known level, such as the optional 50 MHz power calibrator, and enter the level into the carrier **LEVEL** display.

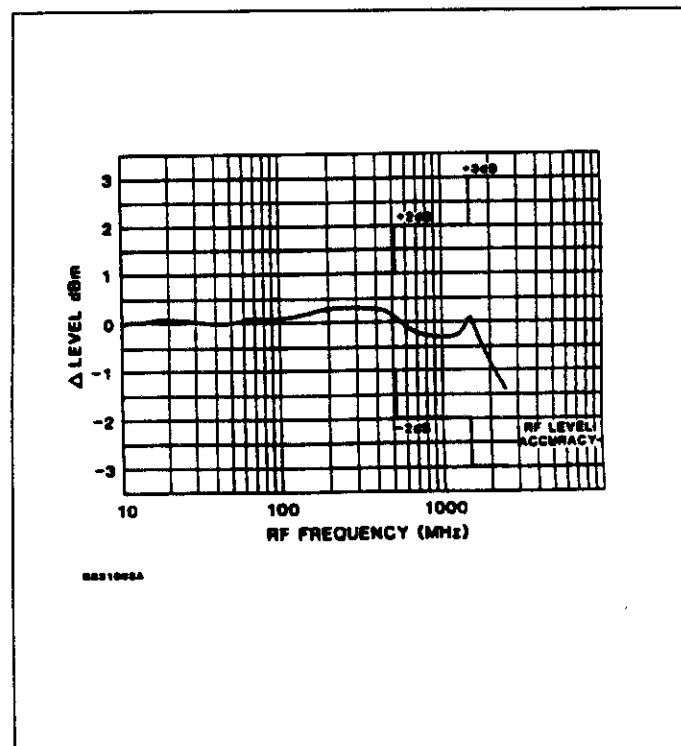


Figure 3-8 Typical Level Response

Depress the CAL key. The calibration routine will take about 3 seconds to complete. The resulting measurement will be the entered value, or an error will be displayed if the input signal is not within 2 dB of the entered value.

3-94. Carrier LEVEL can be set manually in order to eliminate acquisition time. To program carrier LEVEL, first depress the carrier LEVEL function key. For example, to enter -16.5 dBm, depress the [-], [1], [6], [.), and [5] keys, followed by the dBm units key. The FREQUENCY/LEVEL display will now contain -16.5 dBm. To convert the input level in dBm to an equivalent voltage across the 50 ohm input impedance of the sensor, depress the V/GHz or the mV/MHz keys. The resulting display will be in units of mV. In this example, the power level of -16.5 dBm will be converted to 33.45 mV. Depressing the dBm key will restore the -16.5 dBm indication. An input level may be entered in voltage units initially and displayed as a voltage level or a power ratio in dBm.

3-95. SELECTING MODULATION MODE.

3-96. The Model 8201 can detect and display amplitude, frequency, or phase modulation. After the modulation mode is selected, subsequent instrument operation is very similar.

3-97. To select the AM measurement mode, first select carrier frequency and level as described above, then depress the modulation AM key. The modulation display will indicate the recovered AM modulation in %. The IFHI and IFLO messages are active in the AM mode and indicate that the carrier level is not adequate to make a calibrated measurement. The [= =] display indicates that the current measurement is out of range to be displayed, and will occur when autoranging is in progress or the display is overranged.

3-98. To select the FM measurement mode, first select carrier frequency and level as described above, then depress the modulation FM key. The modulation display will now indicate the recovered FM in kHz. The de-emphasis filters may be selected in the FM measurement mode. In addition, they may be placed before or after the modulation display. See above for a description of this option. The de-emphasis filter keys are mutually exclusive, that is depressing one of the keys will cancel the others. Depress the desired de-emphasis key. The AF OUT signal, and optionally the modulation display, will now indicate modulation with the de-emphasis filter on. Depress the de-emphasis OFF key to cancel filter selection.

3-99. To select the PM measurement mode, first select carrier frequency and level as described above, then depress the modulation PM key. The modulation display will now indicate the recovered PM in RADians. The PM modulation mode is a special case of the FM mode. The modulation information is determined by integrating the output of the FM detector. This is mathematically consistent with the definition of frequency as the time rate of change of phase. The integration is only accurate over a selected range of frequencies so that accuracy specifications are relaxed and modulation bandwidth is decreased. Autoranging operation is also different in the PM measurement mode. The modulation range is determined by monitoring the recovered FM signal. This causes the displayed resolution to change based on phase deviation and modulation rate rather than just displayed deviation. For example, below 1 kHz modulation rate, autoranging points are the same as they are for FM, 5199 and 499 counts; however, at 5 kHz modulation rate the autoranging points are 1040 and 99 counts. The displayed resolution continues to decrease with increasing modulation rate.

3-100. MEASUREMENT AND DISPLAY CONTROL.

3-101. After the modulation mode has been selected, recovered modulation can be additionally processed by using the measurement control keys.

3-102. RATIO MEASUREMENTS.

3-103. The RATIO key is used to change displayed values from absolute to relative. RATIO can be displayed with respect to a previous measurement or a set value. The %/Hz, units, and dB/dBm keys in the data keypad toggle the relative display between linear (%), units, and logarithmic (dB).

3-104. If the RATIO key is depressed when the active function is in the measurement mode (LED in the AUTO key is illuminated), the current displayed reading becomes the reference for subsequent relative measurements. For example, if the current measurement is 25.00 kHz deviation and the RATIO key is depressed, and the % display is selected, the display will change to 100.0 and the units annunciators will be kHz and %. If the dB key is depressed the display will change to 0.00 and the annunciators will be kHz and dB. Note that if the active function is AM and the RATIO % display is selected, only the %

annunciator will be displayed.

3-105. In our example, if the deviation now changes to 20.00 kHz, the display will change to 80.0 % or -1.9 dB depending on the selection of the % or dB ratio. Modulation readings can also be displayed relative to a set value of modulation. The value of the reference modulation is keyed into the modulation display using the data keypad before the RATIO mode is activated. The LED in the AUTO key will go off when the data entry is completed. For example, to establish a reference modulation of 40.00% AM depth, select the AM function and cancel the RATIO display if it is active. Enter 40% into the modulation display using the data keypad. Depress the RATIO key to measure AM with respect to 40.00%. The dB key may be depressed to change the displayed units to dB. Suppose that the actual modulation was 47.5%. In our example, the modulation display would indicate either 118.7% or 1.5 dB.

3-106. The RATIO display is a convenient way to alter displayed units. For example, incidental AM is often expressed as a ratio in dB of indicated AM with respect to 100%. To display incidental AM, enter 100% as the reference modulation and select the dB RATIO measurement mode. Residual AM and FM and incidental FM may similarly be displayed with respect to a reference modulation. Carrier frequency will be displayed as MHz, or % frequency shift with respect to a measured, or set frequency.

3-107. Many other displays are possible by using the RATIO mode. Phase modulation may be displayed in degrees by entering 1.745 RAD as a reference and using the RATIO % measurement mode.

3-108. PEAK AND RMS DETECTORS.

3-109. When making modulation measurements, the desired result is normally the peak deviation or the peak or trough of amplitude modulation. The PEAK +, -, and \pm keys provide this display. The + PEAK detector indicates the positive peak excursion of FM or PM deviation (increasing frequency or phase), and the peak of AM modulation. The - PEAK detector indicates the negative peak excursion of FM or PM deviation (decreasing frequency or phase), and the trough of AM modulation. The \pm key indicates the arithmetic mean of the + and - peak key. The display in the PEAK \pm mode is calculated by the display program from independent measurements of the + and - peaks.

3-110. For most measurements there will be a difference in the positive and negative peaks. This is usually due to even order distortion of the recovered modulation signal. For FM modulation, the distortion would also be apparent in the carrier frequency display if the magnitude of the distortion is large enough. This asymmetry is also called carrier shift. For AM a similar effect occurs, shifting the average carrier amplitude.

3-111. In any case some difference in peak readings is normal since the maximum on-scale resolution of the modulation display can be 1 part in 5000, or 0.02%.

3-112. Several measurement situations arise when peak indication is not very useful. The most often encountered of these is the measurement of noise residuals. Because the Model 8201 detectors and local oscillators have very low noise residuals, the instrument can be used to characterize noisy sources. Under these conditions, the rms detectors should be used to give meaningful results.

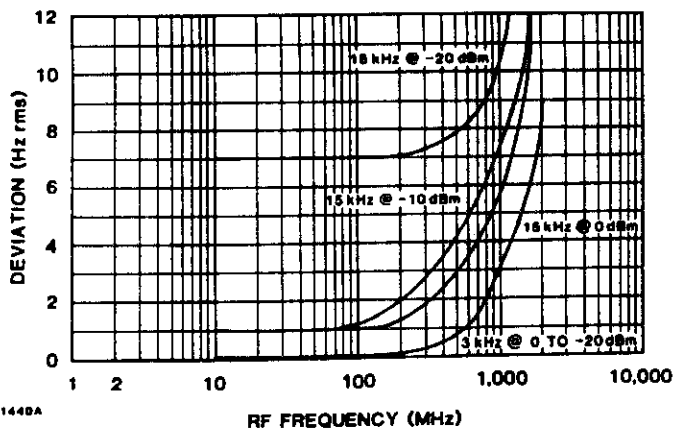
3-113. Two rms detectors are provided, RMS and $\sqrt{2}$ RMS. The detectors differ only mathematically. Selecting SPCL function 18 causes the RMS key to be redefined as $\sqrt{2}$ RMS. This causes the control program to scale the actual rms detector output by the square root of 2, the crest factor for a sinewave; thus, the display is calibrated in peak for sinewave modulation signals. This is very useful for quantifying noise residuals on moderately noisy carriers.

3-114. Root-mean-square (rms) voltage is obtained by summing the squares of the individual components of a waveform and then taking the square root of the result. Thermocouples, thermistors, and calorimeters are examples of rms detectors. The detector in the Model 8201 is a computing type of rms detector, that is, it takes the absolute value of the voltage, squares it, averages it, and finally takes the square root of the result.

3-115. When the measurement situation calls for display of residual modulation, the rms detector should be used. The noise of the carrier under test is combined with the residual noise of the Model 8201 circuits in very predictable manner. This allows the Model 8201 residuals to be easily discounted. For example, if the indicated residual FM is 25 Hz rms with a carrier at 1000 MHz and -10 dBm and with the 15 kHz low-pass filter selected, the residual noise of the carrier alone is simply the square root of the difference of the square of 25 and 7.5 or 23.8 Hz rms. Residual AM and PM are handled in a similar manner. The residual

Operation

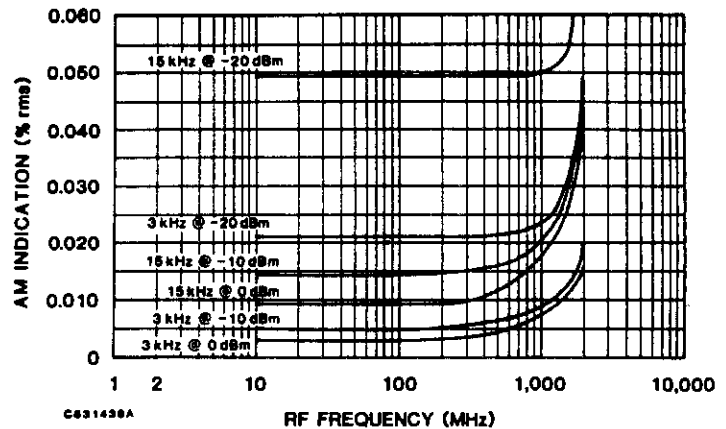
RESIDUAL f.m.
3 kHz & 15 kHz
LOW PASS FILTERS



CS31440A

FIGURE 3-9. Residual FM, 3 and 15 kHz Filters.

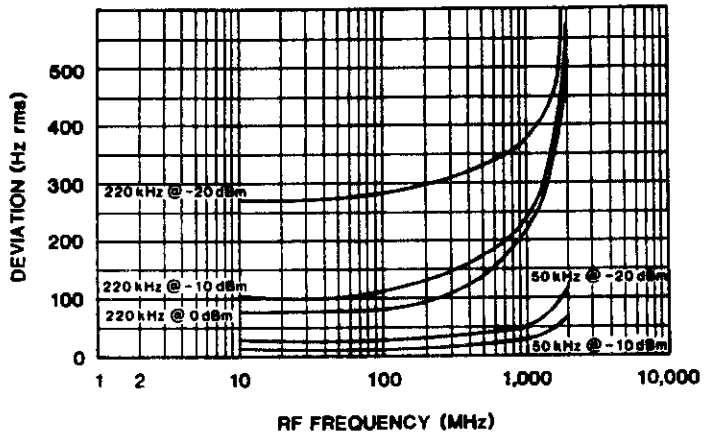
RESIDUAL a.m.
3 & 15 kHz
LOW-PASS



CS31438A

FIGURE 3-10. Residual AM, 3 and 15 kHz Filters.

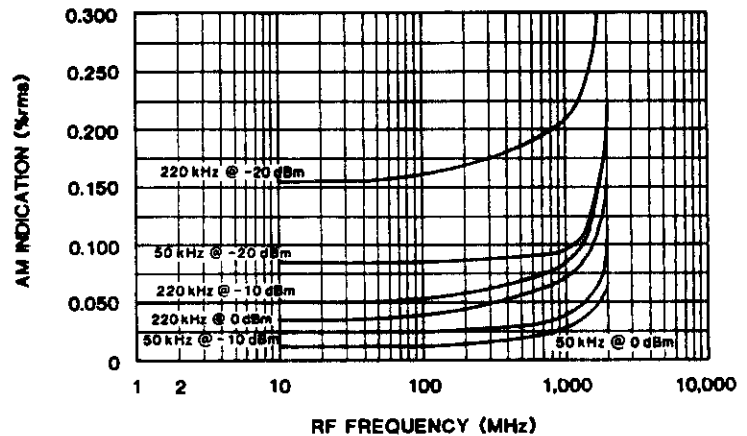
RESIDUAL f.m.
50 & 220 kHz
LOW PASS



CS31441A

FIGURE 3-11. Residual FM, 50 and 220 kHz Filters.

RESIDUAL a.m.
50 & 220 kHz
LOW-PASS



CS31439A

FIGURE 3-12. Residual AM, 50 and 220 kHz Filters.

responses of the Model 8201 are shown in Figures 3-9 through 3-12.

3-116. The QUASI-PEAK detector is included for measurements compatible with CCIR recommendation 468-3. This detector is most useful for measurements using the CCIR bandpass filter, however, it can be used for other measurements as well. Note that the detector indicates the peak value calibrated in rms.

3-117. DETECTOR HOLD.

3-118. The detector HOLD key is useful in measurement situations where the long term modulation peak is desired. The HOLD key can be used with any of the detectors to display the larger of the previous or current measurement. To use the HOLD function, depress the HOLD key. The modulation display will change only if the measurement is greater than the one displayed. Depress the HOLD key again to cancel this measurement control mode.

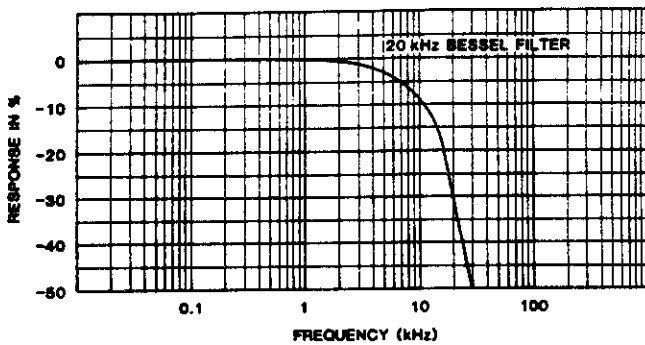
3-119. FILTERS.

3-120. The Model 8201 includes an array of low-pass, high-pass, and de-emphasis filters. These filters can be used to advantage to minimize measurement errors due to noise, or to remove unwanted components of complex modulation signals.

3-121. The high-pass filters are all three-pole Butterworth designs except the < 10 Hz filter. The < 10 Hz filter is a Gaussian response controlled by the coupling capacitors on the Filter circuit board. The three dB corner is much less than 10 Hz. This filter is also specified to have less than 10 % droop with 5 Hz square wave modulation. The response of the high-pass filters is shown in Figure 3-15.

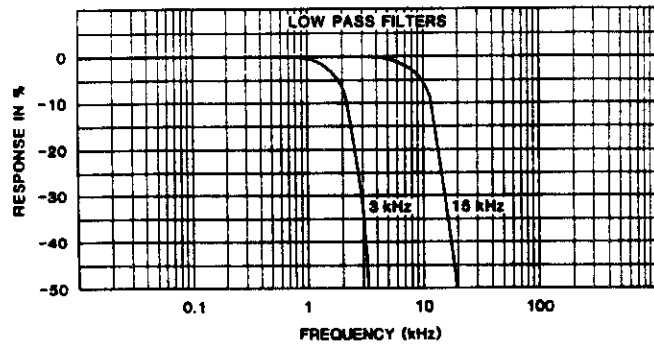
3-122. The low-pass filters are a combination of active and passive designs. The 3 and 15 kHz low-pass filters are three-pole Butterworth designs, the 20 kHz low-pass filter is a three-pole Bessel design, and the 50 and 220 kHz filters are seven-pole Butterworth designs. Low-pass filter response is shown in Figures 3-13, 3-14 and 3-16.

3-123. Filter selection is critical in maintaining accuracy of displayed modulation and distortion. All carriers applied to the RF IN connector of the Model 8201 will contain noise modulation sidebands. The magnitude of the noise can be determined by



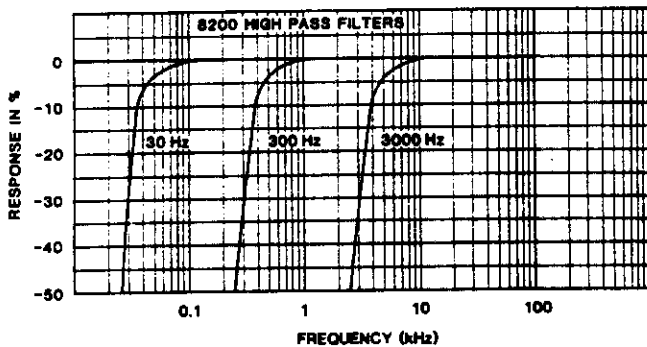
CS81442A

FIGURE 3-13. Response, 20 kHz Bessel Filter.



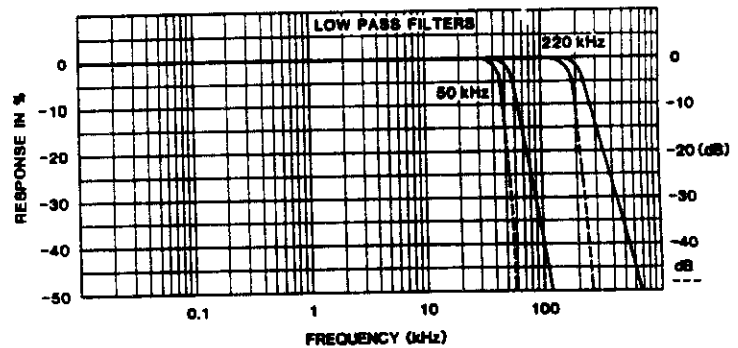
CS81443A

FIGURE 3-14. Response, 3 and 15 kHz Filters.



CS81444A

FIGURE 3-15. Response, High-pass Filters.



CS81445A

FIGURE 3-16. Response, 50 and 220 kHz Filters.

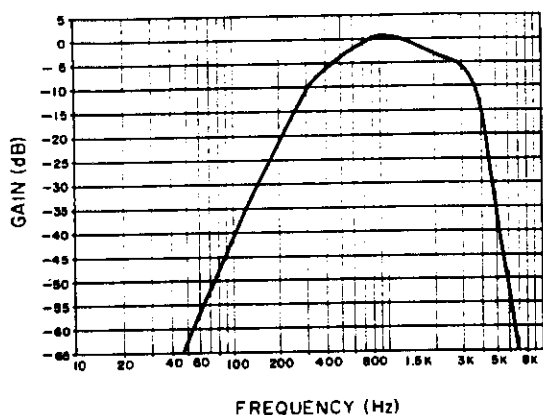
Operation

using rms detection as outlined above. Selection of the lowest low-pass filter possible based on the modulation frequency, will usually produce the most accurate indication. For example, if the modulation frequency is 1 kHz, the 3 kHz low-pass filter should be used.

3-124. If the modulation signal is a squarewave or pulse, the 20 kHz low-pass filter should be used. This filter is a Bessel design which has controlled phase characteristics and modest overshoot.

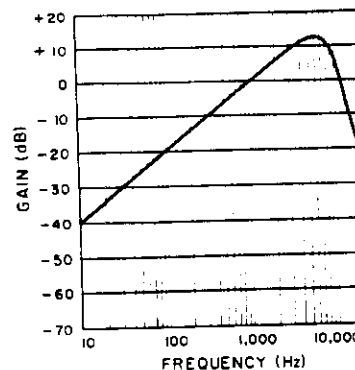
3-125. Filter selection is very important when measuring distortion. A reasonable distortion measurement should include at least the first three harmonics. For example, if a measurement of distortion is made at 2.5 kHz, the 15 kHz low-pass should be used. High-pass selection will also affect distortion measurements. For example, when measuring distortion at 1 kHz with the 300 Hz high-pass is selected, the phase relationship of the fundamental signal, 1 kHz, is changed with respect to the harmonics and a smaller or larger indicated distortion may result.

3-126. As an option, the Model 8201 can be configured with CCITT, CCIR, or C-MESSAGE bandpass filters. These filters are required by various specifying authorities to quantify noise residuals in voice grade telephone or radio-telephone systems. Any one, or all of these filters can be installed in the Model 8201. The responses of these filters are shown in Figures 3-17, 3-18, and 3-19.



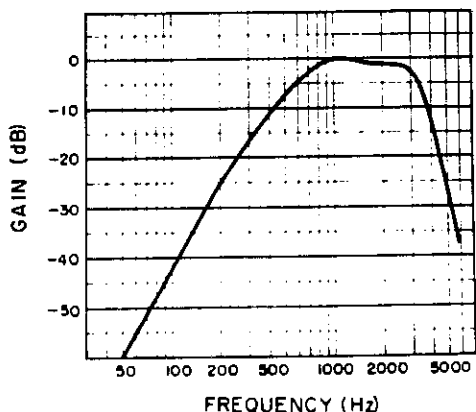
83162300A REV. A

FIGURE 3-17. Response, CCITT Bandpass Filter.



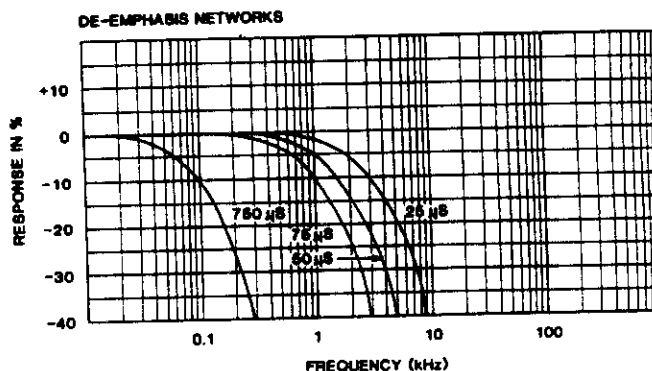
83162100A REV. A

FIGURE 3-18. Response, CCIR Bandpass Filter.



83162200A REV. A

FIGURE 3-19. Response, C-MESSAGE Bandpass Filter.



8316444A

FIGURE 3-20. Response, De-emphasis Filters.

3-127. For situations requiring proprietary or unusual filter shapes, a loop thru filter option can be installed. This option permits external circuitry to be placed between the AM and FM detectors and the baseband detectors. Any circuit or system capable of accepting a 1.0 volt peak-to-peak signal from a 600 ohm source, and able to drive 1 megohm in shunt with about 50 picofarads can be used. Both input and output circuits are protected against over-voltage and static discharge. The frequency response of the loop thru path extends from less than 10 Hz to greater than 220 kHz.

3-128. The de-emphasis filters were described above, The response of the de-emphasis filters is shown in Figure 3-20.

3-129. **AUDIO FREQUENCY AND DISTORTION.** After the modulation mode and measurement control functions have been determined, the recovered modulation can be further processed. The AUDIO display can be used to display audio frequency or distortion.

3-130. To measure audio frequency depress the **FREQ** key under the AUDIO display. The AUDIO display will indicate the frequency of the recovered modulation. Display resolution is determined automatically by the control program. For frequencies below 100 Hz, the resolution is 0.1 Hz, decreasing in decade steps to 100 Hz at 100 kHz modulation frequency.

3-131. The AUDIO display can also be used to display distortion. The internal audio distortion analyzer is automatically adjusted by the control program if the modulation frequency is between 20 Hz and 20 kHz. For frequencies outside this range, or during range changes, the [= =] symbol is displayed. The '----' symbol is displayed if the rms detectors are being used for modulation measurements.

3-132. To measure distortion in percent, depress the **DIST** key under the AUDIO display. The [= =] symbol will appear until the internal analyzer is tuned, and then the measured distortion will be displayed.

3-133. When the key marked **SINAD** is depressed, the distortion will be displayed in dB. SINAD is an acronym for Signal plus Noise and Distortion. The measurement made is the ratio of signal plus noise and distortion to noise and distortion expressed in decibels. The SINAD display has a higher resolution at low distortion readings because of the logarithmic display, however, it is normally used for adjusting receiver sensitivity at indications of about -12 dB. When the SINAD ratio is very low, the distortion analyzer can be tuned manually, by entering the audio frequency into the AUDIO display using the **DATA** keypad. The LED in the **AUTO** key will be out when audio frequency is set. Depressing the **AUTO** key will resume audio frequency measurement.

3-134. As indicated above, filter selection is very important when measuring distortion. Using a wider low-pass bandwidth than necessary will cause a higher distortion indication because of additional noise, and conversely, using a lower low-pass filter than necessary will cause a lower distortion indication because of attenuation of the harmonic components.

3-135. Some care should be taken when comparing Model 8201 distortion indications to those of instruments connected to the **AF OUT** connector. Most distortion analyzers use average rather than rms detection to indicate distortion. Average detectors read noise about 11 percent, or 1.1 dB lower than an rms detector. As a result, this type of instrument gives an optimistic indication when most of the residual signal is noise.

3-136. The **DIST OUT** connector on the rear panel of the Model 8201 can be used to assess the nature of the distorting signal. If the dominant component of the **DIST OUT** signal is noise, then the front panel indication is not representing harmonic distortion, but the residual noise.

3-137. PROGRAM STORE AND RECALL.

3-138. The Model 8201 contains an internal program memory which will hold 99 front panel setups. The programs represent the state of the instrument when the **STO** key is depressed. Storing and recalling program information is accomplished by depressing the **PRGM** key to activate the program function. Once the program function is active, the desired program number is entered into the display using the data keypad and the **ENTER** key. Depress the **STO** key to store the current instrument status or the **RCL** key to restore a previously saved instrument setting.

3-139. The internal memory of the Model 8201 is non-volatile, that is, when power is removed, the contents of the internal memory are not lost. In normal operation, the internal memory is never erased. New programs or changes are simply written

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over the old ones. It is possible, however, to erase the entire program memory by use of test jumpers A9JP1 and A9JP2. See section VI. Erased programs cannot be recalled. After recalling a program, any panel setting may be changed.

3-140. RECALL ONLY PROGRAM.

3-141. Program number 99 is a setup program equivalent to the program installed when the INIT key is depressed. This program is installed during power up if a memory fault occurred on the previous power down. If an attempt is made to store a program at location 99, an error will result.

3-142. REMOTE OPERATION.

3-143. Any front panel operation of the instrument except for the LINE ON/OFF switch can be remotely controlled under direction of an IEEE-488 interface controller. IEEE-488 is a hardware standard which describes the communication and handshaking across an 8-bit parallel bus between a controller and up to 15 instruments.

3-144. Setting the Bus Address. To set the IEEE-488 bus address (MLTA), depress the SPCL key, and enter 17, the special function to set the bus address. The current bus address will be displayed, with the ADRS annunciator illuminated in the SPCL/PRGM display. Select the desired address with the data keypad. The address may be any decimal number from 0 to 30, inclusive. A secondary address is not implemented. The bus address function will remain active until the SPCL function is changed or the PRGM key is depressed.

3-145. Setting the End-of-String Character. To set the IEEE-488 bus end of string character(s), depress the SPCL key, and enter 15, the special function to access the end-of-string setting program. The current end-of-string character(s) will be displayed, in the FREQUENCY/LEVEL display. Select the desired characters by using the DEL and CLR (arrow) keys to step through the possible selections. Selection is automatic. The different character displays and their meanings are tabulated in Table 3-3. In any case, the Model 8201 always terminates on end-or-identify (EOI) true and always sends EOI true with the last character of every string. The display is cleared when another function key or ENTER is depressed.

DISPLAY	LISTEN	TALK
CL-CL	Line Feed.	Carriage Return, Line Feed.
C-CL	Carriage Return.	Carriage Return, Line Feed.
C-C	Carriage Return.	Carriage Return.
L-L	Line Feed.	Line Feed.
EOI	End-or-identify.	End-or-identify.

TABLE 3-3. IEEE-488 End-of-String Characters.

3-146. Entering the Remote Mode. The instrument is put in the remote mode by addressing it as a listener with remote enable (REN) bus signal true. In the remote state the keyboard is disabled, except for the LCL/INIT key and the POWER ON/OFF switch. The REM status annunciator is illuminated.

3-147. Returning to Local Mode. The instrument may be returned to the local mode as follows:

- The LCL/INIT key is depressed, provided local lockout (LLO) is not active.
- The go-to-local (GTL) bus command is sent.
- Remote enable (REN) is set false.

NOTE

The instrument must be placed in the remote mode for it to store and respond to data messages.

3-148. Triggered Operation. In the remote mode the instrument can be operated in the immediate mode (mnemonic IM), or in the wait-for-trigger mode (WT). The immediate mode is the default condition and results in the immediate response to talk requests. The wait-for-trigger mode causes data acquisition be deferred until a trigger is received. This aids in synchronizing the instrument to other system components. The wait-for-trigger mode is set when the WT mnemonic is encountered in the input string. From that point on execution is delayed. No change will occur until one of the following events is encountered:

- "Group-execute-trigger" (GET) is received.
- The mnemonic TR (trigger) is interpreted.
- Any mnemonic following IM (immediate) is interpreted.

NOTE

Event (c), above, go-to-local, or unlock terminates the wait-for-trigger mode and restores the immediate mode. The wait-for-trigger mode is not active in local operation.

3-149. Talk Operation. The instrument may be addressed as a talker without regard for remote/local mode. When the talker state is set by the bus controller, the instrument sends a character string which is determined by the current talk mode. One of four different talk modes is selected by sending the appropriate mnemonic with the Model 8201 addressed as a listener. The selected mode will remain in effect until changed.

Function/Status	Binary Word	ASCII string			
		0	C	A	4
Manual Tuning Set	0				
Manual Level Set	0				
Manual Range Set	0				
Alternate Filter Set	0				
Unlocked	1				
Unleveled	1				
Manual audio tuning	0				
Audio Display overrange	0				
Active Displays					
Distortion	1				
Sinad	0				
Carrier Level	1				
Carrier Frequency	0				
PM	0				
FM	1				
AM	0				
Audio Frequency	0				

TABLE 3-4. Hardware Status, Bit assignments.

Operation

3-150. Talk Status (TS) Mode. If an error is pending, the error code will be returned, otherwise a zero is returned. The TS mode will automatically clear an error after the status is reported. Talk Status (TS) is the default talk mode after initialization of the instrument.

3-151. Talk Function (TF) Mode. The TF mode returns a four character string, in HEX notation, representing the state of the hardware and display functions. The bit assignments are arranged to allow for string or byte oriented decoding. The bit assignments and meanings are presented in Table 3-4.

3-152. Talk Value (TV) Mode. In the TV mode the argument of the active function is returned. All values returned are in basic units such as: Hz, dB, dBm, % etc. FM deviation is returned in kHz, and carrier level in millivolts.

3-153. Talk Program (TP) Mode. In the TP mode a six digit number is returned that uniquely identifies the instrument firmware.

3-154. Identify (ID) Mode. In the ID mode a string containing the instrument identification and serial number is returned. A typical response is:

"Boonton Model 8201, SN: 999, April 12,1991"

which includes the model number, the serial number, and the firmware date.

3-155. Using "Service Request" (SRQ). The Service Request allows the Model 8201 to inform the system controller that some special event has occurred. The instrument then expects the controller to perform a serial poll to find out what event has occurred. The events that can be selected to generate service requests are instrument error, measurement is ready, and calibration is completed. Each of these options can be individually enabled or disabled with the SRQ mask. The default settings for the mask are with all SRQ's disabled. They can only be enabled by setting the appropriate bits high in the SRQ mask over the bus followed by the SQ mnemonic or manually using SPCL function 16. In small systems only one instrument may be capable of using SRQ. In this situation there is no need to execute a serial poll since the nature of the request is known. Error codes may be obtained directly from the talk error (TS) mode. The SRQ line can then be cleared by sending the clear (CL) command.

3-156. Setting the SRQ mask. Table 3-5 indicates the bit positions in the SRQ mask, what each bit enables/disables, and the corresponding bus configuration command. Note that the numeric argument precedes the SQ mnemonic.

Bit Position	Function	Bus Code
0	Instrument Error	1 SQ
1	Calibration Completed	2 SQ
2	Measurement Completed	4 SQ
3	Reserved for future use.	8 SQ
4	Reserved for future use.	16 SQ
5	Reserved for future use.	32 SQ
6	Reserved for future use.	64 SQ
7	Reserved for future use.	128 SQ

More than one item can be selected by adding the corresponding bit positions.

TABLE 3-5. Bus Command Responses.

3-157. Bus Command Responses. IEEE-488 bus commands are sent by the controller to all devices on the bus (Universal Command Group) or to addressed devices only (Addressed Command Group). The response of the instrument is listed in Table 3-6. All unlisted commands are ignored.

3-158. Program Function Mnemonics. Each front panel key is assigned a program mnemonic. Programming the mnemonic, followed by unit values, if appropriate, is analogous to manual front panel operation. In addition, other program mnemonics are used for functions that are applicable only in remote operation. Table 3-7 lists the program function mnemonics.

COMMANDS	RESPONSE
Universal Command Group: Device Clear (DCL) Local Lockout (LLO) Serial Poll Enable (SPE) Serial Poll Disable (SPD)	Clear errors. Disable LCL/INIT key. Set Talk mode for poll response. Disable serial poll response..
Addressed Command Group: Selected Device Clear (SDC) Go to Local (GTL) Group Execute Trigger (GET)	Same as device clear. Returns front panel control. Trigger a measurement.

TABLE 3-6. Bus Command Responses.

3-159. Number Formatting. Number formatting rules are as follows:

- Fixed or floating formats are accepted.
- The optional + or - sign may precede the mantissa or the exponent.
- The optional radix point may appear at any position within the mantissa. A radix point in the exponent is ignored.
- The optional "E" for exponent may be upper or lower case.
- All ASCII characters having hexadecimal values of 0 to 23, and 25 to 2B are ignored.

3-160. Data String Format. Data string formats are as follows:

- The programming sequence is in natural order, that is, a function mnemonic is sent first followed by the argument, if appropriate.
- All ASCII characters having hexadecimal values of 0 to 23, and 25 to 2B are ignored. The ASCII (\$), hexadecimal 24, is reserved. Lower case letters are automatically converted to upper case.
- A primary function mnemonic sent without a following argument will make the specified function active.
- The data string may not exceed 256 characters and may be terminated with LF, CR, or EOI, depending on the end-of-string setting.
- Interpretation of the data string does not begin until the end-of-string character is received.
- If units are unspecified for any argument, default units are automatically appended.

3-161. Data String Errors. Errors are detected during interpretation. The occurrence of an error will display the error code if the display is enabled, and will set SRQ true, if enabled. The error and SRQ can be cleared by a status request (TS), or a clear error function (CL). All errors cause existing valid parameters to be restored. No new input can be processed until a pending error is cleared.

Operation

3-162. Data String Examples. The following are examples of typical programming strings in HP BASIC:

- OUTPUT 715; "SP 25" set SPCL function to 25 and execute it.
- OUTPUT 715; "H2L2" set high-pass to 30 Hz, and low-pass to 15 kHz.
- OUTPUT 715; "RD" select ratio, dB display for the active function.
- OUTPUT 715; "2 SQ" enable SRQ on calibration complete.
- OUTPUT 715; "FMTV" set measurement to FM, and talk mode to talk value.
- OUTPUT 715; "AM CA" set measurement to AM, and calibrate AM detector.
- OUTPUT 715; "A2 TS" set alternate filter 2 (CCIR), and talk mode to talk status.

3-163. Reading Back Calibration Values. Calibration data is normally transient. It exists only during the calibration process. There are occasions, however, when this data is required. In order to capture this data, the instrument should be programmed to the wait-for-trigger (WT) mode. Select the appropriate function and send the TV and CA mnemonics to activate calibration with the talk value mode selected. When calibration completes, the value read back is the calibration data.

- OUTPUT 715; "FMTV" set measurement to FM, and talk mode to talk value.
- OUTPUT 715; "WT CA" set trigger mode to wait-for-trigger, and calibrate FM detector.
- ENTER 715; AS read back calibration data.
- OUTPUT 715; "IM" restore immediate trigger mode.

TABLE 3-7. IEEE-488 BUS MNEMONICS.

BUS MNEMONIC	RESPONSE
Function Control: FR RL SI AF DN AM FM PM SP PG	Carrier frequency, argument range: 100 kHz to 2.5 GHz. Carrier level, argument range: -47 to +30 dBm.(1 mV to 7 V) SINAD, no argument allowed. Audio Frequency, argument range: 10 Hz to 20 kHz. Distortion, no argument allowed. AM modulation, argument range: 0 to 100%. FM modulation, argument range: 0 to 500 kHz. PM modulation, argument range: 0 to 500 RAD. Special Function, argument range 0 to 99. Program number, argument range 0 to 99.
Number Termination: DB GH MH KH HZ VO MV RA	dB for ratio, or dBm for level. Gigahertz for frequency entry. Megahertz for frequency entry. Kilohertz for frequency entry. Hertz for frequency entry. Volts for level entry. Millivolts for level entry. Radians for phase modulation entry.
Display Control: AU RP RD RX WT IM TR BL UD	Activates the measurement mode, for the active function. Not active in SPCL or PRGM. Activate relative measurements of the active modulation function in percent. Activate relative measurements of the active modulation function in dB. Turn OFF ratio mode. Enable the wait-for-trigger talk mode. Enable the immediate trigger talk mode. Trigger a measurement, same as GET. Blank Display and disable display updates. Restore display and enable display updates.
Filter Selections: D1 D2 D3 D4 D5	De-emphasis, 25 us. De-emphasis, 50 us. De-emphasis, 75 us. De-emphasis, 750 us. De-emphasis, OFF.

TABLE 3-6. IEEE-488 BUS MNEMONICS CONTINUED.

BUS MNEMONIC	RESPONSE
<p>H1 H2 H3 H4</p>	<p>High-pass, < 10 Hz. High-pass, 30 Hz High-pass, 300 Hz. High-pass, 3000 Hz.</p>
<p>A1 A2 A3 A4</p>	<p>Optional THRU filter. Optional CCIR filter. Optional CCITT filter. Optional C-MSG filter.</p>
<p>L1 L2 L3 L4 L5</p>	<p>Low-pass, 3 kHz. Low-pass, 15 kHz. Low-pass, 20 kHz. Low-pass, 50 kHz. Low-pass, 220 kHz.</p>
<p>Detector Selection:</p>	
<p>P1 P2 P3 QP RM PR PH PX</p>	<p>Peak +. Peak ±. Peak -. Quasi-peak detector. RMS detector. √2RMS detector. Peak Hold ON. Peak Hold OFF.</p>
<p>Program Control:</p>	
<p>ST RE</p>	<p>Store front panel setup. Recall front panel setup.</p>
<p>Test Function:</p>	
<p>CH</p>	<p>Execute self-check program.</p>
<p>Cancel Errors:</p>	
<p>CL</p>	<p>Clear all errors.</p>
<p>Talk modes:</p>	
<p>TV TL</p>	<p>Talk value, sends the value of the active function. Talk program, sends a string representing the contents of the stored program followed by an ASCII \$.</p>
<p>TS</p>	<p>Talk status, sends the current error number.</p>
<p>TP</p>	<p>Sends a string which identifies the 8201 firmware.</p>
<p>TF</p>	<p>Talk function, sends a string representing the current hardware status.</p>
<p>ID</p>	<p>Sends a string which identifies the 8201.</p>

TABLE 3-6. IEEE-488 BUS MNEMONICS CONTINUED.

BUS MNEMONIC	RESPONSE
<p>Special Control codes: R0 or SP 1 R1 or SP 2 R2 or SP 3 R3 or SP 4 PD or SP 7 AD or SP 8 CA SQ EI DI</p>	<p>Set modulation range to auto. (same as SP 1) Set modulation range 1, 0.000 to 5.000. (same as SP 2) Set modulation range 2, 5.00 to 50.00. (same as SP 3) Set modulation range 3, 50.0 to 500.0. (same as SP 4) Force de-emphasis mode to pre-display. Force de-emphasis mode to post-display. Calibrate the active function. Set SRQ mask, argument range 0 to 7. See text. Enable SRQ interrupts. (8200 compatible) Disable SRQ interrupts. (8200 compatible)</p>

TABLE 3-8. INSTRUMENT ERROR CODES.

ERROR NUMBER		MEANING
Operation: 01 (01) 02 (05) 03 (03) 04 (06) 05 (12) 06 (21) 07 (07) 08 (10) 09 (11) 10 (15) 11 (50) 12 (51) 13 (13) 14 (22) 15 (14) 16 (16) 17 (17) 18 (18)		Carrier Frequency entry out of range. Carrier Level entry out of range. Audio Frequency entry out of range. AM modulation entry out of range. FM modulation entry out of range. PM modulation entry out of range. SPCL function entry out of range. PRGM entry out of range. Units do not match active function. Too many characters entered into display. SPCL function requires A9J1 installed. SPCL function not active. Requested Program is empty. Program is recall only. IEEE-488 bus address out of range. IEEE-488, non-existent mnemonic. IEEE-488 data string format error. IEEE-488, input text buffer overflow.
Calibration: 20 (40) 21 (42) 22 (43) 23 (41) 24 (24) 25 (25) 26 (44) 27 (27) 28 (28)		AM calibration fault. FM calibration fault. PM calibration fault. RMS detector calibration fault. Average detector calibration fault. Quasi-peak detector calibration fault. Carrier Level calibration fault. < 10 Hz filter calibration fault. 220 kHz filter calibration fault.
Hardware: 30 (30) 31 (31) 32 (32) 33 (33) 34 (36) 35 (52) 36 (53) 37 (37) 38 (38) 39 (39)		Oscillator setup error band 1. Oscillator setup error band 2. Oscillator setup error band 3. Oscillator setup error band 4 Frequency Counter self-check error. Memory error, ROM. Memory error, RAM. Memory error, EEPROM GPIB interface fault. Instrument interface fault.
NOTE:		Numbers in () indicate value returned in 8200 error mode.

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SECTION IV THEORY OF OPERATION

4-1. INTRODUCTION.

4-2. The Model 8201 is a versatile, solid-state, microprocessor controlled, modulation analyzer that covers the carrier frequency range of 100 kHz to 2.5 GHz. Recovered modulation is displayed on a four digit LED display, which provides a maximum resolution of 1 Hz deviation, or 0.001 % AM. Operating modes, input frequency, input level, and reference levels can be keyed in through a front panel keyboard. An IEEE-488 interface enables remote programming of the instrument. Selected modes and values are displayed on an alphanumeric display and LED indicators. Input commands are processed by the internal microprocessor, and control signals developed by the microprocessor set up the internal circuits in accordance with the commands. The use of a microprocessor also enables storage of up to 99 complete sets of instrument setup data. Commonly used setups can be stored in non-volatile memory either through the keyboard or via the IEEE-488 interface; thereafter, the instrument front panel settings can be restored by keying in the program number assigned to the desired setup and depressing the RCL key or sending the RE mnemonic on the bus.

4-3. FUNCTIONAL BLOCK DIAGRAM (Figure 4-1).

4-4. Control of instrument operation is exercised by a microprocessor that executes a fixed program in read-only-memory (ROM). Timing of microprocessor operations is controlled by a 18.432 MHz clock. A random-access-memory (RAM) provides storage capability for microprocessor data. To insure retention of data in storage, the non-volatile RAM is powered continuously from an internal 3-volt lithium battery.

4-5. The microprocessor communicates with the internal circuits through a data bus, an address bus, and an I/O printed circuit board. Command information is entered into the microprocessor through the front panel keyboard or an IEEE-488 interface. Special functions are provided for option selection and test purposes. Input data selection is displayed by means of a digital readout and LED indicators. The microprocessor stores and processes input data, and generates data and address information to cause execution of commanded functions.

4-6. The carrier signal is first frequency translated to an intermediate frequency for processing. The intermediate frequency chosen is dependent on carrier frequency. Carriers above 10 MHz are converted to 1.211 MHz, carriers from 2 MHz to 10 MHz are converted to 346 kHz, and carriers below 2 MHz are not converted at all. Frequency translation is accomplished by means of a zero-order hold sampler. The sampler is fully bootstrapped to accept signals as high as 2 Volts rms, without overload.

4-7. A sampling impulse, generated from a tunable local oscillator, converts the RF signal to the appropriate IF signal. After filtering and buffering, the IF signal is processed by the AM and FM circuits. Additionally, the IF signal is processed by the tuning circuits to provide signals to the microprocessor to properly tune the local oscillator.

4-8. The frequency modulation information is recovered by first amplitude limiting the IF signal to remove any AM information, and 'pulse-counting' the resulting signal to determine instantaneous frequency. A direct coupled output of the discriminator is connected to the FM OUT connector on the rear panel.

4-9. The amplitude modulation information is recovered by first setting the gain of the measurement channel to a convenient level for accurate measurement. The resulting signal is amplitude detected by a linear-active detector circuit. A direct coupled output of the detector is connected to the AM OUT connector on the rear panel.

4-10. The phase modulation information is recovered in the audio filter section by integrating the recovered FM signal.

4-11. The recovered audio signal from the AM or FM detectors is further processed by amplification and selectable filtering before being converted to dc for measurement. Audio detection consists of precision peak detectors, a quasi-peak detector, and a true rms detector. The dc information from the audio detectors is digitized by a 13-bit A/D converter for digital processing

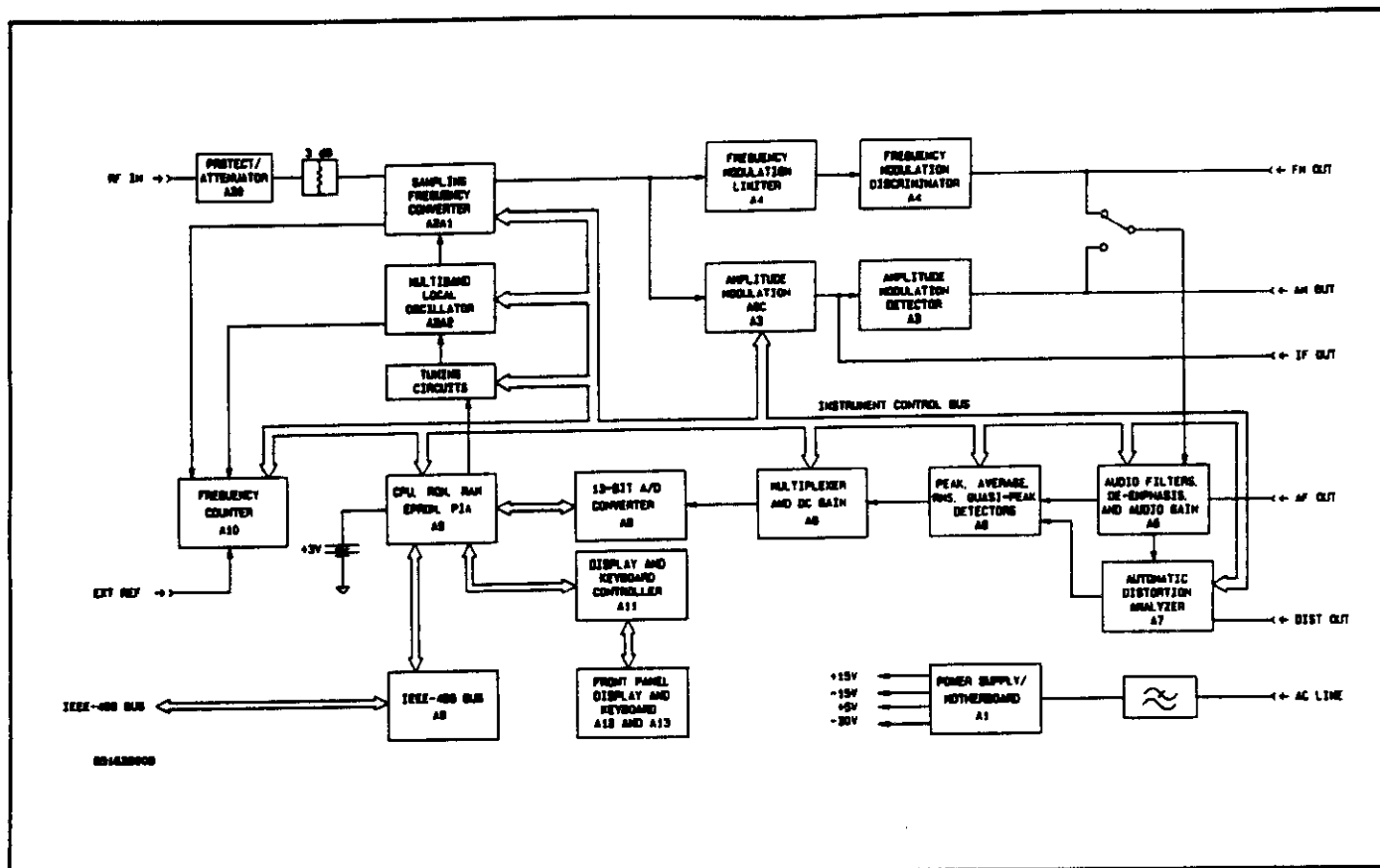


FIGURE 4-1. Functional Block Diagram.

and display.

4-12. The audio signal is also processed by a fully automatic distortion analyzer. This analyzer operates in conjunction with the control program to provide continuous readout of the recovered audio distortion for baseband frequencies from 20 Hz to 20 kHz.

4-13. Internal calibration circuits are operated by control program as required to establish calibration of the internal AM, FM, PM, quasi-peak, and rms detectors.

4-14. Counter/timebase circuits establish the clocks and reference frequencies for operation of the frequency counter and calibrator.

4-15. Power supply circuits convert the incoming line voltage into regulated dc operating voltages to power the instrument circuitry.

4-16. THEORY OF OPERATION, RF CIRCUITS.

4-17. The RF circuits convert the carrier input signal into a suitable IF signal for AM, FM, and PM measurements. See Figures 4-2 and 8-7.

4-18. The carrier to be measured is applied to the front panel RF IN connector. The signal passes through overload protection module A30, and is attenuated by AT1, a 3 dB pad, before it appears at sampling gate CR2. The attenuator provides some isolation and protection for the sampling circuit. The protection module includes a switchable 20 dB pad which is activated for input levels above +20 dBm.

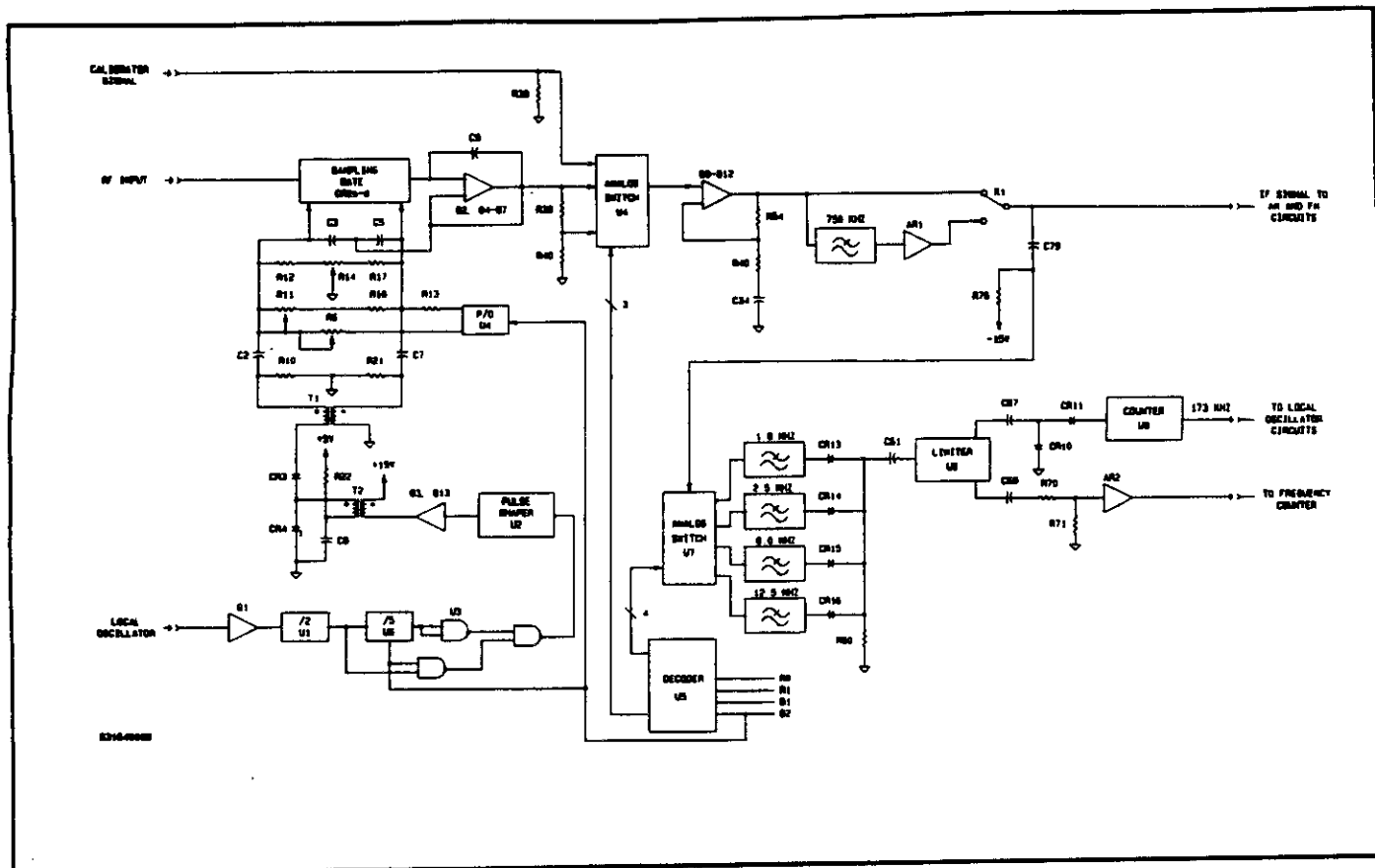


FIGURE 4-2. RF Circuits Block Diagram.

4-19. Simultaneously, a local oscillator signal is buffered by transistor Q1 and associated components and divided by two in U1. The resulting TTL signal is passed directly, or divided by 5 in U6, to a pulse forming circuit U2. Switching is accomplished by U3, and band control line B2. The instrument control program operates the band switch to select the proper operating band based on the RF frequency.

4-20. The pulse signal from U2 is further shaped and amplified by Q3 and Q13 to drive step-recovery diode CR4, through transformer T2. Initially CR4 is forward biased from the +5 volt supply through R22. The pulse signal from Q3 and Q13 drives CR4 into reverse conduction; however, CR4 does not "open" until all of its stored charge is depleted. At that instant the diode recovers and produces a large narrow pulse, which is coupled to the sampling bridge by T1, a balun transformer. The output of T1 is two nearly equal opposite polarity pulses. If the two pulses were exactly equal, they would exactly cancel at the input and output of the bridge. Since such equality is never the case, however, R14 is required to balance the bridge on the various operating bands.

4-21. R6 is adjusted when the local oscillator signal is between 2 and 4 MHz for optimum sampler efficiency. R11 is adjusted when the local oscillator signal is between 10 and 20 MHz.

4-22. The operation of the sampling gate is shown in simplified form in Figure 4-3. Each time the sampling gate is closed, by a short-duration pulse, the input capacitance of the sampler amplifier plus any stray capacitance is charged to a voltage that is less than the instantaneous RF input voltage. Before the next sample is taken, positive feedback from the sampler amplifier causes additional charge to be placed on this capacitance. Charge is added until the voltage at the output of the sampling amplifier is exactly equal to the RF input when the sample was taken. This output is held constant until the next sample is taken. Successive samples are taken until the RF waveform is reconstructed at 1.211 MHz or 346 kHz, depending on the RF frequency. Additional feedback from the sampler amplifier maintains symmetrical reverse bias on the sampling gate.

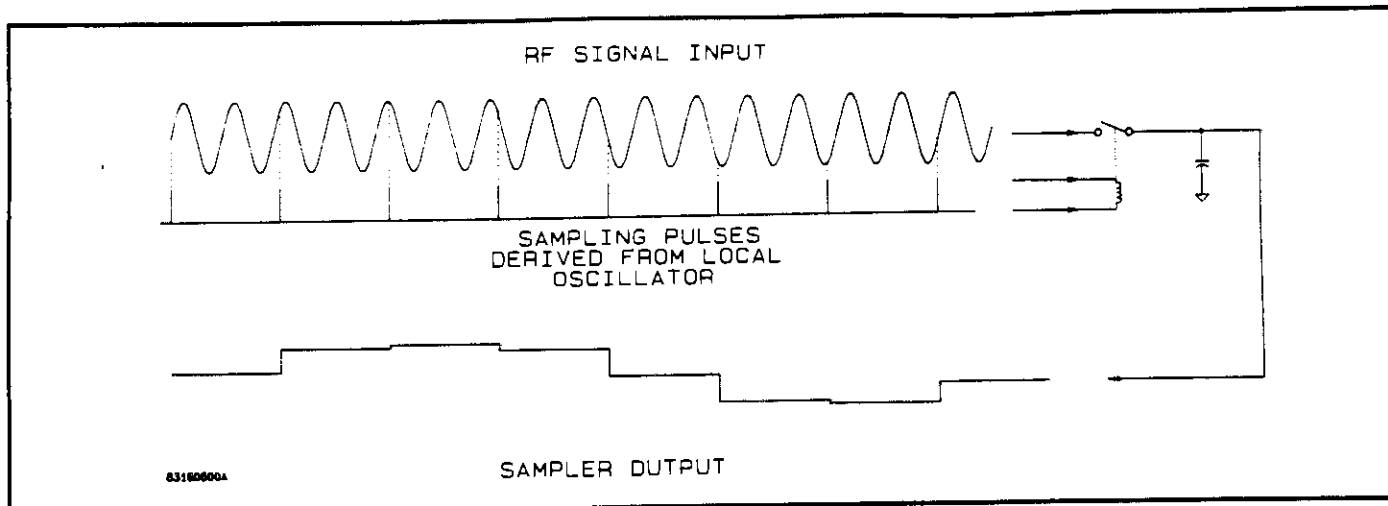


FIGURE 4-3. Sampling Gate Operation.

4-23. When the carrier frequency is between 100 kHz and 2 MHz, the 1.211 MHz IF is selected and the local oscillator is set to about 18 MHz. Under these conditions, the input signal passes through the sampling bridge without conversion. The IF circuits then process the signal directly.

4-24. The sampler amplifier is composed of transistors Q2 and Q4-Q7 and associated components. The gain is fixed at less than one by a direct feedback connection. The stage has a low output impedance required to properly bootstrap the sampling bridge.

4-25. The output of the sampling amplifier is connected to a switched 10 times attenuator consisting of R39 and R40. Analog switch U4 is operated by the control program, via data decoder U5, to select the signal, the signal divided by 10, or the calibrator signal. The calibrator is connected to the IF circuits when the calibration program is operating, otherwise the attenuator outputs are selected. If the carrier level is greater than about 100 millivolts, the signal is attenuated 10 times.

4-26. An amplifier consisting of transistors Q8-Q12 and associated components is required to amplify and buffer the IF signal. This stage has a gain of about 3.3, as determined by R54 and R46. When the 1.211 MHz IF is selected, relay K1 is operated to select the output of this stage. If the 346 kHz IF is being used, the signal is filtered by a 750 kHz low-pass filter consisting of L12, L14, C58, C62, and C64. Amplifier AR1 has a gain of two which compensates for the insertion loss of the filter. The output of AR1 then becomes the IF signal.

4-27. This signal is connected to the AM and FM boards for further processing, and to analog switch U7. U7 is operated by the control program, via data decoder U5, to select one of four low-pass filters. The filters, consisting of L2-L9, C38-C41, C46-49, and C51-54, are designed to reject the local oscillator signal and maintain a bandwidth of at least one-half of the sampling rate.

4-28. At any sampling frequency the carrier signal will be converted to a frequency between dc and one-half the sampling rate. Therefore, to insure proper signal discrimination, the filters must have a bandwidth of at least one-half of the sampling rate. The filter bandwidths are 1.8, 2.5, 8, and 12.5 MHz.

4-29. Diodes CR13-CR16 isolate the individual filters at the input of limiter U8. Diode bias is provided by R76 through U7. U8 limits the IF signal to remove any AM and generates square wave outputs to drive U9, a TTL counter, and AR2, a buffer amplifier used to provide a sample of the IF signal for the frequency counter circuits.

4-30. The counter output signal is used to measure the IF signal frequency for tuning and RF frequency calculation.

4-31. Counter circuit U9 is programmed to divide by 2 or by 7 as determined by the state of control line B2. If B2 is a TTL high, the 10 to 20 MHz local oscillator is active and U9 is set to divide by 7. This converts the 1.211 MHz IF to 173 kHz. If B2 is a TTL low, the 2 to 4 MHz local oscillator is active and U9 is set to divide by 2. This converts the 346 kHz IF to 173 kHz. The 173 kHz signal is connected to the local oscillator circuits for further processing.

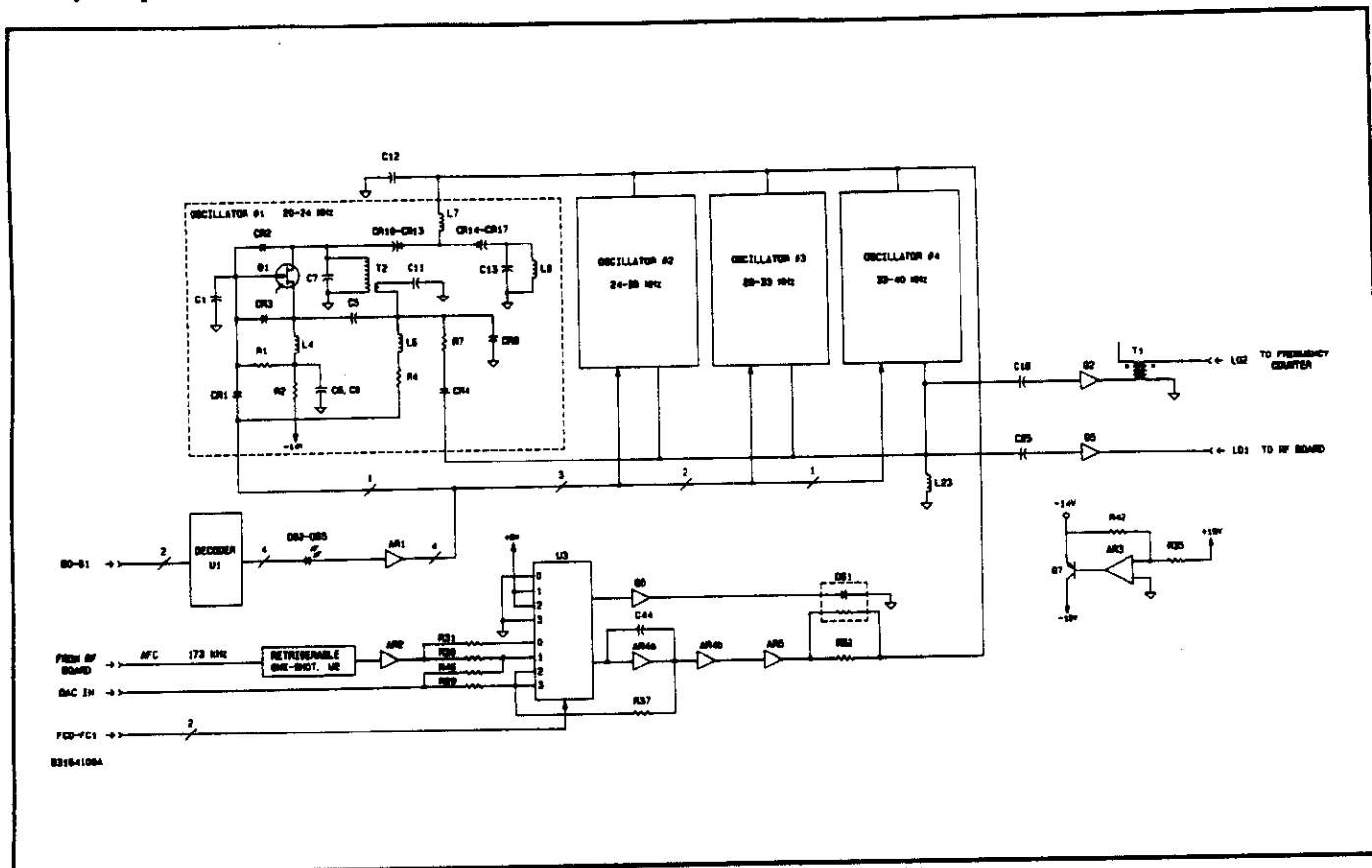


FIGURE 4-4. Local Oscillator Circuits Block Diagram.

4-32. THEORY OF OPERATION, OSCILLATOR CIRCUITS.

4-33. The local oscillator circuits provide the signals to operate the pulse generator circuits on the RF board. See Figures 4-5 and 8-9.

4-34. Four oscillators are operated individually to cover the band of frequencies from 20 to 40 MHz. The oscillators are designed and constructed to produce minimum residual FM. Since all oscillators function the same way, only one will be discussed in detail.

4-35. The lowest band is covered by an oscillator composed of Q1 and associated components. Transistor Q1 provides the gain required to sustain oscillations, while transformer T2 and capacitors C7 and C13 along with varactor diodes CR10-17 form the tuned circuit. Feedback is taken from the secondary winding of T2 and connected to the source of Q1 through dc blocking capacitor C5. Diodes CR2 and CR3 provide output voltage amplitude control by rectifying the feedback and drain voltages and reverse biasing Q1, thus limiting stage operating current. Capacitor C1 bypasses the gate of Q1 at the frequency of oscillation. Resistor R1 is required to establish initial gate bias and inductor L4 provides a dc return for the source.

4-36. The output of the oscillator is connected through isolation resistor R7 and switching diode CR4 to buffer stages Q2 and Q5.

4-37. Band switching is accomplished by the control program via data decoder U1 and level shifter AR1. U1 is a one-of-four decoder which converts data lines B0 and B1 into individual select lines for the four oscillators. Diodes DS2 through DS5, and pull-up resistor array R54 couple the four TTL lines to level shifter AR1. The outputs of AR1 swing from about +13 to -13 volts.

Section 4

4-38. When a band is selected, the LED associated with that band will be illuminated and the corresponding AR1 output will be at +13 volts. With +13 volts at the junction of CR1 and R4, CR1 becomes reverse biased, as does CR9. CR4 is forward biased, thus connecting the output of the selected oscillator to buffers Q2 and Q5.

4-39. When a band is not selected, the LED associated with that band will not be illuminated and the corresponding AR1 output will be at -13 volts. With -13 volts at the junction of CR1 and R4, CR1 becomes forward biased, as does CR9. CR4 is now reverse biased, thus disconnecting the output of the selected oscillator from buffers Q2 and Q5. Diode CR9 shunts the feedback path and stops the oscillator, while CR1 keeps the stage bias at the normal operating level.

4-40. Oscillator tuning is accomplished by varying the voltage at the junction of C12 and L7 from -5 to -25 volts. The four oscillators tune from 20 to 24, 24 to 28, 28 to 33, and 33 to 40 Mhz.

4-41. The 173 kHz IF signal from the RF board is connected to retriggerable one-shot U2. The period of U2 is determined by R15 and C23 to be 2.9 μ s, the semi-period of the 173 kHz signal. The duty cycle of the waveform on pin 6 of U2 is then 50 % and the average value of the waveform is about 2.5 volts. Amplifier AR2 shifts the dc level of the signal to make the average value about 0 volts dc. R19 adjusts the circuit for exactly 0 volts dc at 173 kHz.

4-42. The output of AR2 is connected through R30, R31, and analog switch U3 to integrator AR4a. The output of AR4a is connected through a level shifting circuit composed of AR4b, R43a, c, and d, and transistor Q9 to buffer stage AR5. The output of AR5 is the voltage used to tune all the oscillators.

4-43. Additional connections to the integrator permit the control program to tune the oscillator using a digital-to-analog converter (DAC) located on the CPU board.

4-44. U3 is a dual switch array. The second section is used to operate a bypass circuit consisting of DS1 and Q8. This circuit operates to speed up acquisition by bypassing R52, a 1 megohm resistor, during search.

4-45. Frequency acquisition in the automatic tuning mode proceeds as follows. The input carrier frequency is applied to the sampling bridge for frequency conversion. The resulting IF frequency is somewhere between dc and one-half of the local oscillator frequency. The input signal to U2, the retriggerable one-shot, will produce an output waveform whose duty cycle, and thus average value will be proportional to frequency. The control program configures U3 so as to connect the integrator to R30, providing a closed loop for frequency acquisition. The integrator will ramp until the input frequency to U2 is 173 kHz, corresponding to either a 1.211 or 346 kHz IF frequency.

4-46. The control program monitors the dc voltage at the output of the integrator and at the output of AR2 to determine if a valid IF has been established. If the integrator output is greater than + or -10 volts, the integrator is reset by connecting the junction of R29 and R37 to the input of AR4a, with the DAC IN input set to 0 volts. The band is changed and the integrator is released. This process continues until a valid IF is found.

4-47. When a valid IF signal is found, the control program changes the DAC IN dc level. This causes a current to flow through R46 which causes the IF frequency to change. The control program then measures the resulting IF frequency and the local oscillator frequency to determine the harmonic number.

4-48. Buffer stages Q2 and Q5 are grounded base amplifiers used primarily to isolate the oscillator from influences generated by the circuits they drive. Output LO1 is the signal which drives the pulse generating circuits on the RF board and output LO2 drives a cable and the frequency counter circuits.

4-49. Amplifier AR3 and transistor Q7 regulate the -15 volt supply down to -14 volts to reduce power supply noise and ripple which improves the stability of the oscillator circuits.

4-50. THEORY OF OPERATION, FM CIRCUITS.

4-51. The frequency modulation circuits recover the audio signal from the frequency modulated carrier. See Figures 4-5 and 8-11.

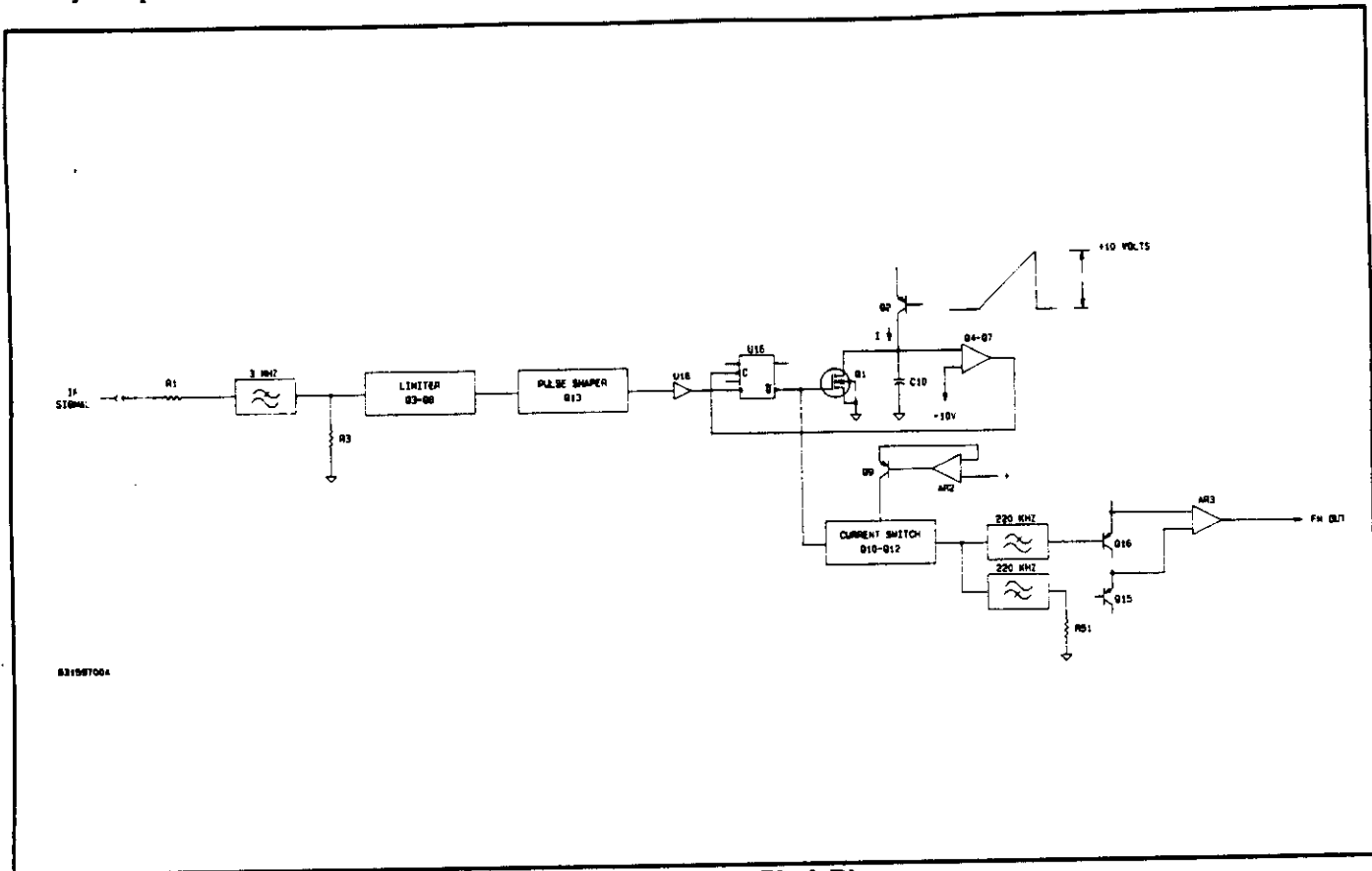


FIGURE 4-5. FM Circuits Block Diagram.

4-52. The intermediate frequency signal from the RF circuits is connected through a 3 MHz, flat-phase, low-pass filter consisting of inductors L3 and L4 and capacitors C1 and C4-C7 to a 4-stage limiter. The limiter is composed of integrated amplifier arrays Q3 and Q8 and associated components. The stages are designed with small signal feedback to minimize phase shift changes with level, thus minimizing incidental FM when the carrier contains large amounts of AM. The output of the limiter is connected to a pulse forming network consisting of Q13, R77, and R78, C48 and C49 and L8. This circuit creates a differentiated signal which drives U1b, a TTL flip-flop, which is wired as an inverter to drive the FM detector.

4-53. The FM detector is a precision monostable multivibrator which operates as follows. Each positive transition of the signal at pin 11 of U1a (corresponding exactly to each cycle of the IF frequency) causes the signal at pin 8 of U1a to go low. Enhancement mode FET Q1 is turned off, and the constant current source consisting of Q2, R2, R4, R11, R13, and CR1 charges C10 toward the positive supply rail. When the voltage reaches the value established at the base of Q5 by R30 and R28, transistor Q4 conducts and Q5 is turned off. This causes Q6 and Q7 to turn on which resets U1a. FET Q1 is turned on and capacitor C10 is discharged, completing the cycle.

4-54. The result of this operation is a constant width pulse at a rate equal to the IF frequency. As the IF frequency varies, the duty cycle and thus the average value of the waveform changes.

4-55. Enhancement mode FET Q10 operates in parallel with Q1 to toggle current switch Q11 and Q12. The collector current of Q12 is a rectangular pulse with a duty cycle determined by the instantaneous IF frequency and an amplitude determined by a precision current generator consisting of AR2, Q9 and associated components. The 220 kHz low-pass filter consisting of capacitors C36, C39, C41, and C42 and inductors L6, L9, and L10 removes the IF frequency components from the signal leaving only the modulation information.

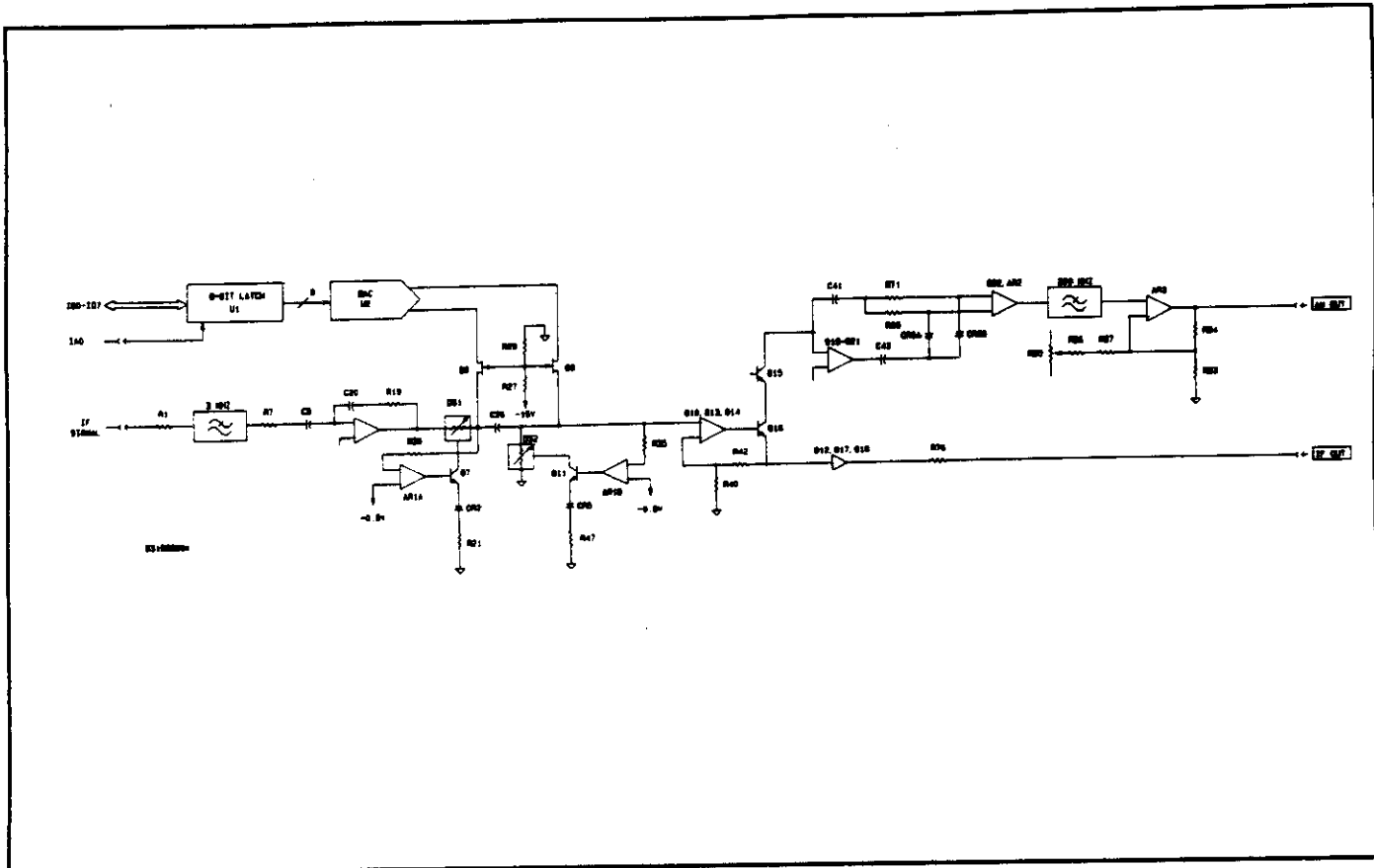


FIGURE 4-6. AM Circuits Block Diagram.

4-56. A phase equalizer consisting of C27, C28, C32, C33, L5, and R51 linearizes the filter phase response.

4-57. Transistors Q15 and Q16 and amplifier AR3 level shift and amplify the signal to drive the audio circuits.

4-58. Two local power supplies are required by the FM circuits. One is generated by Q14, R63, R70, R71 and C35. This circuit isolates the -15 volt instrument supply. The other is a +5 volt supply generated by R14, R15, C12, and AR1. This supply powers the TTL circuits on the FM board.

4-59. THEORY OF OPERATION, AM CIRCUITS.

4-60. The amplitude modulation circuits recover the audio signal from the amplitude modulated carrier. Additionally, these circuits provide a dc signal which is proportional to the carrier level at the RF IN connector. See Figures 4-6 and 8-13.

4-61. The intermediate frequency signal from the RF circuits is connected through a 3 MHz, flat-amplitude, low-pass filter consisting of inductors L5 and L6, and capacitors C1, C7, and C10 to an input amplifier composed of Q3-Q6 and associated components. The gain from the input of the filter to the output of the amplifier is about 1.5, as determined by R1, R7, and R19. This stage is carefully compensated by R88, C62, R18, and C19 to provide very flat response from less than 100 kHz to greater than 2 MHz. A flat frequency response is required to maintain low incidental AM when the carrier contains large amounts of FM.

4-62. A programmable attenuator is required to keep the output of the AM detector within reasonable limits while the carrier level changes about 40 dB. The attenuator consists of two light dependent resistors (LDRs), two control loops, an 8-bit DAC

Theory of Operation

and two isolating transistors.

4-63. Each of the two control loops operate as follows. A current flows through the variable resistance element of DS1 producing a voltage drop. This drop is monitored at one input to loop amplifier AR1a, while the other input is a reference voltage of about -0.5 volts. The output of AR1a is then the amplified difference between the reference and the drop across DS1. This error voltage is coupled to the LED portion of DS1 through buffer Q7 in such a way as to reduce this difference to nearly zero. The result is that by adjusting the current through the LDR, the resistance can be set precisely.

4-64. The variable current is supplied by U2, an 8-bit DAC and isolating transistors Q8 and Q9. The current outputs of the DAC are differential, and proportional to the magnitude of the 8-bit digital data. When the most significant bit, B1 of U2 is high and all others are low, the two currents are nearly equal. The magnitude of this current is set by R5. Any other combination of bits will increase one current while decreasing the other. The two attenuator arms track the DAC current and thus produce an attenuation which is proportional to the digital data. The control program adjusts the digital data to adjust the dc output of the AM detector.

4-65. An amplifier consisting of transistors Q10 and Q13-Q16 increases the level of the attenuator output about 18 times as determined by R42 and R40. The input impedance of the stage is high to avoid loading the attenuator, and the output impedance is high to maximize the loop gain of the following stage, the AM detector.

4-66. The AM detector is a linear-active design, that is, the diode rectifiers are linearized by including them in the feedback path of a high gain amplifier. The amplifier consists of transistors Q19-Q21 and associated components. The stage is optimized for high gain and high output impedance to drive the nonlinear feedback elements. The half-wave rectified voltages at the junctions of CR6a and CR6b and R68 and R71 are buffered by Q22a and Q22b and amplified by differential amplifier AR2. A 220 kHz, seven pole, low-pass filter consisting of inductors L10-L12 and capacitors C50-C54, and C56 removes IF frequency components from the signal, leaving only the modulation and dc components.

4-67. An additional gain of two is provided by AR3. Resistors R85-R87 provide a means to compensate for various offsets between the detector and the output of AR3.

4-68. An amplifier consisting of transistors Q12, Q17, and Q18 provides a sample of the leveled AM signal to the rear panel IF OUT connector.

4-69. THEORY OF OPERATION, FILTER CIRCUITS.

4-70. The recovered modulation from the AM or FM circuits is further processed by the filter circuits. See Figures 4-7, and 8-15.

4-71. Relay K1 is operated to select the output of the FM board for either FM or PM modulation, or the output of the AM board for AM modulation. Relays K2 and K3 are operated to select either an attenuator, or a 50 kHz, seven pole, low-pass filter as determined by the control program and the front panel low-pass filter selection. The 50 kHz filter is in the measurement path for all low-pass filter selections except the 220 kHz filters. The 220 kHz filters are located on the AM and FM boards.

4-72. Capacitors C15 and C16 remove any dc information from the signal before it is connected to a programmable attenuator consisting of R10, R11 and U3a. When the modulation signal is greater than 52.00 kHz, RAD, or %, the attenuator is selected. CR4 and CR5 protect the following stages from severe overload during range switching. Buffer amplifier AR1 has a gain of ten as determined by resistors R9 and R17. This stage is inserted in the signal path when the modulation is less than 5.200 kHz, RAD, or %, otherwise it is bypassed.

4-73. Unity gain buffer AR12 drives the high-pass filter array. The filters are 3-pole Butterworth designs except for the < 10 Hz filter which is dc coupled at this point. Resistors R19 and R26 set the insertion loss of the < 10 Hz position to equal that of the other active filters. The other filters are designed to cut off at 30, 300, and 3000 Hz. The control program operates analog multiplexer U4 based on the front panel high-pass filter selection.

4-74. Amplifier AR2 and associated components comprise the 30 Hz filter. Similarly AR3 and associated components comprise the 300 Hz filter, and AR4 and associated components comprise the 3000 Hz filter.

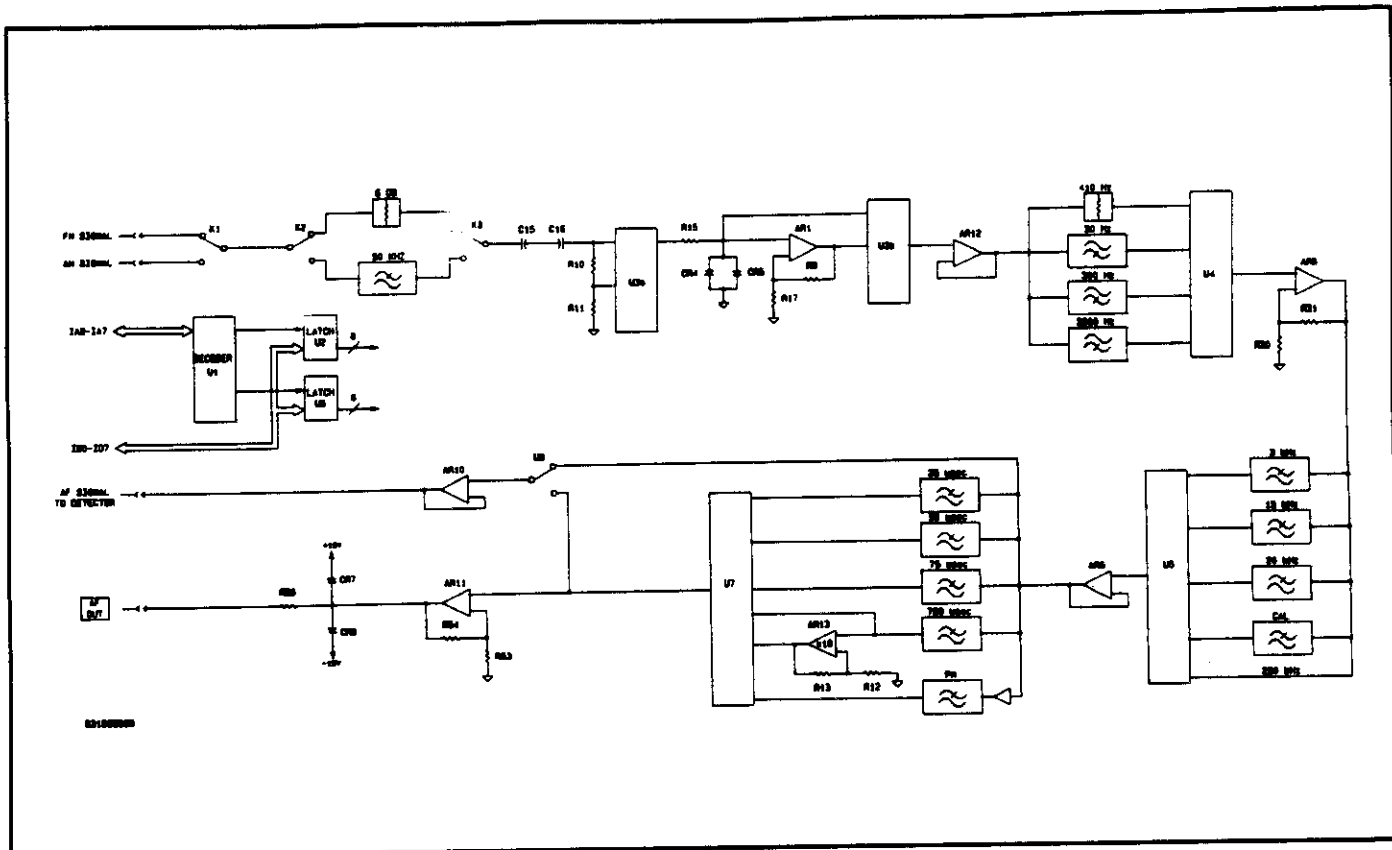


FIGURE 4-7. Filter Circuits Block Diagram.

4-75. AR5 amplifies the signal about 4.6 times, as determined by R30 and R31 and drives a low-pass filter array. The 3 and 15 kHz filters are 3-pole Butterworth designs, and the 20 kHz filter is a 3-pole Bessel design. Additionally, a thru position is provided for the 50 and 220 kHz filters, and a gaussian filter consisting of R34, R38, R40, C36, C38, and C41 is provided for calibration. Analog multiplexer U5 is operated by the control program based on the front panel switch setting or the carrier frequency to select the appropriate filter.

4-76. Unity gain buffer AR8 drives the de-emphasis and phase modulation filters. The de-emphasis networks are single pole gaussian filters with cut frequencies of 212 Hz, 2.122 kHz, 3.183 kHz, and 6.366 kHz corresponding to the time constants of 750, 75, 50, and 25 microseconds respectively.

4-77. AR9a and b and associated components comprise the phase modulation filter. This filter is designed to have an insertion gain of unity at 1 kHz modulation frequency, and a response that approximates an ideal integrator over most of the audio frequency range.

4-78. Analog multiplexer U7 is operated by the control program to select the appropriate de-emphasis network as determined by the front panel de-emphasis switch setting. Additionally, the control program bypasses these networks in the AM measurement mode, and selects the phase modulation filter in the PM mode.

4-79. Unity gain amplifier A10 buffers the signal which is connected to the detector circuit board through analog switch U8. U8 is operated by the control program to select pre-display or post-display de-emphasis as determined by SPCL functions 7 or 8, or the de-emphasis mode as set via the IEEE-488 bus controller.

4-80. Amplifier AR11 increases the signal by about 2.4 times as determined by R53 and R54 to generate the front panel AF OUT signal. Resistor R55 determines the output impedance of 600 ohms and diodes CR7 and CR8 provide reverse power protection for AR11.

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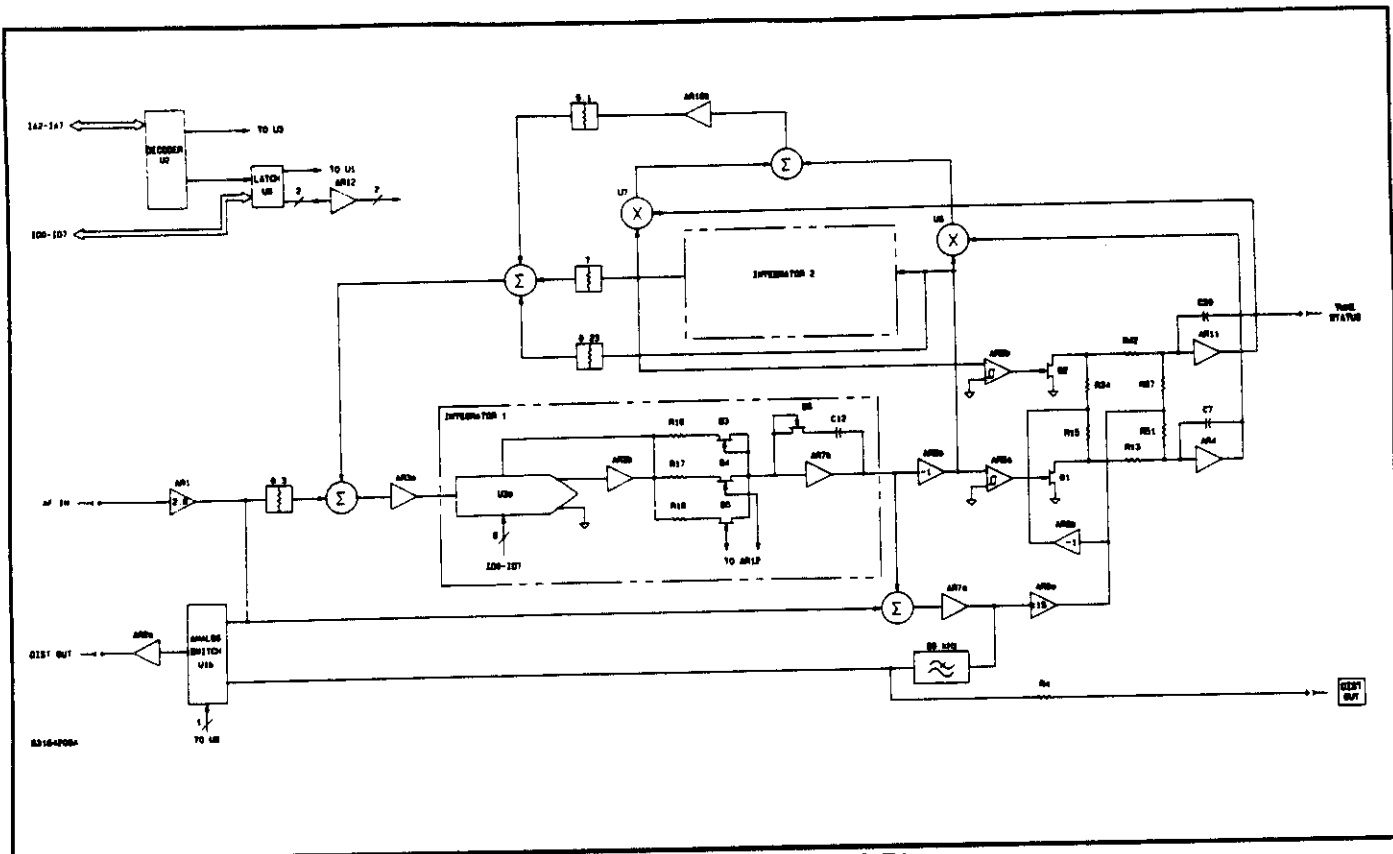


FIGURE 4-8. Distortion Analyzer Block Diagram.

4-81. Digital control signals for the filter board are latched from the instrument control bus by octal latches U2 and U6. Strobe signals to operate the latches are generated by address decoder U1.

4-82. THEORY OF OPERATION, DISTORTION ANALYZER

4-83. The distortion analyzer is an automatically tuned and balanced state-variable notch filter. The circuits operate in conjunction with the filter and detector circuits to produce a display of audio distortion in % or dB SINAD. See Figures 4-8 and 8-17.

4-84. The audio signal to be measured is applied to amplifier AR1 through ac coupling network C28 and R1. AR1 is configured for a gain of 2.82 as determined by R3 and R2. The signal is then connected to the notch generating circuits.

4-85. The notch filter consists of a state variable bandpass filter and a balance amplifier AR7a. The bandpass filter is tuned to the incoming audio signal by the control program. The output of the bandpass filter is subtracted from the input signal leaving only the harmonics and residual noise at the output of AR7a. Fine adjustment of the notch center frequency and the amplitude of the bandpass output is accomplished by two control loops which operate to reduce the in-phase and quadrature components of the signal at the output of the balance amplifier.

4-86. The individual integrators in the filter are identical, so only one will be described in detail. The output signal from summing amplifier AR3a is connected to the reference input of multiplying digital-to-analog converter (DAC) U3a. The gain from the reference input of the DAC to the output of amplifier AR3b is proportional to the digital data on the D0-D7 inputs. The output of AR3b drives resistors R16-R18 and transistor switches Q3-Q5 which are connected to the inverting input of AR7b. Integrating capacitor C12 is connected from the output of AR7b to the inverting input, completing the integrator circuit. Transistors Q6 and Q3 are always conducting and are used to reduce the residual distortion of the integrator stages. Transistors Q4 and Q5 may be turned on by the control program to change the integrator time constant in decade steps. Frequency range breakpoints

are at 250 and 2500 Hz. Coarse tuning on each band is accomplished by changing the digital data inputs to the DAC. The tuning range is about one decade from 25 Hz to 250 Hz, in 1 Hz steps on the lowest band. The circuit values are adjusted such that when the digital data is 25 decimal, the frequency is about 25 Hz. Similarly, when the digital data is 250 decimal, the frequency is about 250 Hz.

4-87. The signal at the output of AR7a is amplified an additional 15 times by AR9a. The gain is determined by R30 and R31. Additionally, AR9b inverts the amplified signal to provide an out of phase signal used to generate a full-wave rectified signal for the tune and balance integrators. The rectifiers operate as follows: While switch Q2 is shorted to ground, a current flows in resistor R57. When switch Q2 opens twice as much current, of the opposite phase, flows in R42. Since the currents in R57 and R42 are 180 degrees out of phase, the net current flow is in the same direction as when Q2 is closed. The result is a full-wave rectified current. This produces a voltage at the output of integrator AR11 which drives four quadrant multiplier U7. The current output at Pin 4 of U7 is proportional to the product of the dc voltage at the output of the integrator AR11 and the ac voltage TP4. This current is summed back into the notch summing amplifier AR3a to cancel balance and tuning errors.

4-88. The notch output signal is filtered by an 80 kHz active low-pass filter consisting of amplifier AR2b, C2, C8, C15, R37, R49, and R50. This signal is connected through 600 ohm resistor R4 to the DIST OUT connector on the rear panel, and through switch U1b and buffer AR2a to the rms detector circuits.

4-89. Switch U1b is operated by the control program to monitor the input signal and the notch signal alternately. The ratio of these signals, times 100 is the distortion in percent. SINAD ratio is calculated by the control program and displayed in dB.

4-90. A tune status output signal is generated by attenuating and level shifting the dc output of the tune integrator. This signal is used by the control program to determine that the notch is properly tuned.

4-91. Decoder U2 generates data latch strobes for the circuits on the distortion analyzer board. A portion of octal latch U8 is used to store range data for the distortion analyzer.

4-92. Comparator AR12 is used to shift the TTL logic signal levels at the outputs to U8 to 15 volt logic signals to operate the FET range switches in the notch filter.

4-93. THEORY OF OPERATION, DETECTOR CIRCUITS.

4-94. The recovered modulation signals from the filter board are converted to dc signals by the detector circuits. The detectors include plus and minus peak detectors, an rms detector, a quasi-peak detector, and an average detector. See Figures 4-9 and 8-19.

4-95. The recovered modulation signal is ac coupled to analog switch U1 through coupling network C36 and R5. U1 is operated by the control program to connect the peak detector circuits to the audio signal or a ground reference established by R11 and C6.

4-96. The output of U1 is connected to the input of U13d through an equalizer network consisting of R12 and R13 and C37 and C38. This network compensates for a slight decrease in peak detector efficiency at about 250 kHz. U13d and U13c are voltage followers cascaded to drive the positive peak detector. The output of U13d also drives a precision inverter circuit consisting of U13a and R55a-R55d which in turn drives the negative peak detector through voltage follower U13b. This seemingly unnecessary symmetry is required because the full-scale resolution of the peak displays is 0.02%. The positive and negative peak detectors are identical circuits driven by audio signals that are 180 degrees out of phase.

4-97. Amplifier U15 and U19a and associated components are arranged as a positive peak detector. During the positive excursion of the audio signal, the output of U15 is driven positive; C20 then charges through CR3. U19a buffers the voltage across C20 and adds a small offset. When the output of U19a reaches a value equal to the positive peak of the waveform plus a small increment, the output of U15 goes negative and thus terminates the charging of C20. The output of U19a is then equal to the positive peak of the audio signal.

4-98. The small offset created by R24 and R25 is required to insure that there is a net positive charge on C20 when the signal on pin 3 of U15 is zero. Diode CR1 improves frequency response by limiting the voltage excursion at pin 6 of U15 at about -0.7 volts in the negative direction.

Theory of Operation

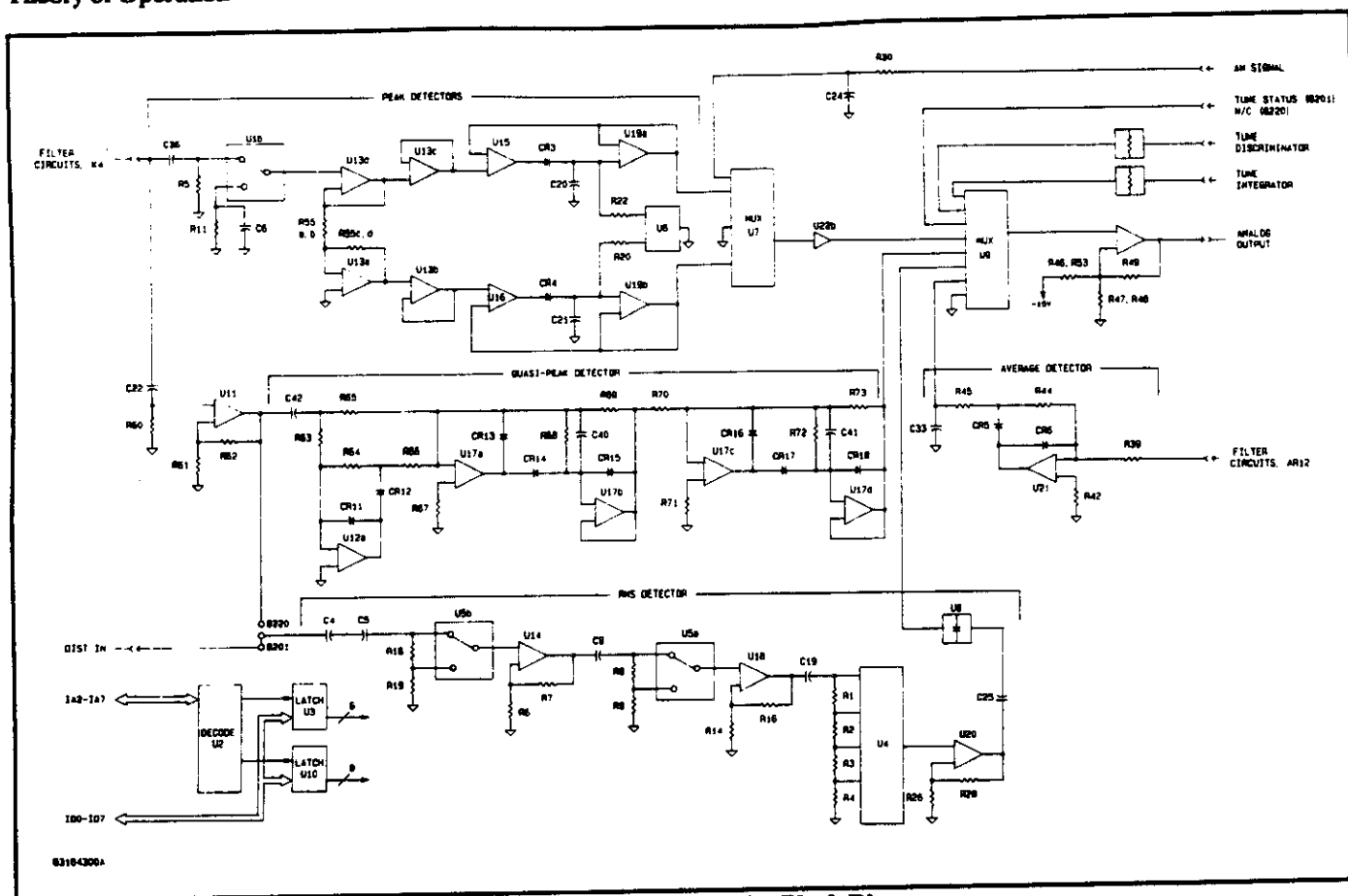


FIGURE 4-9. Detector Circuits Block Diagram.

4-99. The peak detector consisting of U16 and U19b and associated components operates in an identical manner, except that the audio signal at pin 3 of U16 is inverted, so that the positive output voltage at pin 7 of U19b represents the negative peak of the audio waveform.

4-100. Analog switch U6, R20 and R22 are connected across capacitors C20 and 21 to reset the peak detectors during the various phases of the peak measurement cycle.

4-101. The measurement cycle proceeds as follows: The control program asserts the peak detector reset signal discharging capacitors C20 and C21. Analog switch U1 is set to connect the ground reference network R11 and C6 to the input of U13d. After a short wait for transients to settle, the reset signal is removed and both peak detector outputs are measured. The measurements represent the zero input signal condition of the detectors. The reset signal is again asserted, and analog switch U1 is set to connect the audio input signal. The reset signal is again removed and both peak detectors are again measured. The measurement represents the output of the detectors including the input signal and offsets. The offsets are removed by the control program and the corrected measurement displayed on the front panel digital display. The measurement cycle is repeated by the control program as required. The peak average display is generated by adding the plus and minus peaks and dividing the result by two.

4-102. The outputs of the peak detectors and a dc signal from the AM detector are routed through an analog multiplexer, U7, to amplifier U22b. The circuit gain is three, as determined by R43 and R37, which brings the full-scale output of the peak detectors and the nominal output of the AM detector to about three volts. This signal is connected through analog multiplexer, U9, to a second amplifier U22a and associated components. This stage is designed to have a gain of about 2.04 and a dc offset of about 100 millivolts. Gain is required to increase the full-scale signal to about 6 volts for later analog-to-digital conversion; the offset is required to insure that inputs near zero volts still produce a positive dc output. The output of U22a is connected

through the card edge to the CPU board.

4-103. Several other signals are connected to multiplexer U9. A signal representing the output of the frequency acquisition integrator is attenuated and level shifted by resistors R33, R34, and R35. When the output of the integrator is +10 volts, the voltage at the pin 5 of U9 will be about 3.7 volts and when the output of the integrator is -10 volts, pin 5 will be about 0.58 volts. A second voltage from the frequency acquisition discriminator is attenuated and level shifted by R38, R40, and R41. For discriminator voltages between +3 and -3 volts, the voltage at pin 4 of U9 will vary between 3.2 and 0.8 volts respectively.

4-104. The signal on pin 6 of U9 is a signal representing the tuning status of the distortion analyzer circuits. This signal is used to determine that the tuning integrator output voltage is within normal operating range. Pin 7 of U9 is grounded to provide a zero volt reference for the analog to digital converter. Three other inputs to U9 will be covered separately below.

4-105. A second audio signal is ac coupled by coupling network C4, C5, and R18 and R19 to analog switch U5. This signal originates on the distortion analyzer board and represents an amplified version of the signal at the peak detectors. R18 and R19 divide the input signal by ten, so that the signal at pin 3 of U14 is either the input signal, or the signal divided by ten, as determined by the setting of U5. The stage gain of U14 is set at 11.5 as determined by R6 and R7. Capacitor C7 provides high frequency compensation. Similarly, the output of U14 is connected to an attenuator consisting of R8 and R9, analog switch U5, and a second amplifier U18. Diodes CR7-CR10 and resistors R57-R59 speed overload recovery of U14 and U18. U18 is also configured for a gain of 11.5 and is ac coupled to an attenuator consisting of R1-R4 and analog switch U4. This attenuator is programmable for an attenuation of zero, six, fourteen, or twenty dB. Amplifier U20 is configured for a gain of 11.5 and is ac coupled to rms detector U8.

4-106. The complete amplifier/attenuator chain is programmable for a gain change of 0 to 60 dB (1000 times) in steps of 6 or 8 dB. Gain is established as required by the control program to maintain the output of the rms detector between about 1 and 3 volts dc, corresponding to rms inputs of 1 to 3 volts respectively. Capacitor C26 determines the low frequency characteristics of the rms detector and is selected to maintain modest errors down to about 10 Hz. The output at pin 6 of U8 is connected to multiplexer U9 as one of the possible inputs to the analog to digital converter.

4-107. An average detector consisting of U21 and associated components monitors the signal level at the input to the high-pass filter array. This detector is used to determine if an overload condition exists in the filter circuits, since the filters may attenuate an overrange signal before it is detected by the peak or rms detectors. This detector is also used for autoranging in the PM measurement mode.

4-108. The voltage at pin 2 of U21 is nearly zero due to the amplifier's high open loop gain. The voltage at the junction of C35 and R39 produces a current which also flows through R44, CR6, and CR5. If the current is sinusoidal, the current flows through R44 and CR5 on one half-cycle of the waveform, and through CR6 on the other half-cycle. The voltage at the junction of CR5 and R44 is thus half-wave rectified, and a dc voltage equal to the voltage peak divided by π (3.14159) is produced. This voltage is connected to pin 10 of multiplexer U9 through filter R45 and C33. The filter removes the ac components from the rectified signal.

4-109. The quasi-peak detector consists of amplifiers U12a, and U17a-U17d and associated components. This circuitry is designed to meet the requirements of CCIR 468-3. U12a, CR11, CR12, and associated components are configured as an absolute value circuit. The output signal at the junction of R65 and R66 is a full-wave rectified current. U17a and U17b and associated components form a peak detector with a charge time of 2 milliseconds, and a decay time of 400 milliseconds. U17c and U17d and associated components form a peak detector with a charge time of 200 milliseconds, and a decay time of 600 milliseconds. The circuits are cascaded to meet the timing requirements of CCIR 468-3. The output is connected to pin 11 of multiplexer U9.

4-110. Octal latches U3 and U10 are used to store the control data from the instrument bus. The latch strobe signals are generated by address decoder U2.

4-111. Power supply decoupling is provided by L1, L2, C1, and C2. Additional supplies (+5 and -5 volts) are generated on board by U23a and b, and resistors R27, R29, R31, and R32. Capacitors C10 and C13 provide filtering to reduce power supply noise.

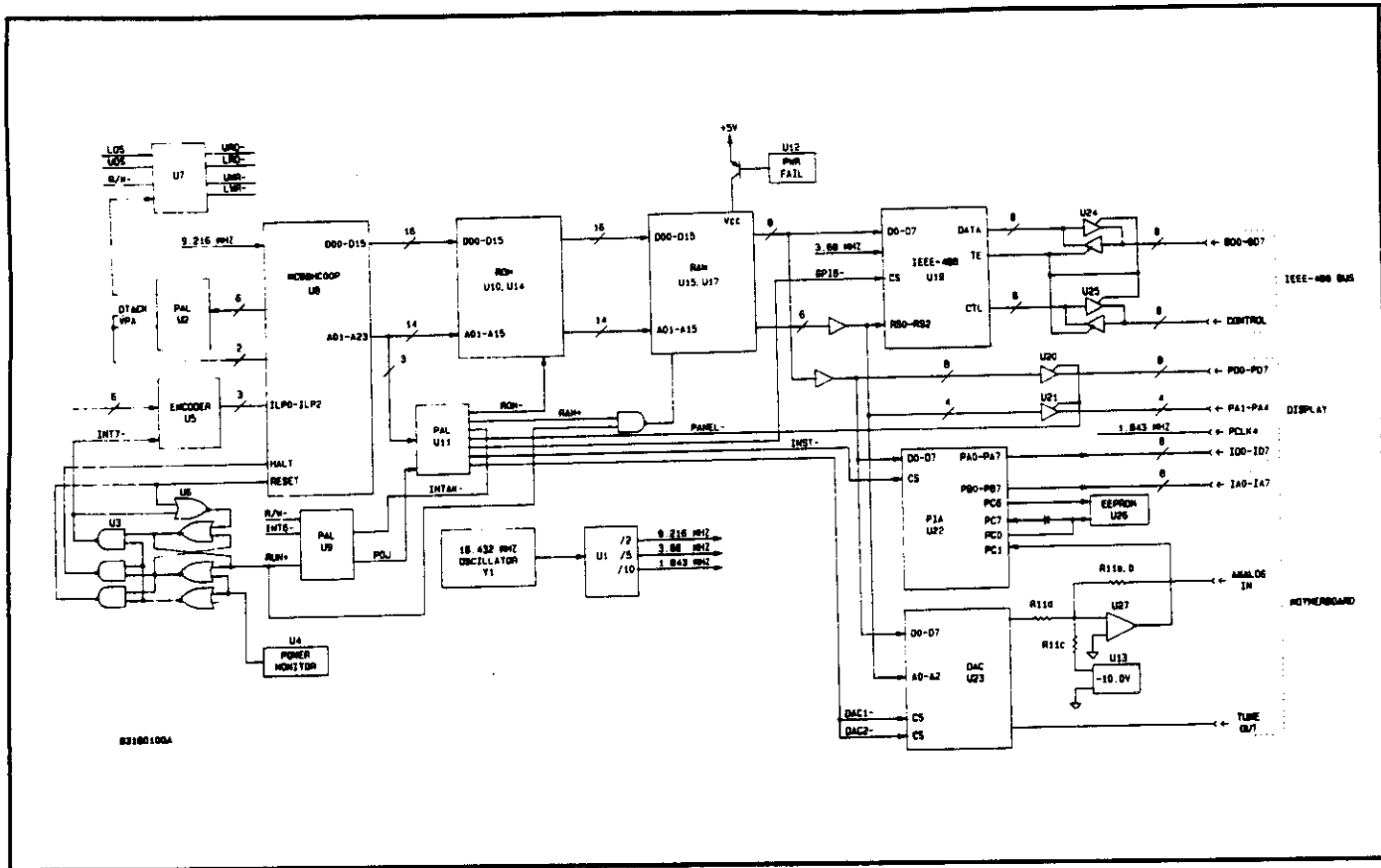


FIGURE 4-10. CPU Circuits Block Diagram.

4-112. THEORY OF OPERATION, CPU CIRCUITS.

4-113. The CPU circuits provide the microprocessor control of all functions of the instrument. Additionally, the IEEE-488 microcontroller is located on this board as are the tuning DAC, the A/D converter and instrument interface circuits. See Figures 4-10 and 8-21.

4-114. The output of crystal oscillator Y1 is connected to U1, a dual bi-quinary counter used to generate the various timing signals required by the CPU and display circuits. The microprocessor clock signal, CLK is 9.21 MHz which is the frequency of Y1 divided by two. The timing of the IEEE-488 controller is generated by dividing the output of Y1 by five. The resulting signal, SCLK is 3.686 MHz. The 3.686 MHz signal is divided by two again to provide the PCLK signal for operation of the keyboard display controllers on the I/O board.

4-115. The 68000 microprocessor executes a control program stored in read-only-memory, (ROM) U10 and U14. Program variables and front panel setups are stored in random-access-memory, (RAM) U15 and U17. Instrument control is accomplished via peripheral interface adapter U22, and IEEE-488 communications is controlled by microcontroller U19 with buffers U24 and U25. Analog-to-digital conversion is accomplished by one-half of DAC U23 in conjunction with reference U13, comparator U27 and precision resistor array R11. The other half of U23 is used to tune the local oscillator circuits.

4-116. Local communications on the CPU board are via the high-speed CPU data bus D00 through D15 and address bus A01 through A17. Address lines A18 through A23 are not utilized. Memory space is partitioned by PAL U11 as follows:

Address.....	Function
00000-0FFFF	ROM, U10 and U14
10000-1FFFF	RAM, U15 and U17
20000-2FFFF	PIA, U22

21000-21FFFA/D, conversion, U23A
22000-22FFFD/A, conversion, U23B
23000-23FFFI/O board, via U20 and U21
24000-24FFFIEEE-488, U19

4-117. U15 and U18 are required to isolate a portion of the devices on the address and data buses to meet the loading requirements of the microprocessor and memories.

4-118. During power-up, the +5 volt supply is monitored by supply supervisor U4 and the POR- control line is held low as long as the supply is below about 4.75 volts. U4 also pulls POR- low if, after normal power-up, the supply drops below 4.75 volts. Capacitor C1 is required to reduce the influence of transients on the +5 volt supply and C2 establishes the time that the POR- line is held low after the supply reaches normal levels. This delay insures proper microprocessor reset operation.

4-119. A flip-flop consisting of gates U6a and U6d is set by the high output of gate U6b, and the microprocessor RESET- and HALT- inputs are pulled low through gates U3b and U3c. The active reset signal is also supplied to peripheral circuits through programmable logic array (PAL) U9. After the +5 volt supply reaches its nominal value, signal POR- goes high, the HALT- and RESET- lines go high and flip-flop U6a/U6d is reset. This flip-flop activates the RUN+ signal to enable operation of the RAMs.

4-120. The RAM integrated circuits are powered from a non-volatile power supply consisting of U12, Q1 and battery BT1. If the +5 volt supply drops below the battery voltage of about 3 volts, U12 automatically transfers the RAM supplies to the battery. At the same time power supply supervisor U4 causes the POR- line to be pulled low. This in turn causes a microprocessor interrupt priority 7, (NMI). The control program is stopped and a RESET instruction is executed which resets all peripheral circuits, again sets latch U6a/U6d, and stops normal program activity. Control line POJ- is not used in normal operation of the instrument and can safely be ignored.

4-121. Analog-to-digital conversion is accomplished by the control program, one-half of DAC U23, comparator U27 and precision resistor array R11. The analog signal to be measured is connected to pins 3 and 4 of R11 which parallels two of the precision resistors and connects them to pin 2 of U27. Connected to the same point is one precision resistor of R11 which is connected to the -10.0 volt reference U13. A second resistor of R11 is connected to the VOA output of DAC U23. The control program successively sets data bits and tests the output of U27 via PLA U22. The progression is from most significant to least significant bit. If the comparator changes states, the bit is reset, otherwise is left set. This successive approximation continues until 13 bits are tested.

4-122. Control of the local oscillator tuning is accomplished with one-half of DAC U23. The 16-bit digital word representing the desired output of U23 (-10 to +10 Volts) is simply written to U23 and the output taken from the VOB terminal.

4-123. U19 is the IEEE-488 interface microcontroller. All IEEE-488 operations are conducted by this circuit in conjunction with the microprocessor interrupt routines. These routines move data into and out of RAM buffers as required and control program flow in response to bus commands. When bus activity occurs, U19 sets the INTS- line low. The microprocessor reads the interrupt status registers to determine the nature of the interrupt and responds accordingly. All bus state transitions are controlled by U19, thus insuring compliance with IEEE-488 timing requirements.

4-124. THEORY OF OPERATION, COUNTER CIRCUITS.

4-125. The counter circuits provide the frequency measurement functions for the Model 8201. Additionally, the calibration signals for internal detectors are generated on the counter circuit board. See Figures 4-11, 8-23, and 8-25.

4-126. A signal from 10.0 MHz crystal oscillator Y1 is divided by two by U20a, and by two again by U20b. The resulting 2.5 Mhz signal is connected to U22 for additional frequency division. The signal on pin 9 of U22 is 1.25 MHz and is used to generate the AM calibration signal. The signal on pin 15 of U22 is 1.221 kHz and is used to generate the AM and FM calibrator modulation. For a complete discussion of calibrator operation, refer to Section 5, Performance Test 12.

4-127. The output of crystal oscillator Y1 is also connected to gate U4a. The other input of U4a is a signal derived from the EXT REF input. If an external reference signal is present, pin 8 of U1b will be alternating between TTL low and high levels.

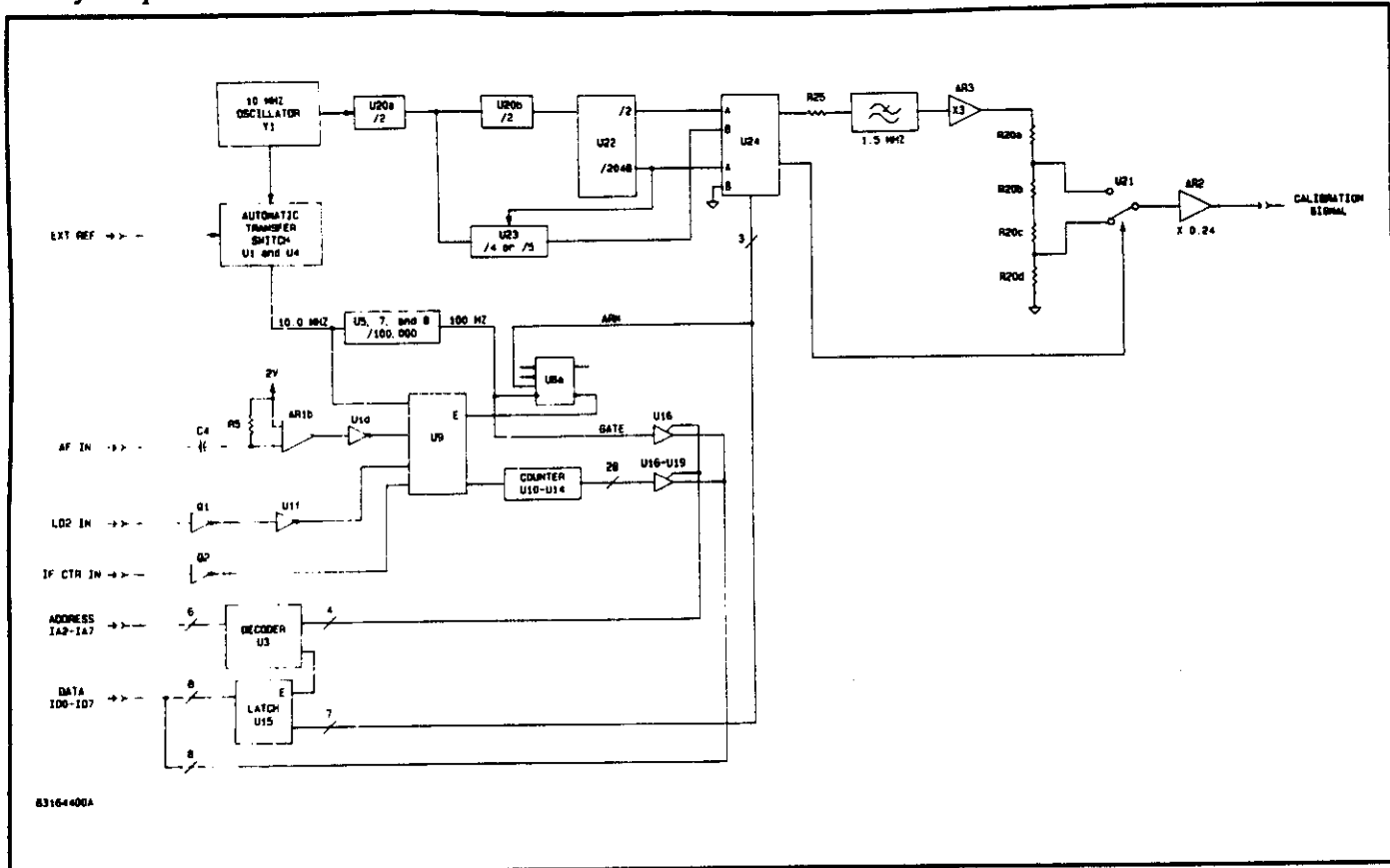


FIGURE 4-11. Counter Circuits Block Diagram.

The low level signal will cause CR1 to become forward biased and thus bias pin 1 of U1c low. The output of U1c will be high, which will enable U4b. This will allow the external timebase signal to appear at pin 6 of U4c. Simultaneously, the output of U1c is inverted by U1e to disable U4a, disconnecting the internal timebase signal. When the external signal is removed, the internal timebase signal will appear at pin 6 of U4c.

4-128. This signal is divided down to 100 Hz by U5, U7, and U8 and is the gate used for all frequency measurements made by the Model 8201. The gate signal is used to clock d-latch U6a and U6b, and an interrupt latch on the CPU circuit board, to interrupt the microprocessor every 10 milliseconds.

4-129. A sample of the local oscillator signal at pin 30 of the edge connector is amplified to TTL levels by Q1 and associated components. U1f further shapes the signal which is applied to data selector U9.

4-130. A sample of the intermediate frequency at pin 32 of the edge connector is similarly amplified by Q2 and associated components and connected directly to data selector U9.

4-131. A sample of the audio frequency signal at pin 34 of the edge connector is converted to TTL levels by AR1b and associated components. Operating bias is supplied by diode DS2 and R4. The output of AR1b is connected to data selector U9 through buffer U1d and to the clock input of U2b.

4-132. U2a and U2b are configured to synchronize one cycle of the audio signal to the interrupt cycle of the microprocessor. The control program arms the gate latch U6a by setting the D input high. On the rising edge of the 10 millisecond gate signal the Q output of U6a goes high. This clocks the high level D input of U2a to its Q output. The rising edge of the audio signal then transfers this high level to the Q output of U2b and allows the 10 MHz reference signal to pass through U4d to data selector U9. When the Q output of U2b goes high, the Q- output goes low and resets U2a. This clears the D input of U2b so that on the next positive transition of the audio signal the Q output goes low and disables the counting sequence. This mode of measurement

is used for audio frequencies below 1 kHz.

4-133. When the audio frequency exceeds 1 kHz, the measurement is made by counting the number of zero crossings of the signal in one second. The actual gate interval is controlled by the firmware by allowing a fixed number of 10 millisecond gate cycles to elapse before the arming signal on the D input of U6a is removed. Each gate cycle causes a microprocessor interrupt. The program counts the number of times an interrupt has occurred since U6 was armed. When the correct number of cycles is reached, the sequence is stopped. The residue in the counter chain is then read and the counter is reset.

4-134. Carrier frequency measurements are made by counting the local oscillator for N gate cycles, where N is the harmonic number used to generate the intermediate frequency. The intermediate frequency is then measured, and the difference is calculated as the carrier frequency. The expression relating the three frequencies is:

$$F_{rf} = N \times F_{lo} - F_{if}$$

4-135. The output of U9 is the signal to be counted. The counter consists of U10, U12, U13, and U14. U10 and U12 are high speed binary dividers which are required to measure the local oscillator signal at 40 MHz. U13 and U14 are relatively slow speed CMOS 12-bit counters which always operate at less than 3 MHz. The counter has a total length of 28 bits which allows counting to greater than 260 MHz with a resolution of 1 Hz.

4-136. The outputs of the counters are connected to the instrument data bus via 3-state buffers U16-U19. The data is read by the microprocessor in 4, 8-bit bytes. Besides the frequency information, the gate and external reference status signals are read.

4-137. U15 is an 8-bit latch which is used to store instrument data bus information when the counter board is addressed by the microprocessor. Address decoder U3 decodes instrument addresses 8 through 11 to operate the select lines for U15-U19.

4-138. THEORY OF OPERATION, I/O CIRCUITS.

4-139. The I/O circuits provide an interface between the microprocessor and the front panel LED displays and keyswitches. See Figures 4-12, and 8-27.

4-140. U2 and U3 are keyboard/display microcontrollers. Each circuit is capable of controlling up to 16 digits of display and a 64 key keyboard. The Model 8201 requires more than 16 display digits, so two circuits are required, however, less than 64 keys are used, so that only one of the keyboard interfaces is used. U2 operates 14 displays including the FREQUENCY/LEVEL display and legends, and the AUDIO display and legends. U3 operates 14 displays including the MODULATION display, the modulation legends, the SPCL/PRGM display and legends, the IEEE-488 legends, and the keyswitch LEDs on the keyboard. Additionally, U2 handles all keyboard switches. When a key is depressed, U2 activates the INT- line via U1 to interrupt the microprocessor. The key closure is recognized by the control program by reading the data from U2 which releases the INT- line.

4-141. U1 is a dual decoder used to generate chip select signals from the address signals PA2-4. The two strobe signals at TP1 and 3 are used to select U2 and U3 respectively. One half of U1 is connected merely to invert the sense of the IRQ signal from U2 to the microprocessor. The panel interrupts are priority level 3. Signals from U2 and U3 are connected to the Display/keyboard via J3. LEDs DS1 and DS2 are activity indicators for the two, five volt supplies present on the I/O board.

4-142. THEORY OF OPERATION, DISPLAY AND KEYBOARD CIRCUITS.

4-143. The display and keyboard circuits provide the operator interface to the Model 8201 circuits. Key closures are detected and sent to the microprocessor which interprets them. The microprocessor then modifies the display LEDs appropriately. See Figures 4-13 and 8-29 through 8-33.

4-144. The software configurable display/keyboard microcontroller circuits A11U2 and A11U3 on the I/O circuit board are programmed to operate 16 display digits. All the displays operated by A11U3 are connected to a common cathode driver bus which is generated by the select lines DA01-DA31 and DB01-DB31. These signals are buffered by U1 and U3 and connected to the display cathodes through current limiting resistors R1 and R2.

Theory of Operation

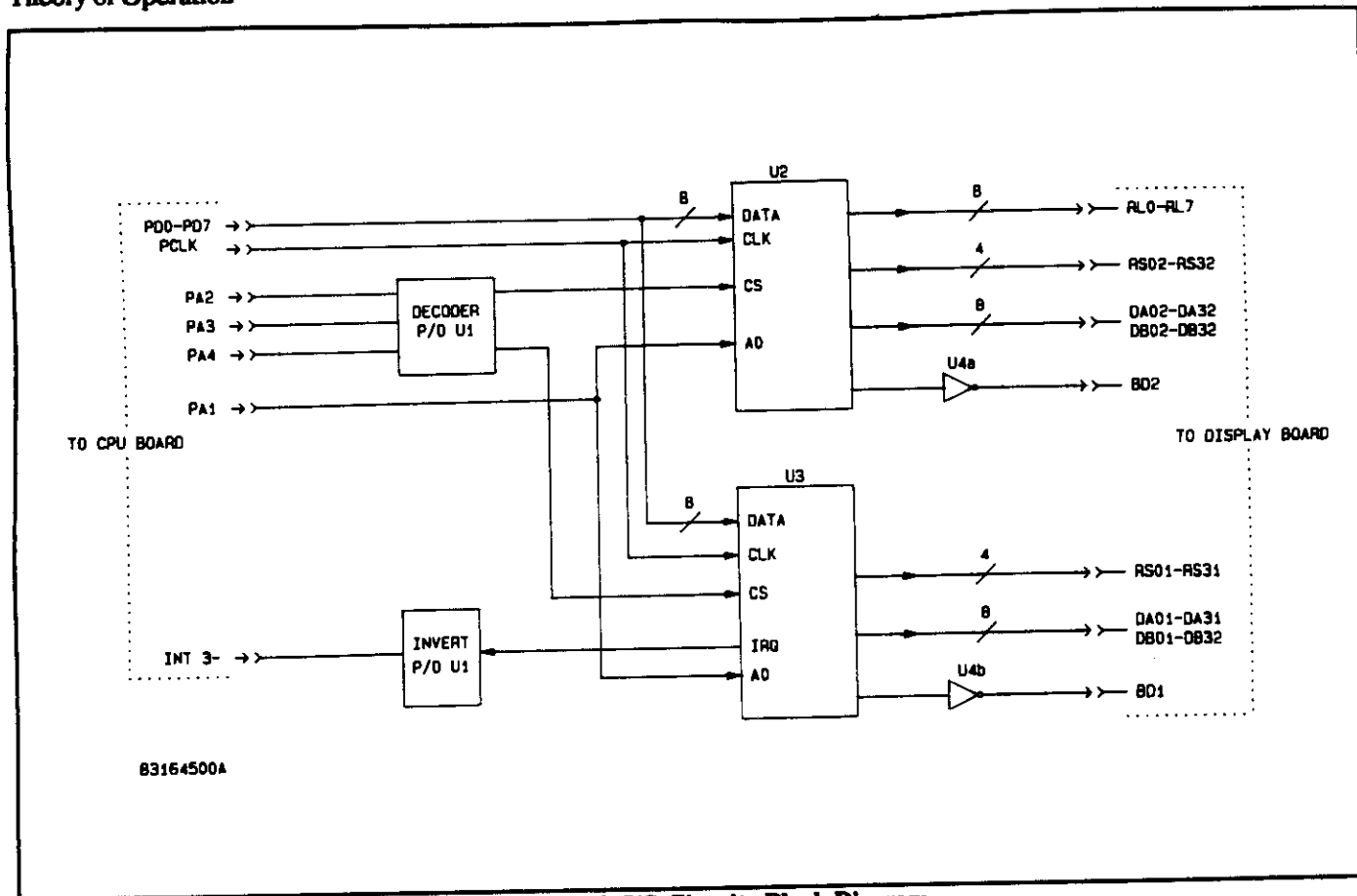


FIGURE 4-12. I/O Circuits Block Diagram.

4-145. The signals RS01-RS31 are connected to a one-of-sixteen decoder consisting of U2 and U4. The sixteen decoder output lines are connected to buffers U5 and U6 where the interdigit blanking is applied by signal BD1-. The signals are then connected to the display anodes via driver circuits U7 and U8. Note that only 6 of the 8 available outputs of U8 are used. All segment decoding is done by the microprocessor so that no additional decoders are required.

4-146. Similarly all the displays operated by A11U2 are connected to a common cathode driver bus which is generated by the signal lines DA02-DA32 and B02-B32. These signals are buffered by U9 and connected to the display cathodes through current limiting resistor R3.

4-147. The signals RS02-RS32 are connected to a one-of-sixteen decoder consisting of U10 and U12. Fourteen of the sixteen decoder output lines are connected to buffers U13 and U14 where the interdigit blanking is applied by signal BD2-. The signals are then connected to the display anodes via driver circuits U15 and U16. Five of the buffered lines from U16 are connected through J5 to the keyboard to operate the keyswitch LEDs. The keyswitch LEDs are connected into five common anode groups with eight common cathode lines. Separate cathode drive lines are generated for the keyboard LEDs by U11 and R4.

4-148. A second decoder, U17 is connected to the RS02-RS22 lines to generate a one-of-eight select signal to drive the keyswitches on the keyboard. The signal lines RL0-RL7 are also connected to the keyswitches. The resulting keyswitch matrix can accommodate sixty-four switches, of which 57 are used. The time division multiplexed signals from U17 are connected to the RL lines when a key is depressed. The keyboard controller, U2 on the I/O board, encodes the key response based on which RL line was active during the time one of the outputs of U17 was active. Multiple keyswitch closures and key debouncing are handled by U2. Keyswitch closures cause microprocessor interrupts as described in the I/O circuits theory.

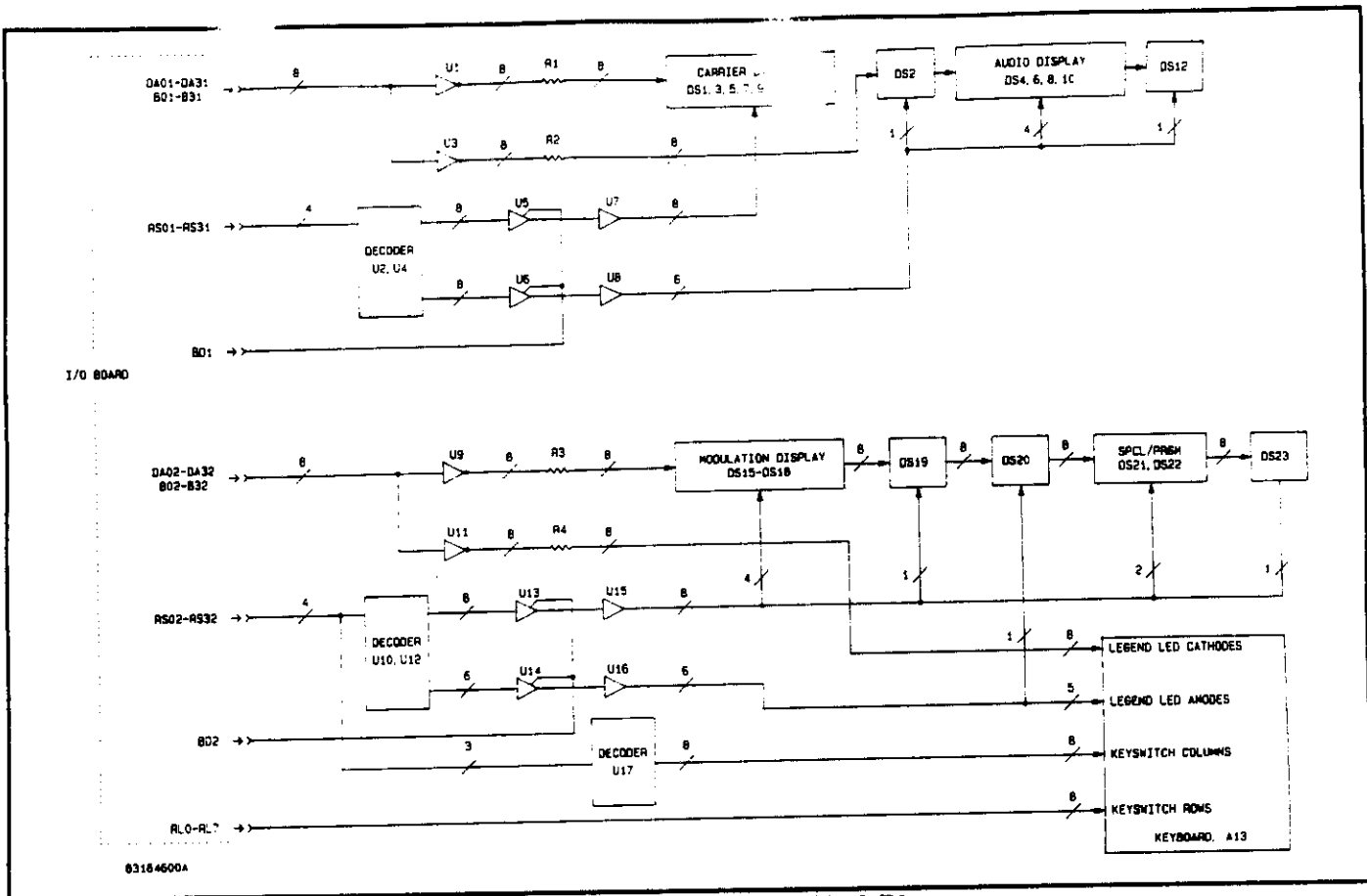


FIGURE 4-13. Display and Keyboard Block Diagram.

4-149. THEORY OF OPERATION, MOTHERBOARD/POWER SUPPLY

4-150. The motherboard circuitry provides the main interconnect for the operating circuits of the Model 8201. The motherboard contains the connectors for the plug-in boards, the regulated power supplies, the decoder and latch for the RF and oscillator circuits, and the power fail circuitry. See Figures 4-14, 8-3, and 8-4.

4-151. The instrument data lines ID0-ID7 are connected to latches U1 and U9 which are selected by decoder U2. Information on the data lines is latched into U1, and connected to the RF circuitry to operate the tuning and conversion circuits. ID0 is latched into U9 to operate analog switch U10 and switch Q1 to drive overload protect/attenuator module A30, for carrier inputs greater than +20 dBm.

4-152. Line power is connected to transformer T1 via line filter FL1, fuse F1, and line voltage selector switch S2. FL1 keeps internally generated RF signals from appearing on the power connecting cable, thus preventing unwanted electromagnetic radiation. Line switch S2 alters connections to the primary of T1 which allows the Model 8201 to be operated from line voltages from 100 to 240 volts.

4-153. One of the two secondary windings on T1 is connected through full-wave bridge CR1 to regulators U7 and U4. These three terminal regulators generate 5 volt regulated voltages for the instrument logic circuits and the front panel display. A separate regulator, U7, is used for the display and I/O circuits in order to minimize internally generated switching noise.

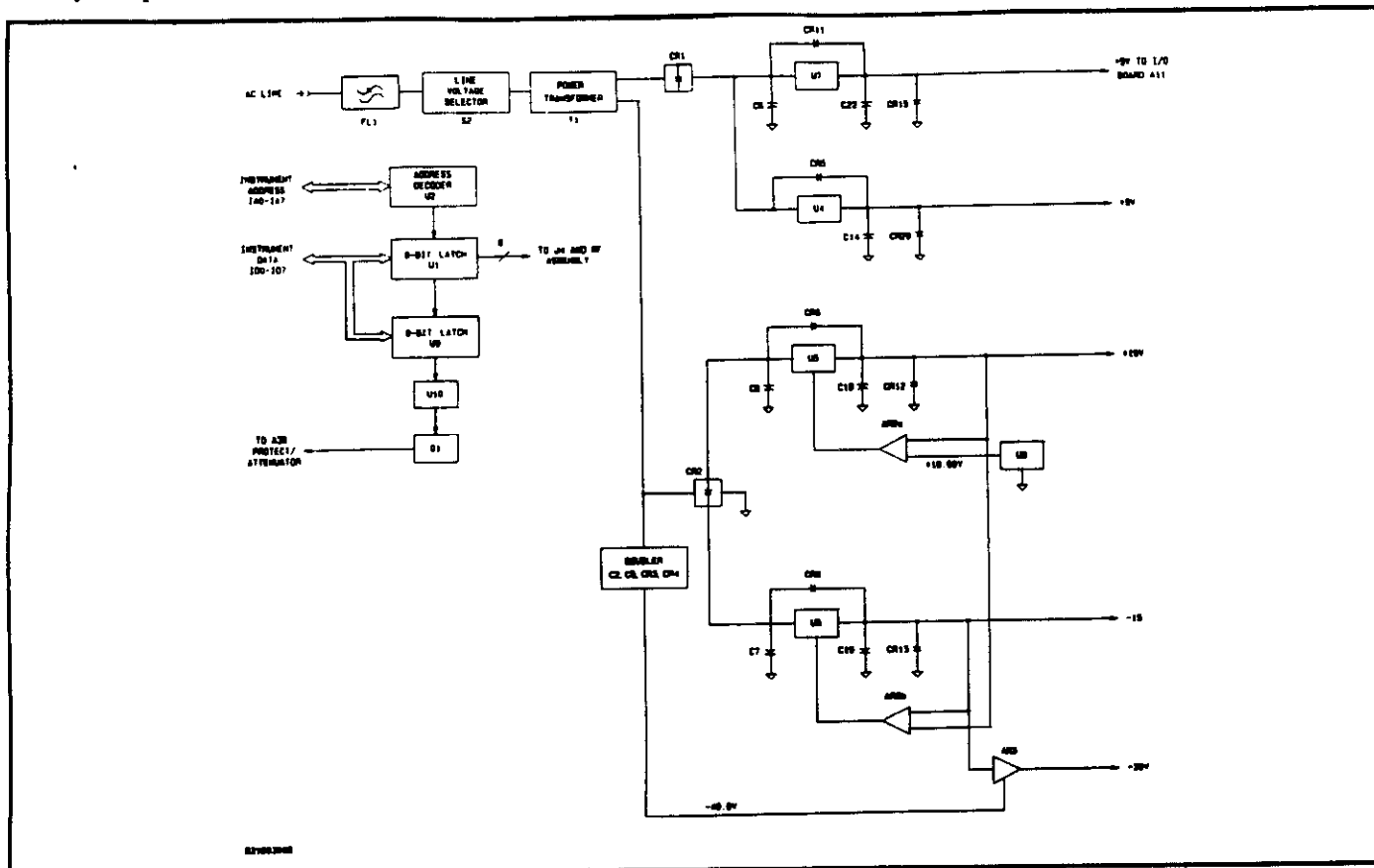


FIGURE 4-14. Motherboard/Power Supply Block Diagram.

4-155. The other secondary winding of T1 is connected through full-wave bridge CR2 to regulators U5 and U6. These regulators are enclosed in feedback loops to improve regulation and increase the operating voltages from 5 to 15 volts. Capacitors C8 and C10 reduce input ripple voltage and CR6, CR8, CR12, and CR13 provide reverse voltage protection. Reference U8 is the primary reference for the power supply circuits. Precision resistors R7a, R7b, and R7d configure AR2a for a gain of +1.5. This converts the +10.00 volt reference into +15.00 volts. R7c and R7f configure AR2b for a gain of -1 which inverts the +15.00 volt supply into -15.00 volts. Zener diodes CR7 and CR9 are required to insure proper startup of the supply and are normally reverse biased when the supply is operating properly. C18 and C19 provide local bypassing to maintain loop stability as the supply loading changes.

4-156. A voltage doubler circuit consisting of C2, C3, CR3, and CR4 produces a dc output of about -40 volts at nominal line. This voltage is regulated to produce a -30 volt level required by the oscillator circuits. R7g and R7h configure AR3 for a gain of exactly +2 which amplifies the -15.00 volt supply to -30.00 volts.

4-157. As a troubleshooting convenience, each supply has an activity LED connected to its output. DS1-DS5 will normally be illuminated when the supplies are operating properly.

4-158. THEORY OF OPERATION, OPTIONAL FILTER BOARD

4-159. The optional filter board, A15, permits three different bandpass filters, and external input connectors to be inserted into the Filter Circuits signal path. Any or all of these options can be installed at one time. See Figures 8-34 through 8-39.

4-160. A signal from the Filter Circuits, A6AR12, is connected via P1, pin 21 to the input pins 12, 22, and 32 of the three optional bandpass filters. This signal is also connected through R2, which establishes a 600 ohm source impedance, and J2 to the rear panel AUDIO OUT connector. Diodes CR1 and CR2 provide reverse power protection.

4-161. The AUDIO IN signal from the rear panel appears at J1. R1 establishes the 1 Megohm input impedance, and R3, CR3, and CR2 provide input over-voltage protection. C1 improves high frequency response. This signal, and the outputs from the three optional filter boards are connected to analog multiplexer U3, a dual 4 input multiplexer. The multiplexer is operated by the control program based on the front panel selection of alternate filter.

4-162. Amplifier U4a is a unity gain buffer which is necessary to provide the last stage of the CCITT filter circuit. U4b is connected to an array of variable and fixed resistors which determine the gain of each selected filter. R5, R6, R10, and R13 are adjusted for nominal gain at the reference frequency for the selected filter.

4-163. A ground connection from each filter assembly (pins 14, 24, and 34) and a 2-circuit jumper between pins 7 and 8 of J3 provide a means of identifying which filter options are installed. These lines are pulled to +5 volts by R4. If one of the filter assemblies is not installed, the signal line associated with that assembly will be at +5 volts. Conversely, if the assembly is installed, the line will be pulled to ground. At power-up the control software checks the state of these lines via programmable array U2, and determines which filters are present.

4-164. U1 is an 8-bit latch which is operated by the control program to select one of the four possible filter connections.

4-165. THEORY OF OPERATION, OPTIONAL 50 MHZ CALIBRATOR CIRCUITS.

4-166. The 50 MHz calibrator circuits provide an accurate output signal to calibrate the Model 8201 carrier LEVEL measurement. See Figure 8-40.

4-167. The output signal is generated by oscillator Q1 and associated components. The circuit oscillates at approximately 50 MHz as controlled by C11, L2 and adjustable capacitor, C12. The circuit is adjusted until the frequency is 50 ± 0.5 MHz. The signal at the junction of C9 and L2 is rectified by CR2 and connected to operational amplifier AR1. A second input to AR1 is provided by precision reference IC1 through adjustable divider R7, R4, and R1 and compensation diode CR1. The error voltage between pins 2 and 3 of AR1 is amplified and applied to varactor CR3, which forms part of a voltage variable divider. This variable signal is connected to the base of Q1 to complete the oscillator feedback loop. The circuit is an automatic gain control which maintains the output voltage at exactly 0.223 volts as determined by the setting of R4.

4-168. Capacitors C9 and C10 provide impedance matching, and R15 determines the output resistance. Inductor L3 is provided to compensate the slightly capacitive output impedance.

SECTION V PERFORMANCE TESTS

5-1. INTRODUCTION.

5-2. The following procedures verify the performance characteristics of the Modulation Analyzer. Detailed tests against specification are included to verify all operational features, including options.

NOTE

A warm-up period of one hour is recommended before detailed testing is started.

5-3. EQUIPMENT REQUIRED.

5-4. Equipment required is listed in Table 5-1. Any equipment which meets the critical specifications may be used for the recommended model.

NOTE

The following procedures assume that the recommended equipment is used. Procedural changes may be required if equipment substitution is made.

5-5. TEST RECORD.

5-6. Each test table contains a test result block. As each test is completed, the results blocks are filled in.

5-7. CALIBRATION INTERVAL.

5-8. The instrumentation should be tested to specification at least once per year.

5-9. INITIAL CALIBRATION.

5-10. Initial calibration is performed before detailed performance testing to insure that all detectors are functioning properly.

5-11. PROCEDURE.

1. Set the LINE ON/OFF switch to ON and depress the LCL/INIT key to initialize the instrument, after the selfcheck program completes.
2. Select SPCL function 30, which calibrates the modulation detectors.
3. Any errors reported during calibration, indicate an operational failure.

TABLE 5-1. RECOMMENDED TEST EQUIPMENT.

INSTRUMENT	CRITICAL SPECIFICATIONS	USAGE		MODEL
		PERFORMANCE EVALUATION	MAINTENANCE	
AM-FM Signal Generator	Frequency Range: 0.01 to 1000 MHz, Level Range: -50 to +19 dBm	X	X	Boonton Model 1021
Synthesizer, CW	Frequency Range: 0.01 to 1300 MHz Residual FM < 1Hz, 3 kHz BW Residual AM < -80 dBc, kHz BW	X	X	Adret Model 7100A
Audio Analyzer	Frequency Range: 20 Hz to 20 kHz Level Range .6 mV to 6 V into 600 ohms Distortion < 0.05%	X	X	Boonton Model 1120
Test Oscillator	Frequency Range: 5Hz to 500 kHz Level Range: 0 to 3 V rms Flatness: +- 0.3 dB	X		Tektronix Model SG502
Spectrum Analyzer	Frequency: 1.2 MHz Resolution BW: 0.1 kHz Frequency span: 1 kHz	X		HP Model 8566B
Modulator	Frequency: 30 MHz Flatness : < 0.3%, 20 Hz to 220 kHz Distortion: < 0.15% at 90 % AM	X		Boonton 96400501A
Low-pass filter	5-pole response, 3dB corner, 50 MHz	X	X	Mini-Circuits NLP-50
RF Calibrator	Frequency: 30.0 MHz, crystal Level Range: -60 to +20 dBm Accuracy: 0.105 dB	X	X	Boonton Model 2520
DC Power Supply	Range: 0.00 to 10.0 volts.	X		Power Designs Model 5015T
Multimeter	Range: 0.001 to 100 volts, dc.		X	Fluke Model 8840A

TABLE 5-1. RECOMMENDED TEST EQUIPMENT CONTINUED.

INSTRUMENT	CRITICAL SPECIFICATIONS	USAGE		MODEL
		PERFORMANCE EVALUATION	MAINTENANCE	
Variac/Line Monitor	20% variation about 100, 120, or 240 Volts	X		Powerstat 3PN116B
Power Meter	Frequency Range: 10 MHz to 1.3 GHz . Accuracy: ± 0.5 dB	X	X	Boonton Model 4220
Network Analyzer	Frequency Range: 10 MHz to 2 GHz .	X		PMI Model 1038-NS20/ 1038-NS207
SWR Autotester	Directivity : 38 dB	X		Wiltron Model 560-97NF50
RF Millivoltmeter ♦	Frequency Range: 100 kHz to 10 MHz . Accuracy: $\pm 2\%$	X		Boonton Model 9200
Precision resistor ♦	Value : 50.00 ohms $\pm 0.1\%$	X		Mepco PME-55
Oscilloscope	Frequency Range: DC to 100 MHz. 0.005 to 50 volts with 10X probes		X	Hewlett-Packard Model 1740A
Bus Analyzer	Real time display of IEEE-488 bus activity.		X	Hewlett-Packard Model 59401A
Milliwatt Test Set ♦	Level Accuracy: ± 0.015 dBm at 0 dBm.	X		Wandel and Golterman EPM-1 with TK-10 probe
Time Standard	Frequency: 10.0000 MHz Stability: 1×10^{-10} per day	X		House Standard
Wave Analyzer	Resolution: 3 Hz bandwidth at 1 kHz. Dynamic Range: > 100 dB		X	Hewlett-Packard Model 3581A

♦ This equipment is required only if calibrator option is installed or for optional VSWR tests.

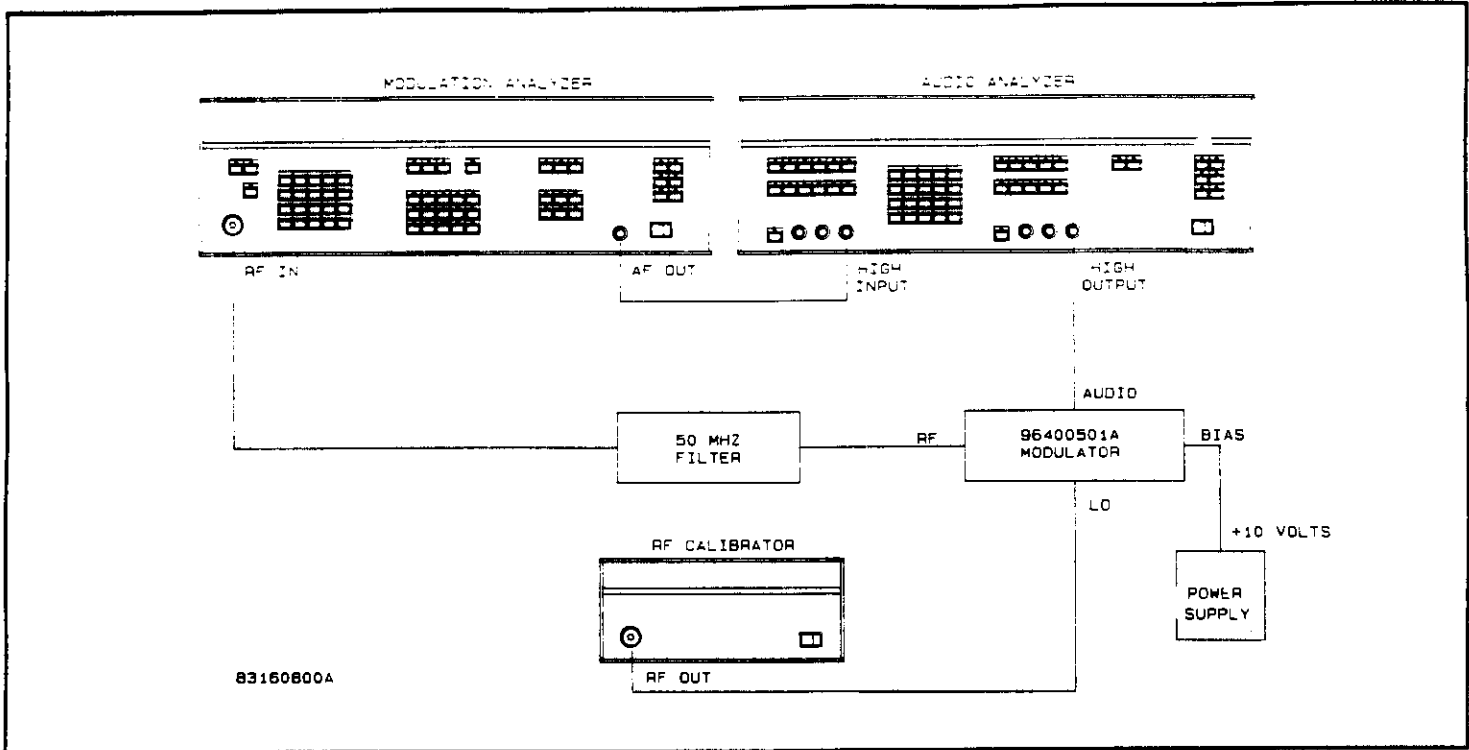


FIGURE 5-1. Measurement Setup #1.

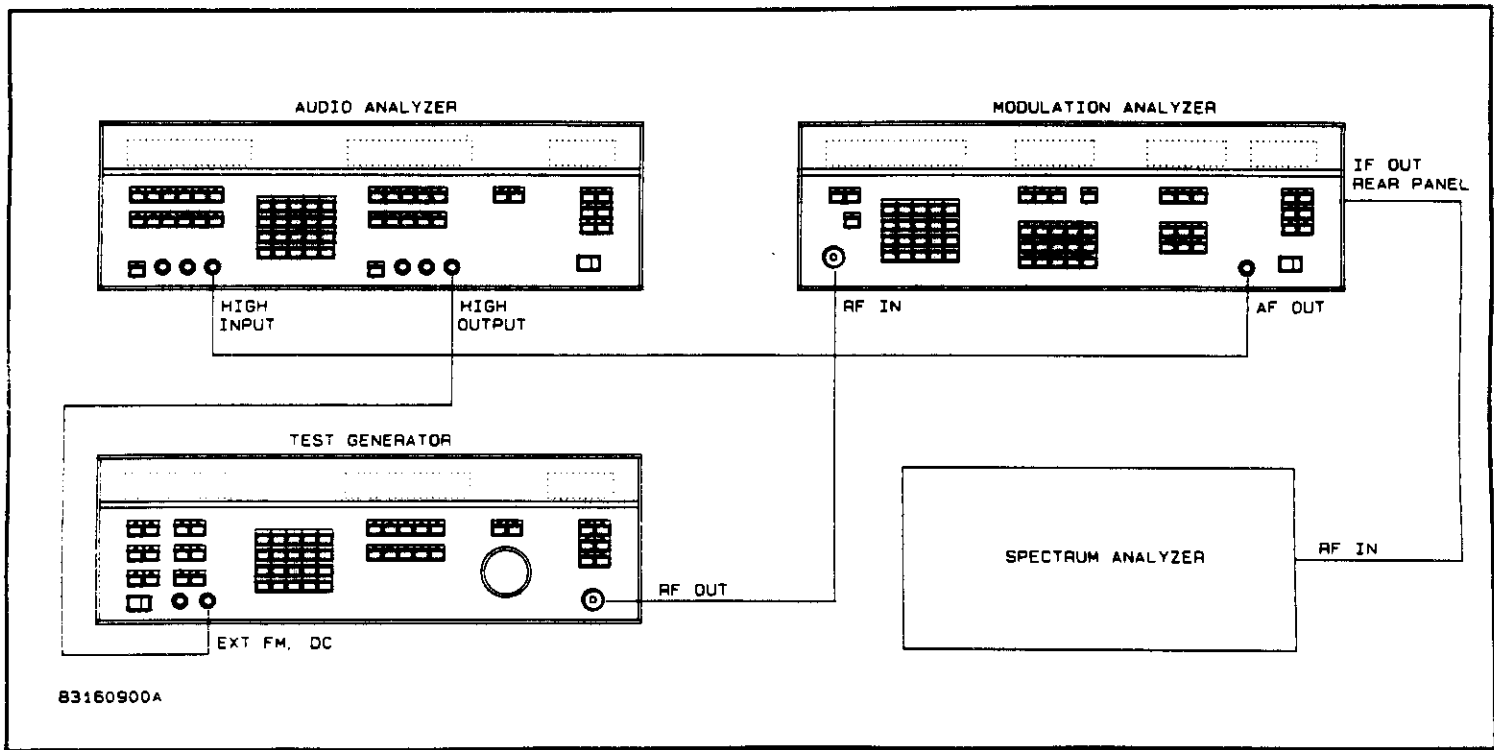


FIGURE 5-2. Measurement Setup #2.

PERFORMANCE TEST 1

AM MODULATION ACCURACY AND RESIDUALS

Specification	: $\pm 1\%$, 30 Hz to 5 kHz, Frf 0.1 to 0.5 MHz
	: $\pm 2\%$, 30 Hz to 7.5 kHz, Frf 0.1 to 0.5 MHz
	: $\pm 1\%$, 30 Hz to 15 kHz, Frf 0.5 to 10 MHz
	: $\pm 2\%$, 30 Hz to 30 kHz, Frf 0.5 to 10 MHz
	: $\pm 1\%$, 30 Hz to 100 kHz, Frf > 10 MHz
	: $\pm 2\%$, 30 Hz to 150 kHz, Frf > 10 MHz
	: residual 0.05%, 15 kHz bandwidth, level > 100 millivolts
	: residual 0.02%, 3 kHz bandwidth, level > 100 millivolts
	: incidental FM 20 Hz peak at 50% AM, 3 kHz bandwidth
: incidental PM 0.02 RAD at 50% AM, 3 kHz bandwidth	

5-12. DESCRIPTION.

5-13. The AM accuracy is verified first by using the internal calibrator which is exactly $50.00\% \pm 0.1\%$ at 1.220 kHz. The AM flatness is then tested by applying the output of a low-residual, wideband linear modulator to the input of the Modulation Analyzer. The Audio Analyzer frequency is then varied, and a modulation RATIO change is noted. The audio frequency is then set to 1 kHz and the incidentals are checked at 50% AM. Finally, the audio signal is removed from the modulator and the residual AM is measured.

5-14. PROCEDURE.

1. Connect the equipment as shown in Figure 5-1. Note that the power supply is set to 10.0 ± 1 volts.
2. Depress the LCL/INIT key to initialize the instrument.
3. Set the RF Calibrator to +10 dBm and turn the output ON.
4. Select the AM modulation mode and depress the CAL key. The calibration routine will display the -CAL- message in the FREQUENCY/LEVEL window and the AM indication in the MODULATION window. Record the modulation indication.
5. Select the <10 high-pass and 220 kHz low-pass filters, and SPCL function 5 to enable the slow detector mode.
6. Adjust the Audio Analyzer for an AM indication of about 47.00% at a 1 kHz rate and select the Modulation Analyzer percent RATIO display mode.

NOTE

The following procedures assume that the Audio Analyzer Level flatness is better than 0.5%. This should be verified before continuing.

7. Set the Audio Analyzer to the test frequencies of Table 5-2 and record the ratio indication.
8. Set the Audio Analyzer to 1 kHz and adjust the LEVEL for an indication of $50 \pm 1\%$ AM. Depress the RATIO key to disable this function.

9. Select the 30 Hz high-pass, the 3 kHz lowpass, and depress the FM modulation key. Increase or decrease the RF Calibrator level for a deviation null, then record the indication.
10. Depress the PM modulation key and record the indication.
11. Remove the Audio Analyzer connection to the Modulator, depress the AM and RMS keys and record the residual AM indication.
12. Select the 15 kHz low-pass filter and record the indication.

Table 5-2. AMPLITUDE MODULATION

FREQUENCY	FILTER SETTING	MINIMUM	ACTUAL	MAXIMUM
30 Hz	220 kHz	99.00	_____	101.00
100 Hz	220 kHz	99.00	_____	101.00
10 kHz	220 kHz	99.00	_____	101.00
50 kHz	220 kHz	99.00	_____	101.00
100 kHz	220 kHz	99.00	_____	101.00
150 kHz	220 kHz	98.00	_____	102.00
Incidental FM	30 Hz-3 kHz		_____	20 Hz
Incidental PM	30 Hz-3 kHz		_____	0.02 RAD
Residual AM	30 Hz -3 kHz		_____	0.02%
Residual AM	30 Hz -15 kHz		_____	0.05%

PERFORMANCE TEST 2

AUDIO FILTERS

Specification : $\pm 4\%$ corner accuracy

5-15. DESCRIPTION.

5-16. Each audio filter of the Modulation Analyzer is tested for corner accuracy by applying the output of a low-noise, wideband modulator to the input of the Modulation Analyzer. The analyzer modulation RATIO measurement mode is used with a reference set at a midband frequency. The frequency of the Audio Modulation Analyzer is then set to the filter corner frequency and the relative amplitude measured and the results recorded.

5-17. PROCEDURE.

1. Connect the equipment as in Fig. 5-1. Note that the power supply is set to 10.0 ± 1 volts.
2. Depress the LCL/INIT key to initialize the instrument, then execute SPCL functions 7 and 9 to set pre-display dc-emphasis, on AM.
3. Set the RF Calibrator to +10 dBm and ON.
4. Adjust the LEVEL of the Audio Analyzer for an indication of about 47.00% at 1 kHz.
5. Select the <10 high-pass and the 220 kHz low-pass filters, and depress the RATIO and % keys to establish a reference modulation.
6. Set the Audio Analyzer test frequency for each high-pass filter in Table 5-3, then depress the key to select the filter, and record the ratio indication.
7. Select the <10 Hz high-pass filter and set the Audio Analyzer test frequency for each de-emphasis filter in Table 5-3. Depress the key to select the filter, and record the ratio indication.
8. Turn the de-emphasis filters off, select the 30 Hz high-pass filter. Set the Audio Analyzer test frequency for each low-pass filter in Table 5-3 except the 50 and 220 kHz, then depress the key to select the filter. Record the ratio indication.
9. For the 50 and 220 kHz filters, connect the Test Oscillator in place of the Audio Analyzer Source in Figure 5-1.
10. Depress the RATIO key and adjust the Test Oscillator amplitude for an indication of about 47.00% AM at 1 kHz rate.
11. Select the 50 kHz low-pass filter, depress the RATIO key and increase the Test Oscillator frequency until the ratio indication is 70.7%. Record the audio FREQ display indication.
12. Select the 220 kHz low-pass and continue to increase the Test Oscillator frequency until the ratio indication is again 70.7%. Record the audio FREQ display indication.

Table 5-3. AUDIO FILTERS

FILTER	SOURCE SETTING	MINIMUM	ACTUAL	MAXIMUM
High-pass:				
< 10Hz	30 Hz	99.50	_____	100.50
30Hz	30 Hz	67.50	_____	73.70
300Hz	300 Hz	67.50	_____	73.70
3000Hz	3000 Hz	67.50	_____	73.70
Dc-emphasis:				
25 μ S	6.366 kHz	67.50	_____	73.70
50 μ S	3.188 kHz	67.50	_____	73.70
75 μ S	2.122 kHz	67.50	_____	73.70
750 μ S	212.2 Hz	67.50	_____	73.70
Low-pass:				
3 kHz	3 kHz	67.50	_____	73.70
15 kHz	15 kHz	67.50	_____	73.70
20 kHz	20 kHz	67.50	_____	73.70
50 kHz	50 kHz approx.	48.00	_____	52.00
220 kHz	220 kHz approx.	211.2	_____	228.8

PERFORMANCE TEST 3

AMPLITUDE MODULATION, DISTORTION

Specification : 0.3% for depths of 90%,

5-18. DESCRIPTION.

5-19. The amplitude modulation distortion is verified by applying the output of a low-residual, wideband, linear modulator to the input of the Modulation Analyzer. The Audio Analyzer level is then adjusted for 90% and the recovered modulation distortion is displayed using the internal distortion analyzer which has to be verified before this test.

5-20. PROCEDURE.

1. Depress the LCL/INIT key to initialize the Modulation Analyzer.
2. Connect the equipment as in Figure 5-1, and select the Modulation Analyzer AM modulation measurement mode.
3. Set the Audio Analyzer to 1 kHz and adjust the level for an AM indication of $90.0 \pm 0.5\%$.
4. Select the audio DIST mode and record the indicated distortion.

Table 5-4. AMPLITUDE MODULATION, DISTORTION

DEPTH	RF FREQUENCY	MINIMUM	ACTUAL	MAXIMUM
90%	30 MHz		_____	0.3%

PERFORMANCE TEST 4

FM MODULATION ACCURACY AND INCIDENTAL AM

Specification	: ± 1%, 30 Hz to 5 kHz, Frf 0.2 to 0.5 MHz
	: ± 2%, 30 Hz to 7.5 kHz, Frf 0.2 to 0.5 MHz
	: ± 1%, 30 Hz to 15 kHz, Frf 0.5 to 10 MHz
	: ± 2%, 30 Hz to 30 kHz, Frf 0.5 to 10 MHz
	: ± 1%, 30 Hz to 100 kHz, Frf > 10 MHz
	: ± 2%, 30 Hz to 150 kHz, Frf > 10 MHz
	: incidental AM 0.2% AM peak at 50kHz peak deviation Frf > 10 MHz
	: incidental AM 0.2% AM peak at 5 kHz peak deviation Frf < 10 MHz

5-21. DESCRIPTION.

5-22. The FM accuracy is verified by using the internal calibrator which is exactly 125.0 kHz \pm 0.1% at a 1.220 kHz rate. The FM flatness is then tested by applying the FM modulated output of the Test Generator to the input of the Modulation Analyzer. The Audio Analyzer frequency is then varied from 30 Hz to 5 kHz, and a modulation RATIO change is noted. Higher audio frequencies are tested by using Bessel null measurements at specific audio frequencies. The audio frequency is then set to 1 kHz and the incidental AM is checked at 50 kHz and 5 kHz deviation.

NOTE

The following procedure is used in lieu of Bessel null measurements. The Bessel zero technique is quite tedious at frequencies below about 1 kHz, as Spectrum Analyzer adjustment is difficult, and eighth order nulls, or higher, must be used to produce enough deviation for reasonable accuracy. The test generator used for the following tests is used over less than one two-hundredth of its modulation bandwidth, and can safely be assumed to be flat.

5-23. PROCEDURE.

1. Connect the equipment as shown in Figure 5-2.
2. Depress the LCL/INIT key to initialize the Modulation Analyzer.
3. Set the Test Generator to 500 MHz, 0 dBm and EXT DC FM.
4. Adjust the Audio Analyzer Source to 0.7 volts at 1 kHz, and program the Test Generator for 50 kHz deviation.
5. Select the Modulation Analyzer FM modulation mode and depress the CAL key. The calibration program will display the FM indication in the MODULATION window during the calibration program. Record the indication.
6. Select the < 10 Hz high-pass and 220 kHz low-pass filters, then adjust the Audio Analyzer LEVEL for an FM indication of about 47.00 kHz at a 1 kHz rate, and depress the RATIO and %/Hz keys to set a modulation reference.

NOTE

The following procedures assume that the Audio Analyzer Level flatness is better than 0.5%. This should be verified before continuing.

7. Set the Audio Analyzer to 30, 100, and 500 Hz and record the ratio indication.

8. Temporarily disconnect the Audio Analyzer from the Test Generator and adjust the Spectrum Analyzer for a full scale indication of the unmodulated carrier. Reconnect the Audio Analyzer signal.
9. On the Modulation Analyzer depress the RATIO key to disable this function, then adjust the Audio Analyzer frequency to 4.1583 kHz. Set the Test Generator to 10 kHz deviation.
10. Observe the Spectrum Analyzer display and, using the Audio Analyzer LEVEL STEP function, adjust for a carrier null of greater than 50 dB. This corresponds to a deviation of exactly 10.00 kHz \pm 0.3%.
11. When the deviation reading settles, select SPCL function 3 to hold the 50.00 modulation range, and temporarily disconnect the the Audio Analyzer from the test generator. Subtract the residual reading from the deviation indication and record the difference.
12. Select SPCL function 1 to resume autoranging, then repeat the above procedure at 41.583 kHz and 100 kHz.
13. Replace the Audio Analyzer in the test setup with the test oscillator and perform the null at 150 kHz. Discount the residual indication as above and record the ratio indication.
14. Select the 30 Hz high-pass and the 3 kHz low-pass filters, and adjust the Test Oscillator for a deviation of 50 kHz peak at a 1 kHz rate. Select the AM modulation measurement of the Modulation Analyzer and record the indication.
15. Change the test generator frequency to 5 MHz, and adjust the Test Oscillator for a deviation of 5 kHz peak at a 1 kHz rate. Select the AM modulation measurement of the Modulation Analyzer and record the indication.

Table 5-5. FREQUENCY MODULATION ACCURACY

FILTER	SOURCE FREQUENCY	MINIMUM	ACTUAL	MAXIMUM
< 10-220 kHz	30 Hz	99.00	_____	101.00
< 10-220 kHz	100 Hz	99.00	_____	101.00
< 10-220 kHz	500 Hz	99.00	_____	101.00
< 10-220 kHz	1000 Hz		Reference	
< 10-50 kHz	4.1583 kHz	9.90	_____	10.10
< 10-220 kHz	41.583 kHz	99.00	_____	101.00
< 10-220 kHz	100 kHz	238.1	_____	242.9
< 10-220 kHz	150 kHz	353.5	_____	367.9
CALIBRATION		123.8	_____	126.3
INCIDENTAL @ 500 MHz			_____	0.2%
INCIDENTAL @ 5 MHz			_____	0.2%

PERFORMANCE TEST 5

FREQUENCY MODULATION, DISTORTION

Specification	: 0.1% for deviations < 30 kHz, Frf 0.2 to 0.5 MHz
	: 0.1% for deviations < 75 kHz, Frf 0.5 to 10 MHz
	: 0.1% for deviations < 100 kHz, Frf > 10 MHz

5-24. DESCRIPTION.

5-25. The Frequency Modulation distortion is verified by applying the output of the Test Generator to the input of the Modulation Analyzer. A small amount of FM deviation is applied to the carrier signal, and the Modulation Analyzer local oscillator frequency is varied. The measurement determines the change of slope of the Frequency Modulation detector. The distortion components are then calculated and compared to the specifications. This technique is extremely sensitive and much easier than finding an FM source of sufficiently low distortion to make the test.

5-26. PROCEDURE.

1. Depress the LCL/INTT key to initialize the Modulation Analyzer.
2. Connect the RF output of the Test Generator to Modulation Analyzer RF IN connector. Set the Generator for 15.211 MHz, 0 dBm, and 3 kHz FM deviation at a 1 kHz rate.
3. Select the 300 Hz high-pass, 3 kHz low-pass, and the RMS detector. Execute SPCL 18 to select the $\sqrt{\text{RMS}}$ detector, and enter 15.0 MHz into the FREQUENCY/LEVEL display.
4. Select the FM modulation mode, and when the reading settles, depress the RATIO and %/Hz keys.
6. Using the DATA keypad, enter the carrier frequencies listed in Table 5-6. Record the ratio indication.

CAUTION

Do not change the Test Generator carrier frequency or FM deviation during this procedure, as large errors will result.

7. The change in indication is small and represents changes in the slope of the FM detector. The second harmonic term is dominant and equal to 1/4 of the change in slope. For example, if the indication at 14.5 MHz was 99.80% and the indication at 15.5 MHz was 100.00%, the slope change would be 0.2% for a + or - 500 kHz deviation. This would indicate a distortion of 0.05%. The difference between indications at 14.9 and 15.1 MHz should be less than 0.4% corresponding to 0.1% distortion for deviations of ± 100 kHz and carriers greater than 10 MHz. The difference between any two indications should be less than 0.4% corresponding to 0.1% distortion for deviations of ± 50 kHz for carriers below 2 MHz. The difference between 14.3 and 14.4 MHz should be less than 0.4% corresponding to 0.1% distortion for deviations of ± 50 kHz for carriers between 2 and 10 MHz.

Table 5-6. FM MODULATION DISTORTION.

FREQUENCY	MINIMUM	ACTUAL	MAXIMUM
14.10 MHz	-0.40	_____	+0.4
14.20 MHz	-0.40	_____	+0.4
14.30 MHz	-0.40	_____	+0.4
14.40 MHz	-0.40	_____	+0.4
14.50 MHz	-0.40	_____	+0.4
14.60 MHz	-0.40	_____	+0.4
14.70 MHz	-0.40	_____	+0.4
14.80 MHz	-0.40	_____	+0.4
14.90 MHz	-0.40	_____	+0.4
15.00 MHz		Reference	
15.10 MHz	-0.40	_____	+0.4
15.20 MHz	-0.40	_____	+0.4
15.30 MHz	-0.40	_____	+0.4
15.40 MHz	-0.40	_____	+0.4
15.50 MHz	-0.40	_____	+0.4
15.60 MHz	-0.40	_____	+0.4
15.70 MHz	-0.40	_____	+0.4
15.80 MHz	-0.40	_____	+0.4
15.90 MHz	-0.40	_____	+0.4
16.00 MHz	-0.40	_____	+0.4

PERFORMANCE TEST 6

FM RESIDUALS, 3 and 15 kHz FILTERS

Specification	: < 15 Hz rms at 2000 MHz, 3 kHz bandwidth
	: < 7.5 Hz rms at 1000 MHz, 3 kHz bandwidth (linear decrease)
	: < 1 Hz rms at 100 MHz, 3 kHz bandwidth (floor)
	: < 30 Hz rms at 2000 MHz, 15 kHz bandwidth
	: < 15 Hz rms at 1000 MHz, (linear decrease)15 kHz bandwidth
	: < 2 Hz rms at 100 MHz, 15 kHz bandwidth (floor)

5-27. DESCRIPTION.

5-28. The FM residual modulation is determined by applying the output of a low-noise Synthesizer to the input of the Modulation Analyzer and noting the modulation indication using the rms detector.

5-29. PROCEDURE.

1. Depress the LCL/INIT key to initialize the Modulation Analyzer.
2. Connect output of the Synthesizer to the RF IN connector of the Modulation Analyzer. Set the Synthesizer to 2 GHz and 0 dBm. Depress the RMS key, and when the reading settles, record FM deviation.
3. Change the low-pass filter setting to 3 kHz and record the FM deviation.
4. Change the Synthesizer frequency to 1000 MHz and record the FM deviation.
5. Change the low-pass filter setting to 15 kHz and record the FM deviation.
6. Change the Synthesizer frequency to 100 MHz and record the FM deviation.
7. Change the low-pass filter setting to 3 kHz and record the FM deviation.

Table 5-7. FREQUENCY MODULATION, RESIDUALS.

FILTER	TEST FREQUENCY	MINIMUM	ACTUAL	MAXIMUM
15	2000 MHz		_____	30 Hz
3	2000 MHz		_____	15 Hz
3	1000 MHz		_____	7.5 Hz
15	1000 MHz		_____	15 Hz
15	100 MHz		_____	2 Hz
3	100 MHz		_____	1 Hz

PERFORMANCE TEST 7

PHASE MODULATION, ACCURACY AND FLATNESS

Specification	: $\pm 3\%$ 200 Hz to 7.5 kHz, Frf 0.2 to 0.5 MHz
	: $\pm 3\%$ 200 Hz to 30 kHz, Frf > 0.5 MHz

5-30. DESCRIPTION.

5-31. The Modulation Analyzer measures Phase modulation by integrating the output of the FM detector, as this is the mathematical relationship of phase and frequency. The PM accuracy is first verified by calibrating the phase detection system with the internal calibrator. The detector flatness is then measured by applying known amounts of FM deviation and comparing the equivalent PM. PM deviation is equal to the FM deviation divided by the modulation rate.

5-32. PROCEDURE.

1. Complete the FM system performance tests, this will verify FM flatness and FM and PM distortion, then connect the equipment as in Fig. 5-2, but omit the Spectrum Analyzer.
2. Select PM, PEAK \pm detector, 30 Hz high-pass, and 50 kHz lowpass filters. Depress the CAL key to calibrate the PM measurement.
3. Set the Test Generator to 100 MHz, 0 dBm, and FM EXT DC.
4. Depress the Modulation Analyzer FM key, set the Audio Analyzer Source frequency to 1 kHz and adjust the LEVEL for a deviation of 50.00 kHz.
5. Depress the Modulation Analyzer PM key and record the deviation.
6. Depress the Modulation Analyzer FM key, set the Audio Analyzer Source frequency to 200.0 Hz and adjust the LEVEL for a deviation of 50.00 kHz.
7. Depress the Modulation Analyzer PM key and record the deviation.
8. Depress the Modulation Analyzer FM key, the 300 Hz high-pass filter, set the Audio Analyzer Source frequency to 30.0 kHz and adjust the LEVEL for a deviation of 50.00 kHz.
9. Depress the Modulation Analyzer PM key and record the deviation.

Table 5-8. PHASE MODULATION, ACCURACY AND FLATNESS.

CARRIER FREQUENCY	SOURCE SETTING	MINIMUM	ACTUAL	MAXIMUM
100 MHz	1 kHz	48.50	_____	51.50
100 MHz	200.0 Hz	242.7	_____	257.5
100 MHz	30.0 kHz	1.62	_____	1.72

Table 5-9. DISTORTION ANALYZER, ACCURACY.

AUDIO ANALYZER	TEST OSCILLATOR	MINIMUM	ACTUAL	MAXIMUM
1 kHz	2 kHz	-39.0	_____	-41.0
20 Hz	40 Hz	-39.0	_____	-41.0
20 kHz	40 kHz	-39.0	_____	-41.0

PERFORMANCE TEST 8

DISTORTION ANALYZER

Specification	: $\pm 10\%$ or 1 dB SINAD : residual distortion < 0.1% (60 dB SINAD)
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5-33. DESCRIPTION.

5-34. The distortion analyzer is tested by applying a synthetically generated distortion reference signal to the Modulation Analyzer FM and audio circuits. This signal is generated by accurately combining the outputs of two audio sources with levels set exactly 40 dB apart to obtain a calibrated distortion indication.

5-35. PROCEDURE.

1. Set the output impedance of the Audio Analyzer and the Audio generator to 50 ohms and connect them together using a 'TEE' connector to the EXT FM input of the Test Generator.
2. Set the Test Generator to 100 MHz, 0 dBm, and EXT DC FM.
3. Connect the Test Generator output to the Modulation Analyzer RF IN connector.
4. Depress the LCL/INTT key to initialize the Modulation Analyzer.
5. Set the Audio Analyzer LEVEL to 0 volts (OFF) and the Audio Generator to 1 kHz and about 0.7 volts.
6. Adjust the Audio Generator LEVEL until the MODULATION display indicates about 45.00 kHz, then depress the Modulation Analyzer RATIO key to set a reference.
7. Turn OFF the Audio generator and adjust the Audio Analyzer level until the indication is 100.0 % at 2 kHz rate.
8. Turn on the Audio generator and reduce the level of of the Audio Analyzer exactly 100 times (-40 dB).
9. Depress the Modulation Analyzer SINAD key and record the settled reading.
10. Depress < 10 Hz high-pass key and repeat the procedure at 20 Hz (Audio Analyzer at 40 Hz).
11. Depress 50 kHz low-pass key and repeat the procedure at 20 kHz (Audio Analyzer at 40 kHz).

PERFORMANCE TEST 9

CARRIER LEVEL

Specification	: ± 1 dB, 0.1 to 520 MHz, -47 to +30 dBm
	: ± 2 dB, 520 to 1500 MHz, -37 to +30 dBm
	: ± 3 dB, 1500 to 2500 MHz, -33 to +30 dBm

5-36. DESCRIPTION.

5-37. The carrier LEVEL measurement is verified by applying the output of the RF Calibrator to the RF IN of the Modulation Analyzer and calibrating the measurement. The RF calibrator is then used to verify performance at 30 MHz. An accurate power meter is then used to verify the accuracy at other frequencies.

5-38. PROCEDURE.

1. On the Modulation Analyzer, depress the LCL/INIT key to initialize the system.
2. Connect the RF Calibrator output to the RF IN connector of the Modulation Analyzer and set the RF Calibrator to 0 dBm and ON.
3. Enter 0 dBm into the carrier LEVEL display, then depress the CAL key to calibrate the measurement.
4. When the calibration routine completes, depress the carrier FREQ and MHZ keys to hold the frequency setting.
5. Depress the carrier LEVEL key and record the indications for the RF Calibrator levels listed in Table 5-10.
6. Connect the Reference Power Meter sensor to the output of the Test Generator using the same cable that is used to connect the Generator to the Modulation Analyzer.
7. Set the Test Generator to 1000 MHz and to the Test levels indicated in Table 5-10. Record the indications.

NOTE

Start the procedure at the highest level to insure that the Modulation Analyzer properly acquires the signal before depressing the MHZ key.

8. Without changing any settings, disconnect the Reference Power Meter and connect the Test Generator to the Modulation Analyzer.
9. On the Modulation Analyzer depress the carrier FREQ and AUTO keys to acquire the signal. When the frequency reading settles, depress the MHZ key to hold the measurement frequency.
10. Depress the LEVEL key and record the indications at the indicated test levels.
11. Repeat the procedure at 2000 MHz.

Table 5-10. CARRIER LEVEL ACCURACY.

FREQUENCY	TEST LEVEL	MINIMUM	ACTUAL	MAXIMUM
30 MHz	0 dBm		REFERENCE	
30 MHz	-47.0 dBm	-48.0	_____	-46.0
30 MHz	-10.0 dBm	-11.0	_____	-9.0
30 MHz	+10.0 dBm	+9.0	_____	+11.0
30 MHz	+19.0 dBm	+18.0	_____	+20.0
1000 MHz	0 dBm	-2.0	_____	+2.0
1000 MHz	-37.0 dBm	-39.0	_____	-35.0
1000 MHz	-10.0 dBm	-12.0	_____	-8.0
1000 MHz	+10.0 dBm	+8.0	_____	+12.0
1000 MHz	+19.0 dBm	+17.0	_____	+21.0
2000 MHz	0 dBm	-3.0	_____	+3.0
2000 MHz	-33.0 dBm	-36.0	_____	-30.0
2000 MHz	-10.0 dBm	-13.0	_____	-7.0
2000 MHz	+10.0 dBm	+7.0	_____	+13.0

PERFORMANCE TEST 10

FREQUENCY ACCURACY AND SENSITIVITY

Specification

: reference ± 3 counts Frf < 100 MHz
 : reference ± 3 counts or 30 Hz whichever is greatest, Frf > 100 MHz
 : sensitivity 10 mV rms, Frf < 520 MHz
 : sensitivity 15 mV rms, Frf < 1000 MHz
 : sensitivity 28 mV rms, Frf < 1500 MHz
 : sensitivity 50 mV rms, Frf > 1500 MHz

5-39. DESCRIPTION.

5-40. Carrier frequency accuracy is measured by locking the Test Generator to a timebase with 1×10^{-10} stability and known accuracy, then applying the output of the generator to the input of the Modulation Analyzer. Frequency readings are taken at various frequencies and levels and the indications recorded. The test also verifies the measurement sensitivity, and audio frequency accuracy, as the same counter and timebase are used.

5-41. PROCEDURE.

1. Connect the EXT REF input of the Test Generator to the output of the Metrology Standard timebase.
2. Connect the Test Generator output to the Modulation Analyzer RF IN connector and set the frequency to 500 kHz and level to 10 mV. Record the settled reading.
3. Increase the Test Generator frequency to 520 MHz. Record the settled reading.
4. Increase the Test Generator frequency to 1000 MHz, and increase the level to 15 millivolts. Record the settled reading.
5. Increase the Test Generator frequency to 1500 MHz, and increase the level to 28 millivolts. Record the settled reading.
5. Increase the Test Generator frequency to 2000 MHz, and increase the level to 50 millivolts. Record the settled reading.

Table 5-11. CARRIER FREQUENCY ACCURACY AND SENSITIVITY

TEST LEVEL	FREQUENCY	MINIMUM	ACTUAL	MAXIMUM
10mV	.500000 MHz	.49997	_____	.50003
10mV	520.00000 MHz	519.9997	_____	520.0003
15mV	1000.00000 MHz	999.9997	_____	1000.0003
28mV	1500.00000 MHz	1499.9997	_____	1500.0003
50mV	2000.00000 MHz	1999.9997	_____	2000.0003

PERFORMANCE TEST 11

VSWR

Specification	: < 1.5 from 100 kHz to 2.0 GHz. : < 1.8 from 2.0 to 2.5 GHz.
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5-42. DESCRIPTION.

5-43. The Modulation Analyzer VSWR is verified by measuring return loss. Measurements are made using a Scalar Network Analyzer from 10 MHz to 2.5 GHz. For optional testing below 10 MHz, the sensor input impedance is measured at several points and the VSWR is calculated.

5-44. PROCEDURE.

1. Set up the Scalar Analyzer for a 10 MHz to 2.5 GHz sweep at a 0 dBm level, and calibrate the SWR autotester using the reference open and short to establish a return loss baseline.
2. Connect SWR autotester test port to the RF IN connector of the Modulation Analyzer, and connect the SWR autotester to the Scalar Analyzer sweep generator with a short low VSWR cable.
3. Enter 100 MHz into the carrier FREQ display to keep the Modulation Analyzer local oscillator frequency constant, and record the minimum return loss from 0.01 to 2.5 GHz.

NOTE

The following procedure is optional as the Modulation Analyzer input impedance below 10 MHz is essentially the same as the DC resistance of the input protection pad and termination.

4. Connect the equipment as in Figure 5-3, page 5-22.
5. Set the voltmeter to display the ratio of the two channels, and vary the generator frequency from 0.1 to 10 MHz at 0 dBm and record maximum amplitude variation in Table 5-12. This variation represents the impedance variation at the RF IN connector. A ratio of -7.96 dB represents 33.3 ohms resistance, and -4.43 dB represents 75 ohms.

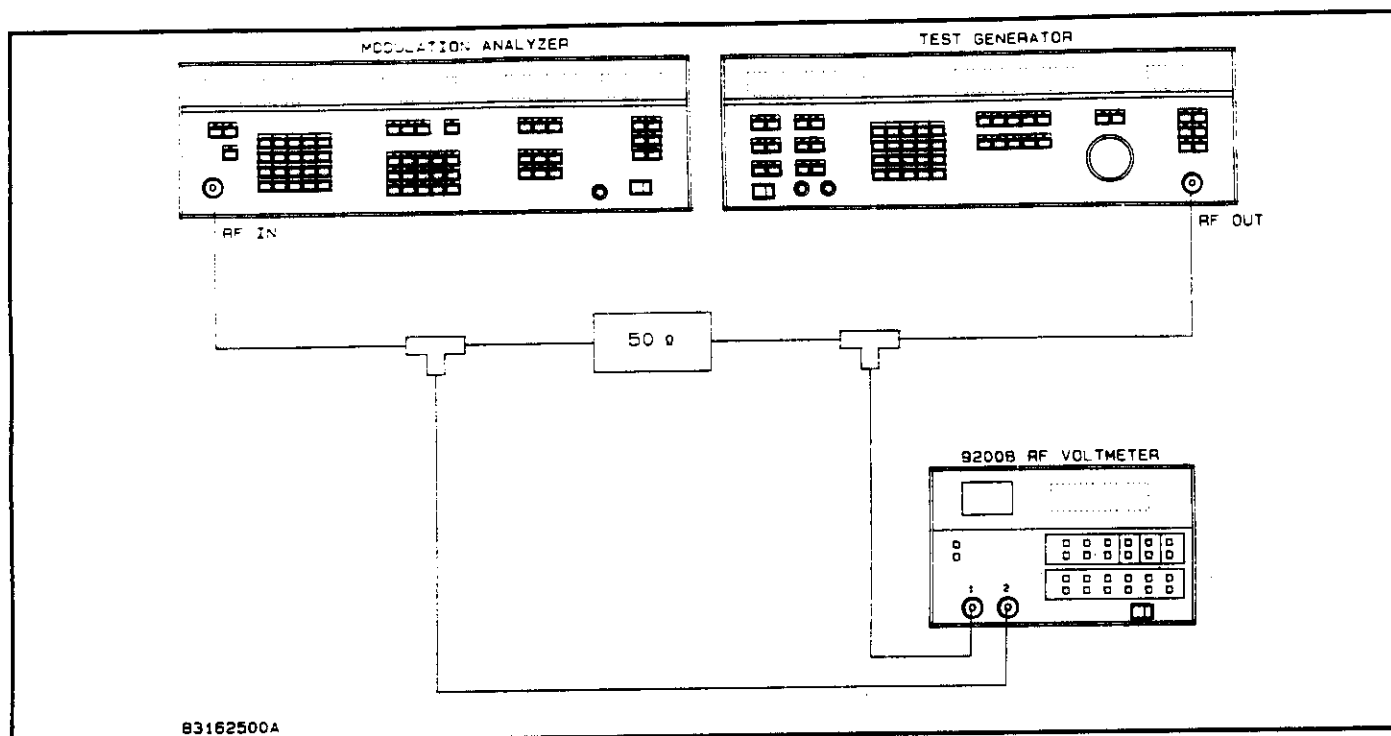


FIGURE 5-3. Measurement Setup #3.

Table 5-12. VSWR

FREQUENCY RANGE	MINIMUM	ACTUAL	MAXIMUM
2.0 GHz - 2.5 GHz	10.9 dB	_____	
10 MHz - 2.0 GHz	13.9 dB	_____	
100 kHz - 10 MHz	-7.96 dB	_____	-4.43 dB *

*VSWR AND IMPEDANCE: VSWR = 1.5, RHO = 0.2, Z_{max} = 75 ohms, Z_{min} = 33.3 ohms

PERFORMANCE TEST 12

CALIBRATORS

Specification	: FM, 0.1% accuracy : AM, 0.1% accuracy
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5-45. DESCRIPTION.

5-46. The theory of operation of the calibrators is described in detail, and the mathematical procedures used to determine the accuracy of the calibrators is disclosed. Since the calibrators are so precise, measurement verification of the stated accuracy is not practical. The following discussion presents the design constraints and the implied accuracy.

5-47. DISCUSSION.

5-48. The internal calibrators of the Modulation Analyzer provide modulation standards for AM and FM measurements; they are activated by the operator as required by the measurement.

5-49. FM CALIBRATION.

5-50. The calibration process consists of (1st) applying to the FM discriminator, in alternation, two accurately controlled frequencies; (2nd) measuring the resulting recovered modulation information; and (3rd) computing a correction factor for subsequent FM measurements. As an aid in following this discussion refer to Figure 8-25.

5-51. The input signal to pin 2 of U23 is the internal timebase frequency divided by two: $5.000 \text{ MHz} \pm 0.01\%$. The preset inputs, P0 through P3 are alternately programmed to divide by 4 or 5, depending on the sense of the signal on pins 3 and 4 of U23. This latter signal is generated by dividing the 5.00 MHz signal by 4096. The resulting signal is phase coherent with the other generated signals and at a frequency of 1.2207 kHz.

5-52. When the preset inputs of U23 are programmed to divide by 5, the resulting signal frequency is 1.000 MHz. Similarly, when the preset inputs are programmed to divide by 4, the resulting frequency is 1.2500 MHz. The average frequency, therefore, is 1.125 MHz; the peak-to-peak deviation is 250 kHz, and the peak deviation is 125.0 kHz.

5-53. From the above discussion it is clear that the frequency deviation is precisely defined by the clock frequency. Additionally, since the modulation signal is phase coherent with the carrier frequency, switching from one carrier tone to the other is consistent.

5-54. In transferring the calibrator deviation to subsequent modulation measurement the primary limitation is the voltmeter resolution, in this case 1 part in 1250 or 0.08%. FM noise is of little or no consequence, since the two frequencies are crystal controlled. The calibration program accumulates ten readings, and averages them to eliminate last-digit uncertainty.

5-55. Cross-correlation measurements using a Bessel null techniques indicate that the actual calibration uncertainty for 100 calibrations is close to 0.04% or one-half digit.

5-56. AM CALIBRATION.

5-57. The operation of the AM calibrator is similar to that of the FM calibrator.

5-58. During AM calibration the fixed divide by two output of U22 is used to generate the carrier frequency of 1.25 MHz. The TTL signal from U24 pin-7 is passed through a low-pass filter consisting of L5, L6 C17, C18, and C20. This filter removes

harmonic of the TTL signal to produce a sinewave at the input of AR3.

5-59. An attenuator AR3 increases the signal level, but more importantly provides a very low output impedance to drive precision divider R20. The increased level also reduces the effects of charge injection in switch, U21.

5-60. The voltage divider comprising R20a through R20d is a precision resistor array. The absolute value of the resistors, however, is not as important as is the match between them. Thus, resistors R20a through R20d are guaranteed to a 0.05% match. Selecting the 3/4 and 1/4 voltage taps for the output insures that the source impedance for subsequent circuits is constant.

5-61. Analog switch U21 alternately switches between the 3/4 and 1/4 voltage taps at the 1.2207 kHz rate, thus producing an amplitude modulated signal with a depth of exactly 50%.

5-62. The effects of the inevitable variation in analog switch on resistance (U21) is obviated by inserting a 20 kohm resistor in series with the switch, thus reducing switch matching errors to less than 0.1%.

5-63. A possible source of error in transferring the calibrator AM accuracy to the measurement is the symmetry of the modulation waveform. The problem is addressed as follows: (In the following analysis, p+ indicates + peak and p- is -peak.)

$$\%p+ = (E_{max} - E_{avg})/E_{avg} \times 100 \quad (1)$$

$$\%p- = (E_{max} - E_{min})/E_{avg} \times 100 \quad (2)$$

$$\text{peak average} = (p+ - p-)/2 \times 100 \quad (3)$$

Therefore, combining Eqs. 1, 2, and 3, for symmetrical modulation,

$$\%AM = (E_{max} - E_{min})/(E_{max} + E_{min}) \times 100 \quad (4)$$

and for the above system:

$$\begin{aligned} \%AM &= (3/4 - 1/4)/(3/4 + 1/4) \times 100 \\ &= 50.00 \end{aligned}$$

5-64. The above calculations assume that the modulation is symmetrical (i.e. perfectly so). Should that not be the case, a dc shift occurs and the plus and minus peaks are not equal. The calibrator program eliminates such an error by calculating AM as:

$$\%AM = (p+ + 3p-)/4 \quad (5)$$

This expression is determined as follows:

Now, since the peak detectors are ac coupled (see figure for symbols),

$$(p+)(T1) - (p-)(T2) = 0 \quad (0 \text{ volts dc}) \quad (6)$$

And:

$$T1 + T2 = 1 \quad (7)$$

$$(p+)(T1) - (p-)(1-T1) = 0 \quad (8)$$

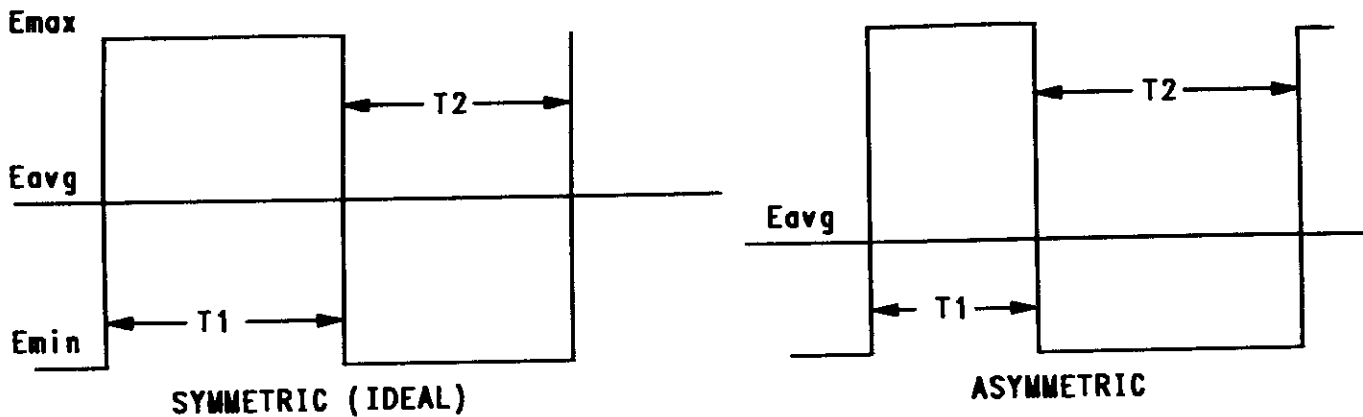
$$T1 = p-/(p+ + p-) \quad (9)$$

Now:

$$E_{avg} = E_{min} + (E_{max} - E_{min}) T1/(T1 + T2) \quad (10)$$

And in the Modulation Analyzer:

$$E_{max} = 3 E_{min} \quad (11)$$



Combining Eqs. 7, 10, and 11:

$$E_{avg} = E_{min} + 2E_{min} (T1) \tag{12}$$

$$E_{avg} = E_{min} (1 + 2T1) \tag{13}$$

If symmetry is perfect:

$$T1 = 0.5 \text{ and } E_{avg} = 2E_{min} \tag{14}$$

If symmetry is less than perfect, the dc ratio error R (that is, Eq. 13 vs Eq. 14) will be:

$$R = (1 + 2T1)/2 \tag{15}$$

Combining Eqs. 9 and 15:

$$R = (p+ + 3p-)/(2 (p+ + p-)) \tag{16}$$

The uncorrected AM is

$$(p+ + p-)/2 \tag{17}$$

and corrected is

$$= (p+ + p-)/2 \times R \tag{18}$$

$$= (p+ + 3p-)/4 \tag{19}$$

5-65. Again, it should be noted that only ratios are involved in the above analysis. The absolute value of the voltages are not important to the method. As in the case of FM, the calibration program accumulates ten readings, and averages them to eliminate last digit uncertainty. The internal voltmeter can resolve the reading to 1 part in 5000 for a quantizing uncertainty of 0.02%. AM noise is of little consequence in determining calibrator depth since the original signal level is determined by TTL gates and the frequency of the carrier and modulation signals are crystal controlled.

5-66. Cross-correlation measurements using a specially calibrated Modulation Analyzer indicate that the actual calibration uncertainty for 100 calibrations is approximately 0.15%.

PERFORMANCE TEST 13

OPTIONAL FILTERS

Specification : See Tables 5-13, 5-14, and 5-15.

5-67. DESCRIPTION.

5-68. Each optional filter is tested for passband gain accuracy by applying the output of a low-noise, wideband modulator to the input of the Modulation Analyzer. The Audio Analyzer Level RATIO measurement mode is used with a reference set at a specific frequency. The frequency of the Audio Analyzer is then varied, and the relative amplitude measured and the results recorded.

5-69. PROCEDURE.

1. Connect the equipment as in Fig. 5-1. Note that the power supply is set to 10 ± 1 volts.
2. Depress the LCL/INIT key to initialize the instrument.
3. Set the RF Calibrator to +10 dBm and ON.
4. Depress the AM and RMS keys, and execute SPCL 18 to select the $\sqrt{\text{RMS}}$ detector.
5. Adjust the LEVEL of the Audio Analyzer Source for an indication of about 47.00% at the reference frequency from Tables 5-13 through 5-15 for the selected filter.
6. Depress the Audio Analyzer LEVEL, RATIO, and dB keys to establish a 0 dB reference level.
7. Select the appropriate optional filter(s), enter the Audio Analyzer test frequencies from Tables 5-13 through 5-15 for the selected filter, and record the RATIO indication.
8. Repeat the above procedure for each installed filter.

Table 5-13. CCITT BANDPASS FILTER.

SOURCE SETTING	MINIMUM	ACTUAL	MAXIMUM
800 Hz		REFERENCE	
50 Hz	-65.0	_____	-61.0
100 Hz	-43.0	_____	-39.0
200 Hz	-23.0	_____	-19.0
300 Hz	-11.6	_____	-9.6
400 Hz	-7.3	_____	-5.3
800 Hz	-0.2	_____	+0.2
1000 Hz	0.0	_____	+2.0
1200 Hz	-1.0	_____	+1.0
1600 Hz	-2.7	_____	-0.7
2000 Hz	-4.0	_____	-2.0
3000 Hz	-6.6	_____	-4.6
3500 Hz	-10.5	_____	-6.5
4000 Hz	-18.0	_____	-12.0
5000 Hz	-39.0	_____	-33.0

Table 5-14. C-MESSAGE BANDPASS FILTER.

SOURCE SETTING	MINIMUM	ACTUAL	MAXIMUM
1000 Hz		REFERENCE	
60 Hz	-57.7	_____	-53.7
100 Hz	-44.5	_____	-40.5
200 Hz	-27.0	_____	-23.0
300 Hz	-17.5	_____	-15.5
400 Hz	-12.4	_____	-10.4
800 Hz	-2.5	_____	-0.5
1000 Hz	-0.2	_____	+0.2
1200 Hz	-1.2	_____	+0.8
1500 Hz	-2.0	_____	0.0
2500 Hz	-2.4	_____	-0.4
3000 Hz	-3.5	_____	-1.5
3500 Hz	-9.6	_____	-5.6
4000 Hz	-17.5	_____	-11.5
5000 Hz	-31.5	_____	-25.5

Table 5-15. CCIR BANDPASS FILTER.

SOURCE SETTING	MINIMUM	ACTUAL	MAXIMUM
1000 Hz		REFERENCE	
31.5 Hz	-30.0	_____	-28.0
63 Hz	-24.9	_____	-22.9
100 Hz	-20.8	_____	-18.8
200 Hz	-14.3	_____	-13.3
400 Hz	-8.3	_____	-7.3
800 Hz	-2.4	_____	-1.4
1000 Hz	-0.5	_____	+0.5
2000 Hz	+5.1	_____	+6.1
3150 Hz	+8.5	_____	+9.5
4000 Hz	+10.0	_____	+11.0
5000 Hz	+11.2	_____	+12.2
6300 Hz	+12.0	_____	+12.4
7100 Hz	+11.8	_____	+12.2
8000 Hz	+11.0	_____	+11.8
9000 Hz	+9.7	_____	+10.5
10.0 kHz	+7.7	_____	+8.5
12.5 kHz	-1.0	_____	+1.0
14.0 kHz	-6.3	_____	-4.3
16.0 kHz	-12.7	_____	-10.7
20.0 kHz	-23.2	_____	-21.2
31.5 kHz	none	_____	-40.7

PERFORMANCE TEST 14

OPTIONAL POWER REFERENCE

Specification	: 50 MHz, \pm 0.5 MHz
	: 0.7% initial accuracy
	: \pm 1.2% over 1 year

5-70. DESCRIPTION.

5-71. The Milliwatt Test Set is first zeroed, and then connected to the Modulation Analyzer 50 MHz power calibrator. The deviation from 0.00 dBm is noted. Then the 50 MHz power calibrator output is connected to the Modulation Analyzer RF IN and the frequency is measured.

5-72. PROCEDURE.

1. Connect the EPM-1 probe to the Milliwatt Test Set reference output with the range set to 0 dBm and resistance set to 50 ohms. Adjust the calibration control for a zero indication.
2. Connect the EPM-1 probe to the PWR REF output on the rear panel of the Modulation Analyzer.
3. Record the deviation from 0.00 dBm in Table 5-16.
4. Connect the PWR REF output on the Modulation Analyzer to the RF IN connector with a suitable cable and select FREQ and AUTO to measure the frequency. Record the calibrator frequency in Table 5-16.

Table 5-16. POWER REFERENCE.

TEST	MINIMUM	ACTUAL	MAXIMUM
Accuracy	-0.05 dB	_____	+ 0.05 dB
Frequency	49.5 MHz	_____	50.5 MHz

SECTION VI MAINTENANCE

6-1. INTRODUCTION.

6-2. This section contains maintenance and adjustment instructions for the Model 8201 Modulation Analyzer.

6-3. SAFETY REQUIREMENTS.

6-4. Although this equipment has been designed in accordance with international safety standards, general safety precautions must be observed during all phases of operation, service and repair of the instrument. Failure to comply with the precautions listed in the Safety Summary located at the front of this manual or with specific warnings given throughout this manual could result in serious injury or death. Service and adjustments should be performed only by qualified service personnel.

6-5. REQUIRED TEST EQUIPMENT.

6-6. Test equipment required for maintenance and adjustments is listed with each procedure. For critical specifications see Table 5-1. Equipment of equivalent characteristics may be substituted for an item listed. An extender board is included in the Model 8201 to facilitate repair and adjustment of the plug-in circuit boards.

6-7. CLEANING PROCEDURE.

6-8. Painted surfaces can be cleaned with a commercial, spray-type window cleaner or with a mild soap and water solution.

CAUTION

Avoid the use of chemical cleaning agents which might damage the plastics used in the instrument. Recommended cleaning agents are isopropyl alcohol, a solution of 1 part kelite and 20 parts water, or a solution of 1% mild detergent and 99% water.

6-9. MAJOR ASSEMBLY LOCATION.

6-10. See Figures 6-1 and 6-2 for the location of the major assemblies of the Model 8201. Coaxial connectors are identified by color coded heat shrink attached to the connectors.

6-11. REMOVAL OF MAJOR ASSEMBLIES AND PARTS.

6-12. **Instrument Covers.** To remove the instrument covers proceed as follows:

1. Disconnect all signal cables and the power cord from the Model 8201.
2. Remove the top cover by removing three No. 6 screws at the rear of the cover and lifting the cover up and to the rear.
3. Turn the instrument over and remove the bottom cover in a similar manner.

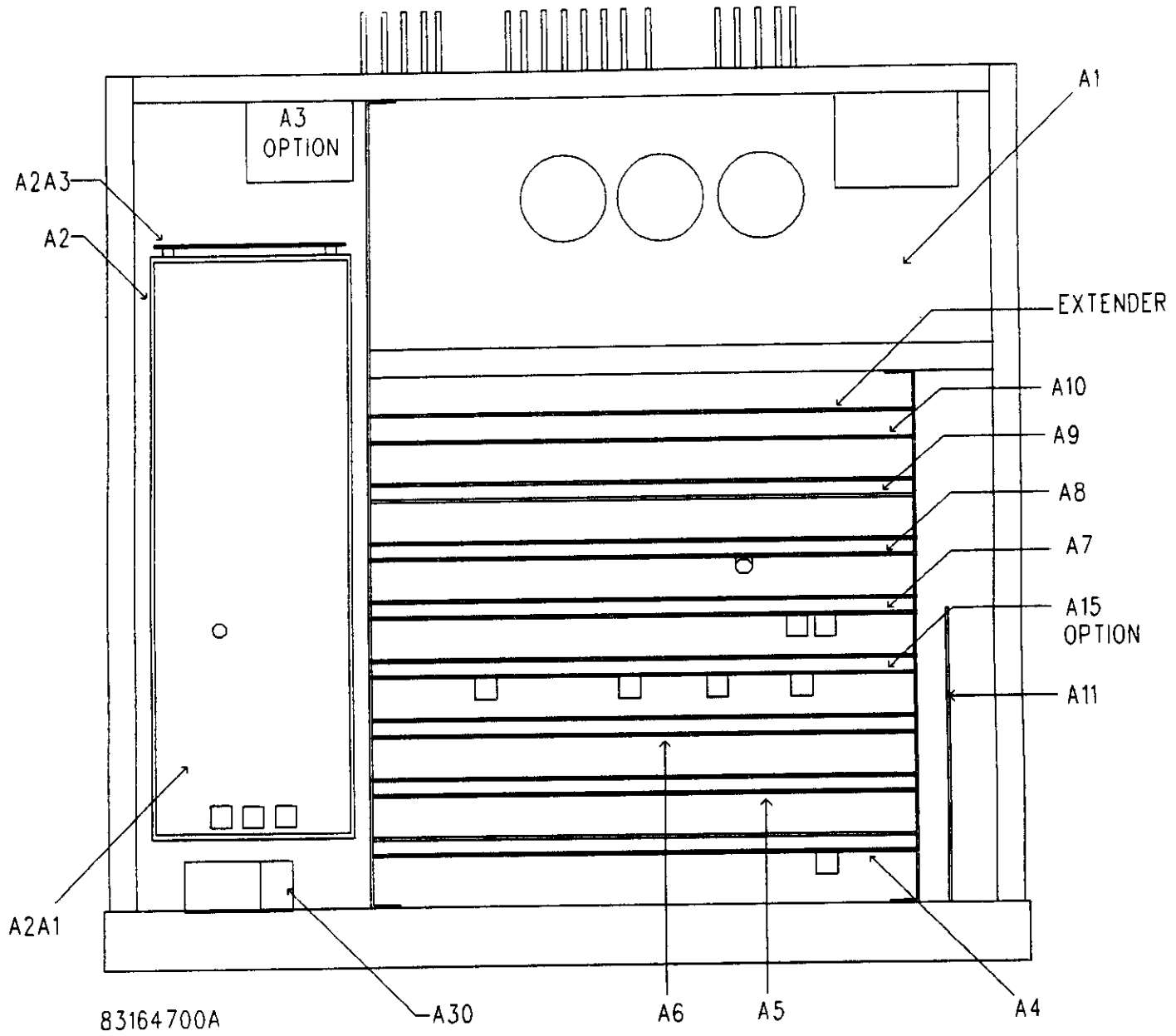
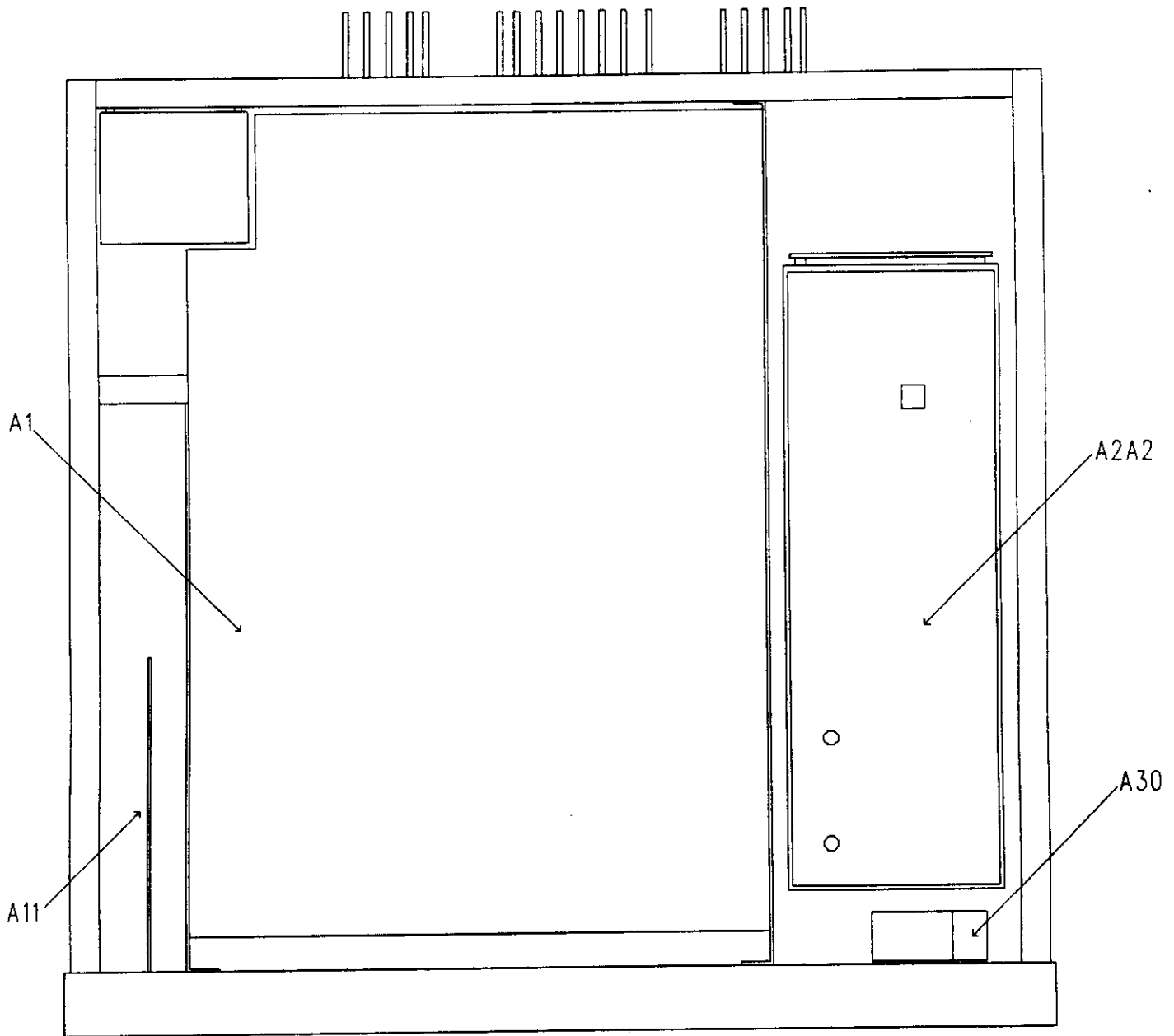


FIGURE 6-1. MAJOR ASSEMBLY LOCATION, TOP VIEW.



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FIGURE 6-2. MAJOR ASSEMBLY LOCATION, BOTTOM VIEW.

6-13. RF assembly covers. To remove the RF assembly covers, proceed as follows:

1. Remove the instrument covers as described above.
2. Remove the No. 4 snipping screw in the RF assembly cover if it has not been removed previously.
3. Grasp the cover near the front and rear of the instrument.
4. Pull up on the cover at the rear of the instrument first, and then at the front. The cover should pull away easily.
5. Turn the instrument over and repeat the above procedure for the bottom cover.

6-14. RF Printed Circuit Board. To remove the RF printed circuit board, proceed as follows:

1. Remove the instrument and RF assembly covers as described above.
2. Remove the connectors from J3, J4, and J5 at the rear of the circuit board.
3. Remove the connector from J2 near the center of the board.
4. Remove 7 No. 4 screws and the hex spacer holding the circuit board to the RF casting.

CAUTION

Be careful in the following steps not to break the center pin of the RF in connector.

5. Use a small pair of pliers to pull up on TP1 to disengage J1 from the local oscillator board.
6. Carefully unsolder the center conductor of the input RF connector while pulling the circuit board toward the rear of the instrument.
7. Pull the circuit board up and away from the casting.
8. To replace the RF circuit board reverse the above procedure.

6-15. Oscillator Board. To remove the local oscillator board, proceed as follows:

1. Remove the instrument and RF assembly covers as described above.
2. Very carefully unsolder the wire from the center pin of the SMB connector at the front of the RF casting.
3. Remove the connectors from J1 and J2 at the rear of the circuit board.
4. Remove 9 No. 6 screws and one hex spacer holding the circuit board to the RF casting.
5. Use a small pair of pliers to gently pull up on TP4 to disengage P1 from the RF circuit board.
6. Pull the circuit board up and away from the RF casting.
7. To replace the Oscillator board reverse the above procedure.

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6-16. Gaining Access to Display/keyboard. To gain access to the display and keyboard, proceed as follows:

1. Remove the instrument covers as described above.
2. Remove three No. 4 screws that hold the top trim extrusion and two grounding clips.
3. Grasp the trim strip by its edges and pull it away.
4. Remove the plastic display window.

CAUTION

Be careful not to scratch the the inner surface of the display window.

5. Turn the instrument over and remove three No. 4 screws that hold the bottom trim extrusion and two grounding clips.
6. Grasp the trim strip by its edges and pull it away.
7. Tilt the bottom of the front panel away from the instrument until all switches are clear; then, pull the front panel up to clear the center trim extrusion.

6-17. Changing Instrument Firmware. To change the instrument eproms, proceed as follows:

1. Remove all cable connections from the Model 8201, including the power cable.
2. Remove the instrument top cover as described above.

CAUTION

When replacing U10 and U14 observe that the orientation of pin 1 is away from the top of the CPU board. The three numbers on the replacement IC should match the numbers on the one being replaced.

3. Extract the CPU board, A9 (Blue Extractors) far enough to remove U10 and replace it with the new eprom.
4. Remove A9U14 and replace with the new eprom.
5. Install jumpers JP1 and JP2, then reseal the CPU board into the motherboard connector.
6. Before replacing the top instrument cover, connect the AC power supply and turn the LINE switch ON.
7. The new firmware number will appear in the CARRIER display, followed by a 'CLEAR' message..
8. Turn the instrument power off, extract the CPU board and remove jumpers JP1 and JP2. Replace the instrument cover.
9. Turn the instrument ON and enter SPCL 30 to calibrate the Model 8201.

6-18. Instrument Test Jumpers. The Model 8201 CPU board has two test jumpers, JP1 and JP2, which are used as an aid in troubleshooting the instrument circuits. The jumper positions and related tests are listed below.

6-19. Removal of Detail Parts. Careful attention has been paid in the design of the Model 8201 to maintainability. Most detail parts are readily accessible for inspection and replacement when the instrument covers and RF shields are removed. Solid-state circuit components, mounted on plug-in circuit boards, are used throughout the instrument. Standard printed circuit board

JP1 - JP2	ACTION
OFF-OFF	Normal operation, no tests are done.
ON-OFF OFF-ON	Enable SPCL functions for test and calibration. Activate Tests. Exercises the software A/D converter system, instrument interface, and GPIB SRQ line.
ON-ON	Erase variable memory and install nominal calibration factors. Used when a repair has been made on the CPU board or when new firmware is installed.

TABLE 6-1. TEST JUMPERS.

maintenance techniques are used for removal and replacement of parts. Excessive heat must be avoided; a low wattage soldering iron and suitable heat sinks should be used for all soldering and unsoldering operations.

6-20. PRELIMINARY CHECKS.

6-21. Visual checks. If equipment malfunction occurs, perform a visual check of the Model 8201 before performing electrical tests. Visual checks often help to isolate the cause of a malfunction quickly and simply. Inspect the instrument for signs of damage caused by excessive shock, vibration, or overheating, such as broken wires, loose hardware and parts, loose electrical connections, electrical shorts, cold solder connections, or dirt or other foreign matter. Correct any problems discovered, then complete the operational checks to verify that the instrument is functional. If a malfunction persists or the instrument fails any of the operational checks, continue with the troubleshooting procedures below.

6-22. Power Supply Check. Improper operation of the Model 8201 may be caused by incorrect dc operating voltages. Before proceeding with any other electrical checks, perform the power supply checks in the Motherboard/Power Supply section.

6-23. TROUBLESHOOTING.

6-24. Instrument malfunction will generally be evident from front panel indications, or IEEE-488 bus responses. The problems will fall into two general categories; selective failure of one sub-system or catastrophic failure.

6-25. Selective failure of one section of the instrument or out of specification performance will be evident from manipulation of the front panel controls. For example, incorrect or erratic FM deviation indications would be evident from display readings only in the FM modulation mode, and the problem would most likely be associated with the FM circuit board, A4. However, similar performance on both AM and FM displays would indicate a problem on the Filter or Detector boards.

6-26. Catastrophic failures, on the other hand, would generally cause the Model 8201 to be completely inoperative. For instance, if the microprocessor was not operating properly, the displays would contain meaningless symbols and the keyboard would not be responsive.

6-27. Further isolation of the problem requires some understanding of the simplified block diagram. Read over the theory of operation section and then proceed with the troubleshooting section below. When the problem is localized to a specific assembly, refer to the service information for that assembly.

6-28. TROUBLE LOCALIZATION.

6-29. Many malfunctions are evident from the front panel display. See Table 6-2.

6-30. Other front panel indications might include erratic or incorrect displays or an inoperative keyboard. In each case the circuit board most closely associated with that display should be tested first.

Display	Probable fault on
No display	A1 Motherboard/Power Supply or A12 Display Board
Meaningless symbols	A9 CPU Board
Error 20	A5 AM Board
Error 21	A4 FM Board
Error 22	A4 FM or A6 Filter Board
Error 23-25	A8 Detector Board
Error 26	A5 AM or A2A1 RF Board
Error 27,28	A6 Filter Board
Error 30-33	A2A2 Oscillator Board
Error 34	A2A2 Oscillator Board
Error 35-39	A9 CPU Board

TABLE 6-2. HARDWARE ERROR DISPLAYS.

6-31. TROUBLESHOOTING, MOTHERBOARD/POWER SUPPLY.

6-32. GENERAL. Procedures for checking the Motherboard circuits are given below. Test points and other measurement points are indicated on the schematic diagram and circuit board overlay, Figures 8-2, 8-3, and 8-4.

6-33. EQUIPMENT REQUIRED. The test equipment required for these tests is listed below. See Table 5-1 for critical specifications.

- Oscilloscope.....HP 1740A
- DC voltmeterFluke 8840A



Line voltages up to 240 volts AC may be encountered in the power supply circuits. To protect against electrical shock, observe suitable precautions when connecting and disconnecting test equipment, and when making voltage measurements.

6-34. PROCEDURE.

6-35. With the instrument covers removed and power applied, observe DS1-DS5. These displays indicate if the supplies are operating normally. All of the LEDs should be about the same brightness. If not, troubleshoot the circuit associated with the incorrect display LED. The LED and associated circuits are:

NOTE

For the following oscilloscope measurements, use a high impedance probe.

6-36. +5V Display (DS2). The +5 volt display supply is a three terminal regulator, U7, and associated components. If the output voltage is incorrect check for shorted CR11, CR15, or C22. The regulator output can be isolated by disconnecting J4 on the I/O board.

LED	Circuit
DS1	-30V supply
DS2	+5V (display)
DS3	+5V (instrument)
DS4	+15V
DS5	-15V

TABLE 6-3. Power Supply LEDs.

6-37. +5V Instrument (DS3). The +5 volt instrument supply is a three terminal regulator, U4, and associated components. If the output voltage is incorrect check for shorted CR5, CR10, or C14. The regulator output can be isolated by extracting all of the plug-in boards and disconnecting J4 at the RF housing.

6-38. +15V (DS4). The +15 volt instrument supply is a three terminal regulator, U5, enclosed in a feedback loop consisting of AR2a and associated components. Proceed as follows:

1. If the dc voltage at the +15 volt bus is near ground a short circuit is the most likely problem. The supply can be isolated by extracting all of the plug-in boards and disconnecting J4 at the RF housing. This can be done one board at a time to isolate the defective circuit.
2. If the voltage at the +15 volt bus is low, but not zero, the problem may be with the -15 volt supply. See below.
3. In any case measure the dc voltage at the positive terminal of C8. The voltage should be +20 volts at nominal line. If not, check for defective CR2 or replace defective U5.
4. Measure the dc voltage at pin 6 of U8. The voltage should be +10 volts. If not, replace defective U8. Note that if the +15 supply voltage is less than 12 volts U8 will not operate properly.
5. Measure the dc voltage at pin 1 of AR2. The voltage should be +10 volts. If not, replace defective AR2, or check for shorted CR7.

6-39. -15V (DS5). The -15 volt instrument supply is a three terminal regulator, U6, enclosed in a feedback loop consisting of AR2b and associated components. Proceed as follows:

1. If the dc voltage at the -15 volt bus is near ground a short circuit is the most likely problem. The supply can be isolated by extracting all of the plug-in boards and disconnecting J4 at the RF housing. This can be done one board at a time to isolate the defective circuit.
2. If the voltage at the -15 volt bus is low, but not zero, the problem may be with the +15 volt supply.
3. In any case measure the dc voltage at the negative terminal of C10. The voltage should be -20 volts at nominal line. If not, check for defective CR2 or replace defective U6.
4. Measure the dc voltage at pin 6 of U8. The voltage should be +10 volts. If not, replace defective U8. Note: If the +15 supply voltage is less than 12 volts U8 will not operate properly.
5. Measure the dc voltage at pin 7 of AR2. The voltage should be -10 volts. If not, replace defective AR2, or check for shorted CR9.

6-40. -30V (DS1). The -30 volt instrument supply consists of a voltage doubler and operational amplifier AR3 and associated components. Proceed as follows:

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1. If the dc voltage at pin 6 of AR3 is near ground a short circuit is the most likely problem. The supply can be isolated by disconnecting J4 at the RF housing.
2. Measure the dc voltage at the negative terminal of C3. The voltage should be -40 volts at nominal line. If not, check for defective CR3 or CR4 or replace defective AR3.
3. Measure the dc voltage at pin 3 of AR3. The voltage should be -15 volts. If not, troubleshoot the -15 volt supply.
5. Measure the dc voltage at pin 7 of AR3. The voltage should be -12 volts. If not, replace defective CR14.

6-41. LOGIC SIGNALS.

6-42. Proper operation of the RF and Oscillator circuits depend on correct logic levels on the following control lines:

IA2-IA7 instrument address bus
ID0-ID7 instrument data bus

The instrument address lines are decoded by U2 to produce latch strobes. IA7 is a write strobe and IA6 is a read strobe. In operation, data on the instrument bus is latched into octal latch U1, when address lines IA4 and IA5 are high, IA2, IA3, and IA6 are low, and strobe IA7 goes from high to low. Data is strobed into U9 under the same conditions except that IA2 is high.

To troubleshoot the logic circuits proceed as follows:

1. With the Model 8201 powered up normally, but with no RF input signal, depress the INTT key.
2. Use the oscilloscope to monitor the activity on the instrument data bus on pins 1-8 of the plug-in card connectors. All of the data lines should show activity and normal TTL levels. If not, the problem is on the CPU board.
3. Connect the oscilloscope to pin 6 of U2 and set the timebase to 0.5 mSEC/DIV.
4. The signal should be a narrow positive pulse indicating a write operation to the instrument circuits. If the signal is incorrect, the problem is on the CPU board.
5. Move the oscilloscope probe to pin 12 of U2. The signal should be as in the previous step, except that it is inverted. If not, replace defective U2.
6. The following table presents logic levels on various pins of U1 when the indicated data is keyed into the CARRIER or PRGM displays.

Pin numbers	15-16-12
logic level	data entered
low-low-high	Enter -20 dBm into carrier LEVEL display.
low-high-high	Enter + 10 dBm into carrier LEVEL display.
high-low-high	not used
high-high-low	SPCL 30
Pin numbers	19-2-5
logic level	data entered
low-low-low	2.0 MHz FREQ
high-low-low	2.2 MHz FREQ

low-high-low	2.5 MHz FREQ
high-high-low	3.2 MHz FREQ
low-low-high	10.1 MHz FREQ
high-low-high	12.0 MHz FREQ
low-high-high	15.0 MHz FREQ
high-high-high	18.0 MHz FREQ

7. Depress the carrier FREQ and AUTO keys and observe the signals on pins 6 and 9 of U2. The signal should be TTL logic waveforms indicating proper operation of the frequency acquisition circuits. If not, replace defective U2, or check for wiring shorts between the motherboard and the RF casting assembly.

8. Move the oscilloscope probe to pin 19 of U9. Enter +26 dBm, and then 0 dBm into the carrier LEVEL display. The signal should change from TTL low to high. If not, replace defective U9.

9. Move the oscilloscope probe to pin 1 of U10. The signal should be as in the previous step except that it is inverted and is 15 volts peak-to-peak. If not, replace defective U10.

10. Move the oscilloscope probe to the circuit pad connected to J1, pin 1. (pin 1 is nearest R20). The signal should be as in the previous step except that it is again inverted. If not, replace defective Q1.

11. If steps 8-10 are correct, but A30 does still not operate properly, replace defective A30, or check for open or shorted wiring.

6-43. TROUBLESHOOTING, RF BOARD.

6-44. GENERAL. Procedures for checking the RF circuit board are given below. Test points and other measurement points are indicated on the schematic diagram and circuit board overlay, Figures 8-6 and 8-7.

6-45. EQUIPMENT REQUIRED. The test equipment required is listed below. See Table 5-1 for critical specifications.

Oscilloscope	HP 1740A
Signal Generator.....	Boonton 1021
DC voltmeter.....	Fluke 8840A

6-46. PROCEDURE.

1. Set the signal generator to 15 MHz CW at 0 dBm and connect the RF OUT to the Model 8201 RF IN connector.

2. Select the carrier FREQ function and key 15 MHz into the display.

NOTE

For the following oscilloscope measurements, use a high impedance probe with a very short ground connection. A spring clip type ground connection is recommended.

3. Connect the oscilloscope probe to the RF input connector, A2J1 on the circuit board, and measure the incoming signal. The signal should be about 400 millivolts peak-to-peak with a period of 67 nanoseconds. Some of the local oscillator signal may be present. Incorrect signals indicate defective input connectors, A30 module, or cables.

4. Connect the oscilloscope to TP1. The signal should be about 700 millivolts peak-to-peak with a period of 33 nanoseconds. No signal indicates a defective local oscillator board.

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5. Move the oscilloscope to pin 11 of U1. The signal should be about 3.5 volts peak-to-peak with a period of 33 nanoseconds. If not, replace defective Q1 or U1.
6. Move the oscilloscope to pin 9 of U1. The signal will be a TTL signal with a period of 67 nanoseconds. Some ringing and overshoot is normal. If not, replace defective U1.
7. Use the oscilloscope probe to trace the TTL signal to pin 8 and pin 6 of U3. If not, replace defective U3.
8. Move the oscilloscope probe to pin 3 of U2. This should be a negative going TTL pulse about 12 nanoseconds wide with a period of 62 nanoseconds. If not, replace defective U2.
9. Move the oscilloscope probe to the collector (case) of Q3 or Q13. The signal should be a negative going pulse about 12 volts peak-to-peak. If not, replace defective Q3 or Q13.
10. Move the oscilloscope probe to the anode of CR4. The signal should be as shown in Figure 6-3,D. If not, check for defective T2 or replace defective CR4.
11. The signals at pins 1 and 6 of T1 should be nearly equal amplitude, opposite polarity pulses between .7 and 1.1 volts peak with a 100 MHz oscilloscope bandwidth. If not, replace defective T1 or open CR3.
12. The signal at the junction of C2 and R9 should be as indicated in Figure 6-3,B. Incorrect signals indicate defective sampling bridge or bridge bias circuits.
13. The signal at the junction of C7 and R20 should be as indicated in Figure 6-3,A. Incorrect signals indicate defective sampling bridge or bridge bias circuits.
14. Move the oscilloscope probe to TP2. The signal should appear as in Figure 6-3,C. If the signal is not as indicated, troubleshoot the sampler amplifier, Q2 and Q4-Q7 by dc and waveform measurements.
15. Connect the oscilloscope probe to TP3. The signal is the same as at TP2, but ten times smaller. (40 millivolts peak-to-peak) If not, replace defective U4.
16. Connect the oscilloscope probe to TP4. The signal is the same as that at TP3, but 3.6 times larger. (150 millivolts peak-to-peak) If the signal is not as indicated, troubleshoot the amplifier Q8-Q12 by dc and waveform measurements.
17. Connect the oscilloscope probe to A2J4 (center SMB connector). The signal is the same as that at TP4. If not, replace defective K1.
18. Change the generator frequency to 500 kHz and set the Model 8201 carrier FREQ to 9 MHz. The signal at A2J4 pin 1 should be about 150 millivolts peak-to-peak with a period of 2 microseconds. If not, replace defective AR1.

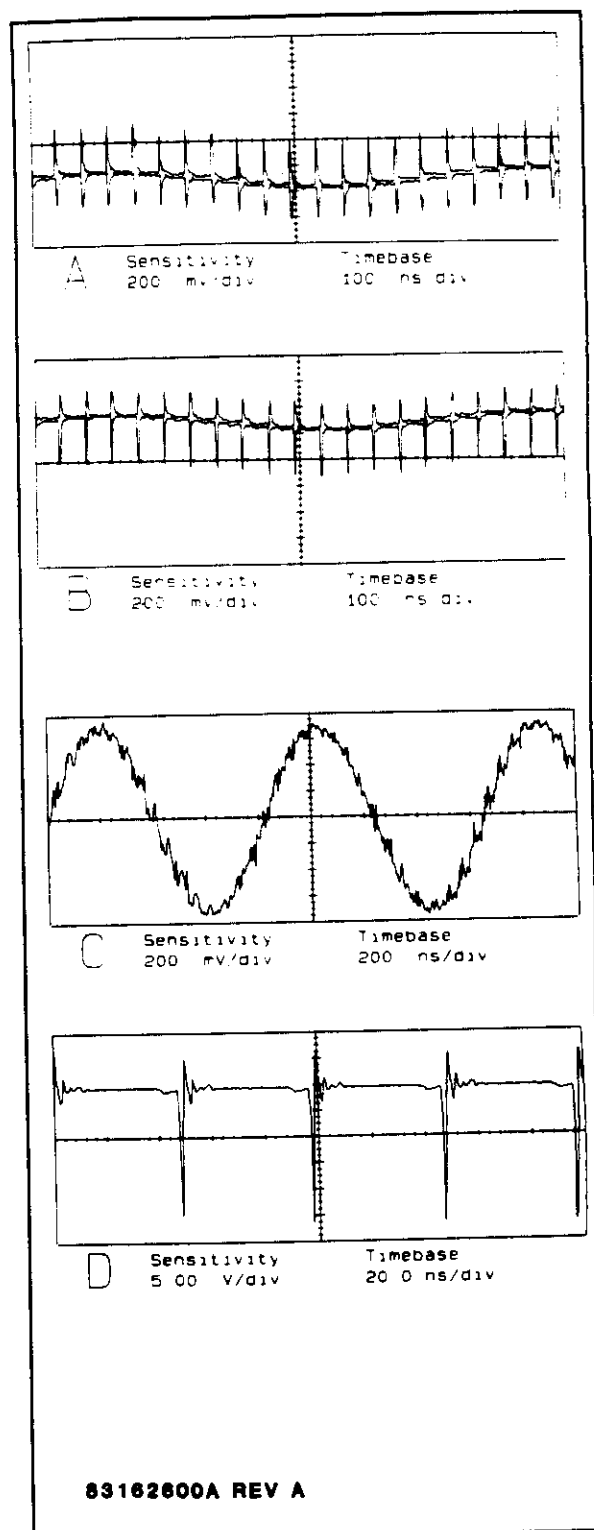


FIGURE 6-3. RF Board Waveforms.

19. Move the oscilloscope probe to pin 1 of U8. The signal should be about 75 millivolts peak-to-peak. If not, replace defective U7 or troubleshoot filter L3, L7, C39, C47, C52.

20. Enter the following frequencies into the carrier FREQ display and observe the waveform on the indicated pins of U7. The signal is a 500 kHz signal as in step 18. Incorrect signals indicate defective U7 or decoder U5.

FREQUENCY	PIN
2 MHz	pin 2
9 MHz	pin 7
11 MHz	pin 15
18 MHz	pin 10

21. Probe the signals on pins 7 and 8 of U8. The signal should be a square wave about 3.5 volts peak-to-peak, with a 2 microsecond period. If not, replace defective U8.

22. Move the oscilloscope probe to pin 6 of AR2. The signal is a square wave as in step 21 with an amplitude of 600 millivolts. If not, replace defective AR2.

23. The signal on pin 2 of U9 is as in step 21 with an amplitude of about 2 volts peak-to-peak. If not, replace defective U9, shorted CR10, or open CR11.

24. The signal on pin 9 of U9 is a TTL waveform with a period of 14 microseconds. If not, replace defective U9.

25. Enter 2 MHz into the carrier FREQ display. The signal on pin 9 of U9 is a TTL waveform with a period of 4 microseconds. If not, replace defective U9.

6-47. LOGIC SIGNALS.

6-48. Proper operation of the RF circuits depend on correct logic levels on the following control lines:

- R0,R1.....IF attenuation and calibration**
- B1,B2.....band switching**

The following table indicates the TTL logic levels and the associated function for control lines R0 and R1:

Logic Line	logic value	operation
R0-R1	low-low	no IF attenuation
	low-high	attenuate IF by 10
	high-low	not used
	high-high	calibrator signal

The following table indicates the TTL logic levels and the associated function for control lines B1 and B2:

Logic Line	logic value	operation
B1-B2	low-low	select filter U7,2 U9 divide by 7 U3, select /10
	low-high	select filter U7,7 U9 divide by 7 U3, select /10
	high-low	select filter U7,15 U9 divide by 2 U3, select /2
	high-high	select filter U7,10 U9 divide by 2 U3, select /2

Incorrect logic signals on the R0, R1, B1, or B2 lines indicate a problem on the motherboard decoder U2 or latch U1, or the CPU board.

Maintenance

6-49. TROUBLESHOOTING, OSCILLATOR BOARD.

6-50. GENERAL. Procedures for checking the oscillator board are given below. Test points and other measurement points are indicated on the schematic diagram and circuit board overlay, Figures 8-8 and 8-9.

6-51. EQUIPMENT REQUIRED. The test equipment required is listed below. See Table 5-1 for critical specifications.

Oscilloscope.....HP 1740A
 Signal GeneratorBoonton 1021
 DC voltmeterFluke 8840A

6-52. PROCEDURE.

1. Measure the dc voltage at pin 16 of U3. The voltage should be approximately + 5 volts. If not, the power supply circuits or the motherboard connectors are defective.
2. Measure the dc voltage at pins 7 and 4 of AR2. The voltages should be + 15 and -15 respectively. If not, the power supply circuits or the motherboard connectors are defective.
3. Measure the dc voltage at TP3. The voltage should be -14.0 volts. If not, troubleshoot regulator AR3 and Q7 using dc measurements.
4. Enter 10 MHz into the carrier FREQ display. Observe that LED DS2 is illuminated. If not, proceed to logic signals troubleshooting for additional tests.
5. Measure the dc voltage at pin 7 of AR1. The level should be about + 13 volts. If not, replace defective AR1 or U1.

NOTE

For the following oscilloscope measurements, use a high impedance probe with a very short ground connection. A spring clip type ground connection is recommended.

6. Connect the oscilloscope probe to the anode of CR4. The signal should be about 400 millivolts peak-to-peak with a period of 45 nanoseconds. If the indication is incorrect, troubleshoot oscillator Q1 using dc and waveform measurements.
7. Select the carrier FREQ function and key 12 MHz into the display. Observe that LED DS3 is illuminated. If not, proceed to logic signals troubleshooting for additional tests.
8. Measure the dc voltage at pin 1 of AR1. The level should be about + 13 volts. If not, replace defective AR1 or U1.
9. Connect the oscilloscope probe to the anode of CR21. The signal should be about 400 millivolts with a period of 37 nanoseconds. If the indication is incorrect, troubleshoot oscillator Q3 using dc and waveform measurements.
10. Select the carrier FREQ function and key 15 MHz into the display. Observe that LED DS4 is illuminated. If not, proceed to logic signals troubleshooting for additional tests.
11. Measure the dc voltage at pin 8 of AR1. The level should be about + 13 volts. If not, replace defective AR1 or U1.
12. Connect the oscilloscope probe to the anode of CR32. The signal should be about 400 millivolts with a period of 33 nanoseconds. If the indication is incorrect, troubleshoot oscillator Q4 using dc and waveform measurements.
13. Select the carrier FREQ function and key 18 MHz into the display. Observe that LED DS5 is illuminated. If not, proceed to logic signals troubleshooting for additional tests.
14. Measure the dc voltage at pin 14 of AR1. The level should be about + 13 volts. If not, replace defective AR1 or U1.

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15. Connect the oscilloscope probe to the anode of CR43. The signal should be about 600 millivolts with a period of 26 nanoseconds. If the indication is incorrect, troubleshoot oscillator Q6 using dc and waveform measurements.
16. Connect the oscilloscope probe to ungrounded end of L23. The signal should be about 500 millivolts with a period of 26 nanoseconds. If not, replace defective diode CR43.
17. Connect the oscilloscope probe to TP4. The signal should be about 800 millivolts with a period of 26 nanoseconds. If not, troubleshoot amplifier Q5 by dc and waveform measurements.
18. Move the oscilloscope to the LO2 SMB connector on the front of the RF casting. The signal should be 500 millivolts with a period of 26 nanoseconds. If not, troubleshoot amplifier Q2 by dc and waveform measurements, or replace defective T1, or check for shorted RF cable connecting to Motherboard.
19. Set the signal generator to 15 MHz CW and 0 dBm and connect the RF OUT to the RF IN of the Model 8201.
20. Depress the Model 8201 INIT key and then enter 15 MHz into the carrier FREQ Display.
21. Connect the oscilloscope probe to pin 3 of U2. The signal should be a TTL signal with a period of 6 microseconds. If not, the problem is associated with the RF circuit board.
22. Move the oscilloscope probe to pin 6 of U2. The signal should be a TTL signal with a period of 6 microseconds. Additionally, the time from the falling edge to the rising edge should be 3 microseconds. If not, replace defective U2 or check C23 and R15.
23. Move the oscilloscope probe to pin 6 of AR2. The signal should be a distorted TTL signal with a period of 6 microseconds and an average value of near zero volts. The oscilloscope must be dc coupled for this test. If not, replace defective AR2.
24. Enter SPCL 37 to activate the local oscillator test. The MODULATION display will indicate 0 -- LO.
25. Measure the dc voltage at the end of R29 nearest TP2. The voltage should be -10 volts. If not, the problem is on the CPU board or in the interconnecting cable.
26. The other end of R29 should be 0 volts dc. If not, U3 or AR4a is defective.
27. Measure the voltage at TP2. The voltage should be +10 volts. If not, U3 or AR4a is defective.
28. Measure the voltage at pin 3 of AR5. The voltage should be -5 volts. If not, AR4b or Q9 is defective.
29. Measure the voltage at pin 6 of AR5. The voltage should be -5 volts. If not, AR5 is defective.

NOTE

If all measurements to this point are correct, but trouble persists, the problem is with the logic circuits or U3 or possibly Q8 or DS1. Troubleshoot by dc voltage measurement or refer to logic signals troubleshooting below.

6-53. LOGIC SIGNALS.

6-54. Proper operation of the oscillator circuits depend on correct logic levels on the following control lines:

FC0,FC1.....oscillator tuning
B0,B1,B3 band switching

The following table indicates the logic levels and the associated function for control lines FC0 and FC1:

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Logic Line	logic value	operation
FC0-FC1	low-low	frequency lock, DS1 off
	low-high	frequency lock, DS1 on
	high-low	set frequency, DS1 on
	high-high	set frequency, DS1 off

Logic Line	logic value	operation
B0,B1,B3	low-low-high	oscillator Q1 active, DS2 on
	low-high-high	oscillator Q3 active, DS3 on
	high-low-high	oscillator Q4 active, DS4 on
	high-high-high	oscillator Q6 active, DS5 on
	X - X -low	all oscillators inactive

X means don't care

Incorrect logic signals on the FC0, FC1, B0, B1, or B3 lines indicate a problem on Motherboard decoder U2, latch U1, or problems on the CPU board.

6-55. TROUBLESHOOTING, FM BOARD.

6-56. GENERAL. Procedures for checking the FM circuit board are given below. Test points and other measurement points are indicated on the schematic diagram and circuit board overlay Figures 8-10 and 8-11.

6-57. EQUIPMENT REQUIRED. The test equipment required is listed below. See Table 5-1 for critical specifications.

- Oscilloscope.....HP 1740A
- Signal GeneratorBoonton 1021
- DC voltmeterFluke 8840A

6-58. PROCEDURE.

1. Turn off the instrument and remove the FM circuit board. (Brown extractors) Insert the FM board into the Extender board (Grey extractors), and plug the combination back into the FM board slot. Turn on the instrument power, wait for a normal power up sequence, then depress the INIT key.
2. Measure the dc voltage at pin 6 of AR1. The voltage should be approximately +5 volts. If not, troubleshoot the regulator circuit AR1 using dc measurements.
3. Repeat step 1. at pins 7 and 4 of AR1. The voltages should be +15 and -15 volts respectively. If not, the problem is in the power supply circuits or the Motherboard interconnect.
4. Measure the dc voltage at either end of L7. The voltage should be -12.5 volts. If not, troubleshoot regulator Q14 using dc measurements.
5. Set the signal generator to 15 MHz and 0 dBm with 50 kHz FM at a 1 kHz rate.
6. Connect the RF OUT of the generator to the RF IN of the Model 8201 and depress the FM function key.

NOTE

For the following oscilloscope measurements, use a high impedance probe with a very short ground connection.

7. Connect the oscilloscope probe to pin 2 of the edge connector. (also the right end of R1). The signal should be an FM modulated signal with an amplitude of about 150 millivolts peak-to-peak and a period of 0.83 microseconds. Some of the local oscillator signal will be present. If not, the problem is on the RF board or the interconnecting cables.
8. Move the oscilloscope probe to TP3. The signal should be as in step 7 except that the amplitude should be 75 millivolts peak-to-peak and the local oscillator signal should not be present. If not, check low-pass filter L3-L4, C1, and C4-C7 for open inductors or shorted capacitors.
9. Move the oscilloscope probe to TP2. The signal should be a clipped sinewave with an amplitude of 1 volt peak-to-peak. If not, troubleshoot limiter stages 1 and 2 (Q3) using dc and waveform measurements.
10. Move the oscilloscope probe to TP6. The signal should be a squarewave with an amplitude of 1 volt peak-to-peak. If not, troubleshoot limiter stages 3 and 4 (Q8) using dc and waveform measurements.
11. Move the oscilloscope probe to TP7. The signal should be as shown in Figure 6-4,A. If not, troubleshoot level shifter Q13 and associated components using dc and waveform measurements.
12. Move the oscilloscope probe to pin 5 of U1. The signal should be as shown in Figure 6-4,B. If not, replace defective U1.
13. Move the oscilloscope probe to TP8. The signal should be as shown in Figure 6-4,C. If not, troubleshoot comparator Q4-Q7 and current source Q2 using dc and waveform measurements. Additionally, check for defective Q1 or Q10.
14. Move the oscilloscope probe to TP1. The signal should be as shown in Figure 6-4,D. If not, troubleshoot comparator Q4-Q7 and current source Q2 using dc and waveform measurements. Additionally, check for defective Q1 or Q10.
15. Move the oscilloscope probe to TP9. The signal should be as shown in Figure 6-4,E. If not, troubleshoot current switch Q11 and Q12, or current source AR2 and Q9 using dc and waveform measurements. Additionally, check for defective Q1 or Q10.
16. Move the oscilloscope probe to TP11. The signal should be a sinewave with an amplitude of 300 millivolts peak-to-peak and a period of 1 millisecond. If not, check low-pass filter L5, L6, L9, L10, and C27, C28, C32, C33, C36, C39, C41, C42, and C44 for open inductors or shorted capacitors.
17. Move the oscilloscope probe to TP12. The signal should be a sinewave with an amplitude of 1 volts peak-to-peak and a period of 1 millisecond. If not, replace defective AR3, Q15 or Q16.

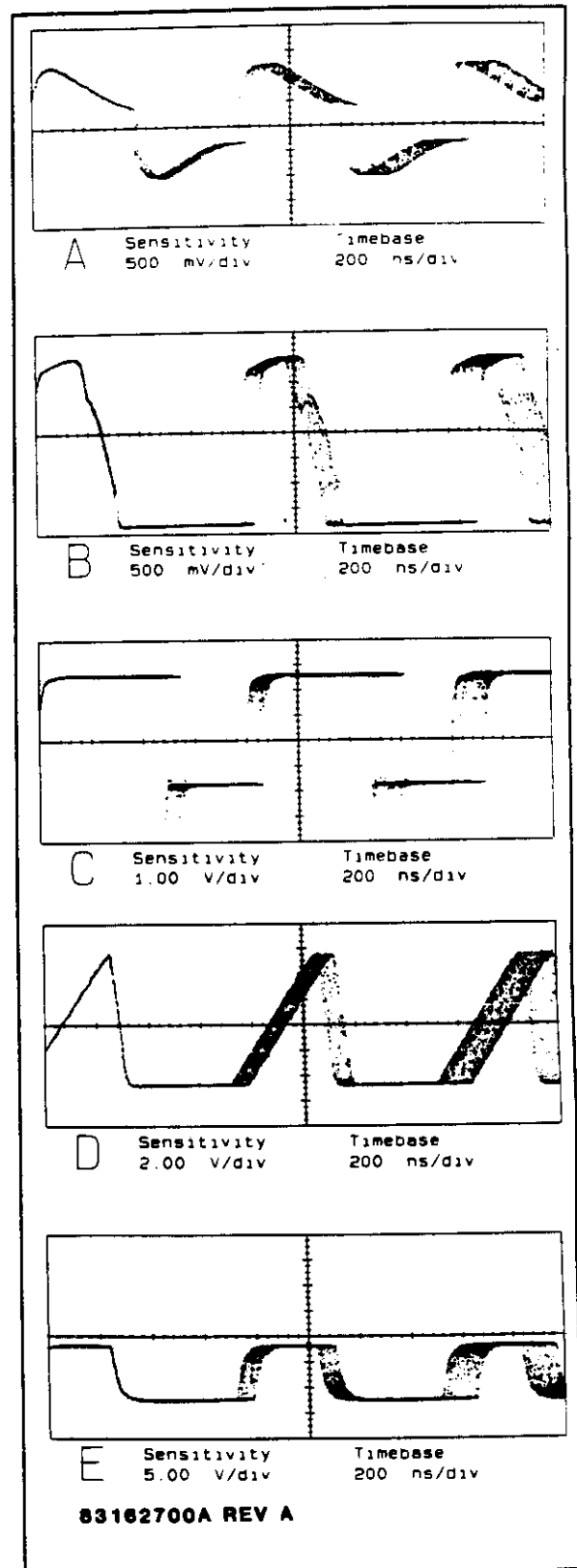


FIGURE 6-4. FM Board Waveforms.

6-59. LOGIC SIGNALS.

6-60. The operation of the FM circuits does not require interface to the control logic, however, instrument address line IA1 is dedicated to the FM circuits for future developments.

6-61. TROUBLESHOOTING, AM BOARD.

6-62. GENERAL. Procedures for checking the AM circuit board are given below. Test points and other measurement points are indicated on the schematic diagram and circuit board overlay Figures 8-12 and 8-13.

6-63. EQUIPMENT REQUIRED. The test equipment required is listed below. See Table 5-1 for critical specifications.

Oscilloscope.....HP 1740A
 Signal GeneratorBoonton 1021
 DC voltmeterFluke 8840A

6-64. PROCEDURE.

1. Turn off the instrument and remove the AM circuit board. (Black extractors) Insert the AM board into the Extender board (Grey extractors), and plug the combination back into the AM board slot. Turn on the instrument power, wait for a normal power up sequence, then depress the INIT key.

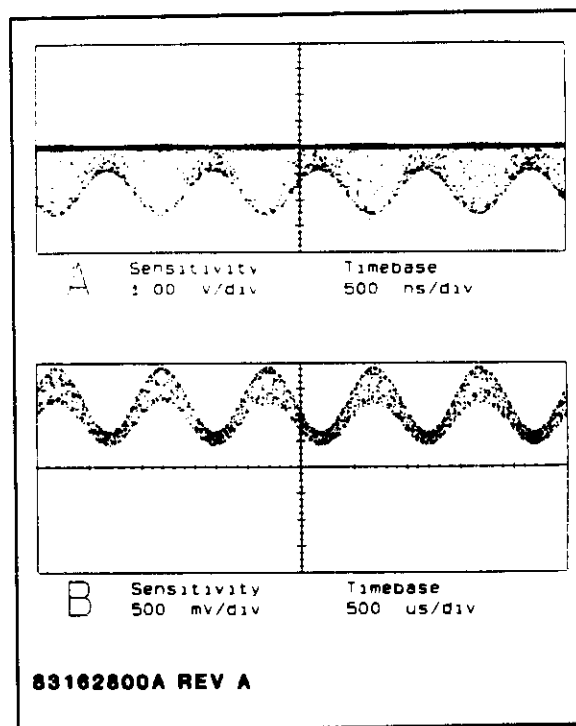
2. Measure the dc voltage at pin 20 of U1. The voltage should be approximately +5 volts. If not, the power supply circuits or the motherboard connectors are defective.

3. Measure the dc voltage at pin 13 and pin 3 of U2. The voltages should be +15 and -15 volts respectively. If not, the power supply circuits or the motherboard connectors are defective.

4. Measure the dc voltage at either end of L7. The voltage should be +12 volts. If not, troubleshoot regulator Q1 and Q2 using dc measurements.

5. Set the signal generator to 15 MHz and 0 dBm with 50 % AM at a 1 kHz rate.

6. Connect the RF OUT of the generator to the RF IN of the Model 8201 and depress the AM function key.

**FIGURE 6-5. AM Board Waveforms.****NOTE**

For the following oscilloscope measurements, use a high impedance probe with a very short ground connection. A spring clip type ground connection is recommended.

7. Connect the oscilloscope probe to pin 2 of the edge connector. (also the right end of R1). The signal should be an amplitude modulated signal with an amplitude of about 200 millivolts peak-to-peak. The carrier period should be 0.83 microseconds and the modulation period should be 1 millisecond. Some local oscillator signal will be present. If not, The problem is on the RF board or the interconnecting cables.

8. Move the oscilloscope probe to TP1. The signal should be as in the previous step, except that the amplitude should be 350 millivolts peak-to-peak. Additionally, the local oscillator signal should not be present, and the dc level should be about 0 volts. If not, troubleshoot amplifier Q3-Q7 using dc and waveform measurements.

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9. Move the oscilloscope probe to TP6. The signal should be as in the previous step, except that the amplitude should be 120 millivolts peak-to-peak and the dc level should be -0.5 volts. If not, proceed to logic signals troubleshooting for additional tests.
10. Move the oscilloscope probe to TP2. The signal should be as in the previous step, except that the amplitude should be 2.5 volts peak-to-peak. If not, troubleshoot feedback amplifier Q10 and Q13- Q16 using dc and waveform measurements.
11. Move the oscilloscope probe to pin 4 of Q22. The signal should be as shown in Figure 6-5,A. If not, troubleshoot active detector Q19-Q21 using dc and waveform measurements.
12. Move the oscilloscope probe to pin 8 of Q22. The signal should be as in the previous step, except it is inverted. If not, troubleshoot active detector Q19-Q21 using dc and waveform measurements.
13. Move the oscilloscope probe to pin 6 of AR2. The signal should be as shown in Figure 6-5,B. If not, troubleshoot buffer stage Q22 and AR2 using dc and waveform measurements.
14. Move the oscilloscope probe to pin 3 of AR3. The signal should be a 0.55 volt peak-to-peak sine wave with a period of 1 millisecond and a dc level of +0.5 volts. If not, check for open inductors or shorted capacitors in low-pass filter L10-L12 and C50-C56.
15. Move the oscilloscope probe to TP3. The signal should be as in the previous step, except that the amplitude should be 1.1 volt peak-to-peak at a dc level of about 1 volt. If not, replace defective AR3.
16. Move the oscilloscope probe to the emitter lead of Q18. The signal should be an amplitude modulated signal with an amplitude of 2 volts peak-to-peak. The carrier period should be 0.83 microseconds and the modulation period should be 1 millisecond. If not, troubleshoot IF OUT buffer Q12 and Q17-Q18 using dc and waveform measurements.

6-65. LOGIC SIGNALS.

6-66. Proper operation of the AM agc circuits depend on correct logic levels on the following control lines:

IA0agc latch strobe
ID0-ID7.....instrument data bus

6-67. The instrument address line IA0 is dedicated to the AM board. In operation, data on the instrument data bus is latched into octal latch, U1, when IA0 makes the transition from high to low. The instrument data bus will contain the programming byte for agc digital-to-analog (DAC) at that time. To troubleshoot the logic and agc circuits proceed as follows:

1. With the Model 8201 powered up normally and no carrier signal connected, depress the INTT key.
2. Use the oscilloscope to monitor activity on the instrument data lines ID0-ID7 on pins 4-11 of the edge connector. All of the data lines should show activity and normal TTL levels. If not, the problem is on the CPU board or the Motherboard interconnect.
3. Set the Model 8201 carrier FREQ to 15 MHz, and select SPCL 35 to activate the AGC test program.
4. Connect the oscilloscope probe to pin 12 of the edge connector and set the timebase to 0.5 mSEC/DIV.
5. The signal should be narrow positive pulses indicating an agc level change. If the signal is incorrect, the problem is on the CPU board or the Motherboard interconnect.
6. Enter SPCL 35 to activate the AGC attenuator test program. Enter 15 into the modulation display to set maximum attenuation. The levels on the B1-B8 pins (5-12) of U2 should be:

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B1	B2	B3	B4	B5	B6	B7	B8
Low	Low	Low	Low	High	High	High	High

If the TTL levels are incorrect, U1 or U2 is defective.

7. Enter 250 into the modulation display to set minimum attenuation. The levels on the B1-B8 pins (5-12) of U2 are tabulated below.

B1	B2	B3	B4	B5	B6	B7	B8
High	High	High	High	High	Low	High	Low

If the TTL levels are incorrect, U1 or U2 is defective.

6-68. AGC ATTENUATOR.

6-69. The agc attenuator in the Model 8201 is a programmable L-pad whose series and shunt arm resistance is controlled by adjusting the current through a light dependent resistor while holding the dc voltage across the resistance constant. To troubleshoot the agc attenuator, proceed as follows:

1. Program the Model 8201 to 15 MHz carrier FREQ and 0 dBm carrier level.
2. Measure the dc voltage from TP6 to ground. The voltage should be -0.5 volts. If the indication is incorrect, troubleshoot the shunt arm control loop consisting of AR1b and Q11 and associated components by dc voltage measurements, or replace defective Q9.
3. Measure the dc voltage across R28. The voltage should be -0.5 volts. (+ 0.5 volts if the voltmeter polarity is reversed) If the indication is incorrect, troubleshoot the series arm control loop consisting of AR1a and Q7 and associated components by dc voltage measurements, or replace defective Q8.

6-70. TROUBLESHOOTING, FILTER BOARD.

6-71. **GENERAL** Procedures for checking the FILTER circuit board are given below. Test points and other measurement points are indicated on the schematic diagram and circuit board overlay, Figures 8-14, 8-15, and 8-16.

6-72. **EQUIPMENT REQUIRED.** The test equipment required is listed below. See Table 5-1 for critical specifications.

- Oscilloscope.....**HP 1740A**
- Audio Analyzer.....**Boonton 1120**
- DC voltmeter**Fluke 8840A**

6-73. PROCEDURE.

1. Turn off the instrument and remove the FILTER circuit board. (Pink extractors) Insert the FILTER board into the Extender board (Grey extractors), and plug the combination back into the FILTER board slot. Extract the FM circuit board (Brown extractors) just far enough to disengage the circuit board connector. Turn the instrument ON and enter 15 MHz into the carrier FREQ display.
2. Measure the dc voltage at pin 20 of U2. The voltage should be approximately +5 volts. If not the power supply circuits or the motherboard connectors are defective.
3. Measure the dc voltage at pins 7 and 4 of AR1. The voltages should be +15 and -15 volts respectively. If not the power supply circuits or the motherboard connectors are defective.
4. Set the audio analyzer source to 1 kHz and 600 millivolts.

5. Connect the audio analyzer source output to the FM OUT connector on the rear panel of the Model 8201.

NOTE

For the following oscilloscope measurements, use a high impedance probe. TP7 may be used as a convenient ground terminal.

6. Connect the oscilloscope probe to pin 35 of the edge connector. The signal should be a sinewave signal with an amplitude of about 800 millivolts peak-to-peak and a period of 1 millisecond. If not, the problem is on the Motherboard.
7. Move the oscilloscope probe to TP1. The signal should be as in the previous step, except that the amplitude should be 400 millivolts peak-to-peak. If not, check for defective relay K1, K2, or K3, or open inductor L4, L5, L6, or shorted capacitor C9-C12 or C14.
8. Change the audio analyzer frequency to 50 kHz. The signal should be as in the previous step, except that the amplitude should be about 250 millivolts peak-to-peak. If not, troubleshoot defective 50 kHz low-pass filter L4-L6 and C9-C12 and C14.
9. Depress the modulation analyzer 220 kHz low-pass filter key. The signal should be as in the previous step, except that the amplitude should be 0.4 volts peak-to-peak. If not, check for defective relay K1, K2, or K3, or defective attenuator R4-R6.
10. Move the oscilloscope probe to TP2. The signal should be as in the previous step, except that the amplitude should be 4 volts peak-to-peak. If not, check for defective U3 or amplifier AR1, or proceed to logic troubleshooting for additional tests.
11. Move the oscilloscope probe to TP9. The signal should be as in the previous step, except that the amplitude should be 0.4 volts peak-to-peak. If not, check for defective U3 or amplifier AR12 or proceed to logic troubleshooting for additional tests.
12. Reduce the audio analyzer level to 60 millivolts. The Model 8201 should autorange and the signal at TP9 should be as in the previous step. If not, check for defective U3 or proceed to logic troubleshooting for additional tests.
13. Increase the audio analyzer level to 6 volts. The Model 8201 should autorange and the signal at TP9 should be as in the previous step. If not, check for defective U3 or proceed to logic troubleshooting for additional tests.
14. Move the oscilloscope probe to TP3 and set the audio analyzer frequency to 30 Hz. Depress the < 10 Hz high-pass filter key. The signal should be 1.8 volts peak-to-peak with a period of 33 milliseconds. If not, check for defective U4 or amplifier AR5, or proceed to logic troubleshooting for additional tests.
15. Depress the 30 Hz high-pass key. The signal should be as in the previous step, except that the amplitude should be 1.3 volts peak-to-peak. If not, check for defective U4 or amplifier AR2, or proceed to logic troubleshooting for additional tests.
16. Change the audio analyzer frequency to 300 Hz and depress the 300 Hz high-pass key. The signal should be 1.3 volts peak-to-peak and the period should be 3.3 milliseconds. If not, check for defective U4 or amplifier AR3, or proceed to logic troubleshooting for additional tests.
17. Change the audio analyzer frequency to 3000 Hz and depress the 3000 Hz high-pass key. The signal should be 1.3 volts peak-to-peak and the period should be 0.33 milliseconds. If not, check for defective U4 or amplifier AR4, or proceed to logic troubleshooting for additional tests.
18. Change the audio analyzer frequency to 1 kHz and depress the 30 Hz high-pass key. Move the oscilloscope probe to TP4. The signal should be 1.8 volts peak-to-peak and the period should be 1 millisecond. If not, check for defective U5 or amplifier AR8, or proceed to logic troubleshooting for additional tests.
19. Change the audio analyzer frequency to 20 kHz and depress the 20 kHz low-pass key. The signal should be 1.3 volts peak-to-peak and the period should be 50 microseconds. If not, check for defective U5 or amplifier AR7, or proceed to logic troubleshooting for additional tests.

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20. Change the audio analyzer frequency to 15 kHz and depress the 15 kHz low-pass key. The signal should be 1.3 volts peak-to-peak and the period should be 67 microseconds. If not, check for defective U5 or amplifier AR6a, or refer to logic signals troubleshooting for logic troubleshooting.
21. Change the audio analyzer frequency to 3 kHz and depress the 3 kHz low-pass key. The signal should be 1.3 volts peak-to-peak and the period should be 333 microseconds. If not, check for defective U5 or amplifier AR6b, or proceed to logic troubleshooting for additional tests.
22. Change the audio analyzer frequency to 1 kHz and depress the 50 kHz low-pass key. Move the oscilloscope probe to TP5. The signal should be 1.8 volts peak-to-peak and the period should be 1 millisecond. If not, check for defective U7 or amplifier AR10, or proceed to logic troubleshooting for additional tests.
23. Change the audio analyzer frequency to 6.366 kHz and depress the 25 uSEC de-emphasis key. The signal should be 1.25 volts peak-to-peak and the period should be 157 microseconds. If not, check for defective U7 or filter R44, C49 or proceed to logic troubleshooting for additional tests.
24. Change the audio analyzer frequency to 3.183 kHz and depress the 50 uSEC de-emphasis key. The signal should be 1.25 volts peak-to-peak and the period should be 314 microseconds. If not, check for defective U7 or filter R45, C50, or proceed to logic troubleshooting for additional tests.
25. Change the audio analyzer frequency to 2.122 kHz and depress the 75 uSEC de-emphasis key. The signal should be as 1.25 volts peak-to-peak and the period should be 471 microseconds. If not, check for defective U7 or filter R46, C51, or proceed to logic troubleshooting for additional tests.
26. Change the audio analyzer frequency to 212 Hz and depress the 750 uSEC de-emphasis key. The signal should be 1.25 volts peak-to-peak and the period should be 4.7 milliseconds. If not, check for defective U7 or filter R47, C52, or proceed to logic troubleshooting for additional tests.
27. Change the audio analyzer frequency to 1 kHz and depress the de-emphasis OFF key. Note the amplitude of the signal, then depress the MODULATION PM key. The signal should remain the same. If not, check for defective U7 or amplifier AR9, or proceed to logic troubleshooting for additional tests.
28. Change the audio analyzer frequency to 2 kHz. The signal amplitude should decrease to one-half of that in step 27. If not, troubleshoot filter circuit AR9 and associated components.
29. Move the oscilloscope probe to pin 18 of the edge connector. The signal should be as in the previous step. If not, replace defective relay K4.
30. Move the oscilloscope probe to TP6. The signal should be as in the previous step, except that the amplitude should be 2.4 volts peak-to-peak. If not, replace defective AR11.

6-74. LOGIC SIGNALS.

6-75. Proper operation of the FILTER circuits depend on correct logic levels on the following control lines:

IA2-IA7instrument address bus
ID0-ID7instrument data bus

The instrument address lines IA2-IA5 are decoded by U1 to produce latch strobes. IA7 is a write strobe and IA6 is a read strobe. Logic signals from the instrument data bus are transferred into octal latch, U2, when address lines IA2, IA3, IA4, and IA5 are low and IA7 goes from high to low. Similarly data is transferred into U6 when address IA2 is high and IA3-IA5 are low and IA7 goes from high to low.

To troubleshoot the logic circuits proceed as follows:

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1. With the Model 8201 powered up normally and configured as above, depress the INIT key.
2. Use the oscilloscope to monitor activity on the instrument data lines ID0-ID7 on pins 1-7 of the edge connector. All of the data lines should show activity and normal TTL levels. If not, the problem is on the CPU board or the Motherboard interconnect.
3. Set the audio analyzer level to 600 millivolts at 1 kHz and enter 15 MHz into the Model 8201 carrier FREQ display.
4. Connect the oscilloscope probe to pin 16 (IA7) of the edge connector and set the timebase to 0.5 mSEC/DIV.
5. The signal should be a narrow positive pulse indicating a write operation to the instrument circuits. If the signal is incorrect, the problem is on the CPU board or the Motherboard interconnect.
6. Move the oscilloscope probe to pin 15 of U1 and alternately depress the high-pass filter keys. The signal should be as in the previous step, except that the pulse is inverted. If not, replace defective U1.
7. Move the oscilloscope probe to pin 14 of U1 and alternately depress the low-pass filter keys. The signal should be as in the previous step. If not, replace defective U1.
8. Move the oscilloscope probe to pin 2 of U2. Alternately depress the MODULATION AM and FM keys. The signal should change from TTL high to low. If not, replace defective U2 or shorted Q1.
9. Move the oscilloscope probe to pin 5 of U2. Alternately depress the low-pass 220 and 50 keys. The signal should change from TTL high to low. If not, replace defective U2 or shorted U9.
10. Enter the following SPCL functions and note the corresponding activity on pins 6 and 9 of U2.

SPCL	PIN 6	PIN 9
2	low	low
3	high	low
4	low	high

If the indications are incorrect, replace defective U2 or U3.

11. Operate the high-pass filter keys and note the corresponding activity on pins 12, 15 and 16 of U2.

KEY	PIN 12	PIN 15	PIN 16
<10	high	low	low
30	high	high	low
300	high	high	high
3000	high	low	high

If the indications are incorrect, replace defective U2 or U4.

12. Alternately depress the FM and PM keys and observe the corresponding activity on pin 19 of U2.

KEY	PIN 19
FM	high
PM	low

If the indications are incorrect, replace defective U2 or U4.

13. Operate the low-pass filter keys and note the corresponding activity on pins 9, 12, and 15 of U6.

KEY	PIN 9	PIN 12	PIN 15
3	high	low	high

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15	high	low	low
20	low	low	high
50	high	high	high
220	high	high	high

If the indications are incorrect, replace defective U6 or U5.

14. Select the MODULATION FM function, operate the de-emphasis keys and note the corresponding activity on pins 2, 5, and 6 of U6.

KEY	PIN 2	PIN 5	PIN 6
25	low	low	low
50	low	low	high
75	high	low	low
750	high	high	low
OFF	low	high	low

If the indications are incorrect, replace defective U6 or U7.

6-76. TROUBLESHOOTING, DISTORTION ANALYZER BOARD.

6-77. **GENERAL.** Procedures for checking the DISTORTION ANALYZER circuit board are given below. Test points and other measurement points are indicated on the schematic diagram and circuit board overlay, Figures 8-16 and 8-17.

6-78. **EQUIPMENT REQUIRED.** The test equipment required is listed below. See Table 5-1 for critical specifications.

Oscilloscope.....HP 1740A
 Audio Analyzer.....Boonton 1120
 DC voltmeterFluke 8840A

6-79. PROCEDURE.

1. Turn off the instrument and remove the DISTORTION ANALYZER circuit board. (Yellow extractors) Insert the DISTORTION ANALYZER board into the Extender board (Grey extractors), and plug the combination back into the DISTORTION ANALYZER board slot. Extract the FM circuit board (Brown extractors) just far enough to disengage the circuit board connector. Turn the instrument ON and enter 15 MHz into the carrier FREQ display.
2. Measure the dc voltage at pin 20 of A7U8. The voltage should be approximately +5 volts. If not the power supply circuits or the motherboard connectors are defective.
3. Measure the dc voltage at pins 7 and 4 of AR1. The voltages should be +15 and -15 volts respectively. If not the power supply circuits or the motherboard connectors are defective.
4. Set the audio analyzer source to 1 kHz and 600 millivolts.
5. Connect the audio analyzer source output to the FM OUT connector on the rear panel of the Model 8201.

NOTE

For the following oscilloscope measurements, use a high impedance probe.

6. Depress the audio FREQ key and enter 1 kHz into the AUDIO display.
7. Remove the feedback jumper J1 from the header P1.

8. Connect the oscilloscope probe to the edge connector, pin 18. The signal should be a sinewave with an amplitude of about 1.8 volts peak-to-peak, and a period of 1 millisecond. If not, the problem is on the FILTER board, A6.

9. Move the oscilloscope probe to AR1 pin 6. The signal should be as in the previous step, except that the amplitude should be 4.8 volts peak-to-peak. If not, replace defective AR1.

10. Move the oscilloscope probe to AR3, pin 1. The signal should be as in the previous step. Additionally, the dc level should be near zero volts.

11. Temporarily short TP4 to ground. If the dc level returns to zero volts, the problem is between TP2 and TP4, otherwise the problem is between AR3a and TP2. If the signal is okay, proceed to step 14.

12. If the problem is between TP2 and TP4, temporarily short TP2 to ground. The voltage on AR8, pin 7 should be near zero volts. If not, replace defective U3 or AR8, or proceed to logic troubleshooting for additional tests.

13. If the problem is between AR3 and TP2, temporarily short AR3, pin 3 to ground. The voltage on AR3, pins 1 and 7 should be near zero volts. If not, replace defective U3 or AR3, or proceed to logic troubleshooting for additional tests.

14. Move the oscilloscope probe to TP2. The signal should be 4.5 volts peak-to-peak with a period of 1 millisecond. If not, check for defective Q4, Q6, or amplifier AR7b, or proceed to logic troubleshooting for additional tests.

15. Move the oscilloscope probe to TP4. The signal should be as in the previous step. If not, check for defective Q8, Q10, or amplifier AR10a, or proceed to logic troubleshooting for additional tests.

16. Move the oscilloscope probe to AR5, pin 1. The signal should be a 15 volt peak-to-peak squarewave, and the period should be 1 millisecond. If not, replace defective Q1 or AR5.

17. Move the oscilloscope probe to AR5, pin 7. The signal should be a 15 volt peak-to-peak squarewave, and the period should be 1 millisecond. If not, replace defective Q2 or AR5.

18. Change the audio analyzer frequency to 1.1 kHz, 200 millivolts and move the oscilloscope probe to TP3. The signal should be one-half cycle of a sinewave, 7 volts peak for 450 microseconds, and zero volts for 450 microseconds as shown in Figure 6-6, waveform A. If not, check for defective Q2 or amplifier AR9.

19. Move the oscilloscope probe to TP1. The signal should be one-half cycle of a cosinewave, 14 volts peak-to-peak for 450 microseconds, and zero volts for 450 microseconds as shown in Figure 6-6, waveform B. If not, check for defective Q1 or amplifier AR5.

21. Change the audio analyzer frequency to 1 kHz. Connect the oscilloscope probe to AR11, pin 6. Temporarily replace jumper J1. The dc level should be between +10 and -10 volts. If not, check for defective U7 AR10b, or AR11.

22. Change the audio analyzer frequency to 2 kHz, 600 millivolts, and move the oscilloscope probe to AR2, pin 7. The signal should be a sinewave 4.5 volts peak-to-peak and the period should be 0.5 milliseconds. If not, replace defective AR2.

23. Move the oscilloscope probe to U1, pin 7 or 10. The signal should be as in the previous step. If not, check for defective U1 or AR2 or proceed to logic troubleshooting for additional tests.

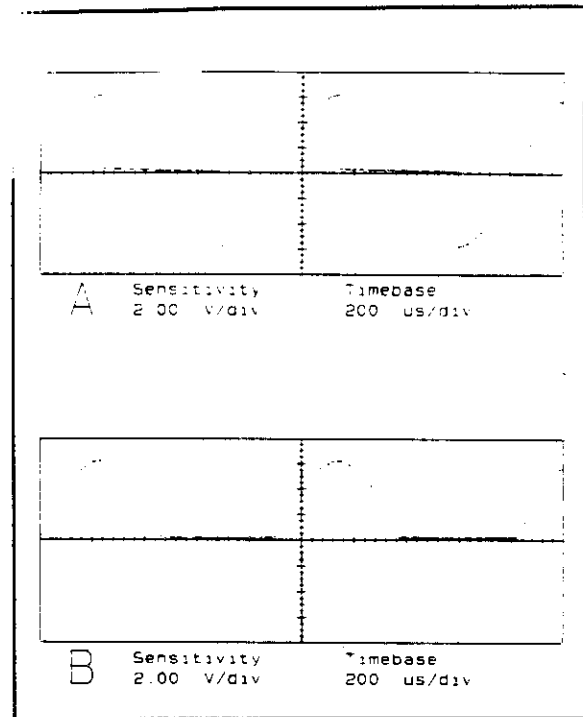


FIGURE 6-6. Distortion Analyzer Waveforms.

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- 24. Change the audio analyzer frequency to 1 kHz and depress the RMS detector key. Allow time for one measurement.
- 25. Connect the oscilloscope probe to U1 pin 7 or 10. The signal should be a sinewave 4.5 volts peak-to-peak and the period should be 1 millisecond. If not, check for defective U1 or AR2, or proceed to logic troubleshooting for additional tests.
- 26. Depress the audio FREQ key, the AUTO key, the + - PEAK key and the DIST key. Set the audio analyzer frequency to 100 Hz.
- 27. Connect the oscilloscope probe to AR2, pin 1. The signal should initially be 4.5 volts peak-to-peak, then the fundamental should be notched out, indicating proper operation of the tuning circuits. If not, check for defective Q3 or Q7, or proceed to logic troubleshooting for additional tests.
- 28. Change the audio analyzer frequency to 5 kHz. The signal should initially be 4.5 volts peak-to-peak, then the fundamental should be notched out, indicating proper operation of the tuning circuits. If not, check for defective Q4 or Q8, or proceed to logic troubleshooting for additional tests.

6-80. LOGIC SIGNALS.

6-81. Proper operation of the DISTORTION ANALYZER circuits depend on correct logic levels on the following control lines:

IA2-IA7instrument address bus
ID0-ID7instrument data bus

The instrument address lines IA2-IA5 are decoded by U1 to produce latch strobes. IA7 is a write strobe and IA6 is a read strobe. Logic signals from the instrument data bus are transferred into dual 8-bit DAC, U3, when address lines IA2, IA4, and IA5 are low, IA3 is high, and IA7 goes from high to low. Similarly data is transferred into U5 and U8 when address IA4 and IA2 are high and, IA3, and IA5 are low and IA7 goes from high to low.

To troubleshoot the logic circuits proceed as follows:

- 1. With the Model 8201 powered up normally and configured as above, depress the INIT key.
- 2. Use the oscilloscope to monitor activity on the instrument data lines ID0-ID7 on pins 1-7 of the edge connector. All of the data lines should show activity and normal TTL levels. If not, the problem is on the CPU board or the Motherboard interconnect.
- 3. Set the audio analyzer level to 600 millivolts at 1 kHz and enter 15 MHz into the Model 8201 carrier FREQ display.
- 4. Connect the oscilloscope probe to pin 16 (IA7) of the edge connector and set the timebase to 0.5 mSEC/DIV.
- 5. The signal should be a narrow positive pulse indicating a write operation to the instrument circuits. If the signal is incorrect, the problem is on the CPU board or the Motherboard interconnect.
- 6. Move the oscilloscope probe to pin 13 of U2, depress the audio FREQ key, and successively enter 1, 2, and then 3 kHz into the display. The signal should be as in the previous step, except that the pulse is inverted. If not, replace defective U2.
- 7. Depress the DIST key and connect the oscilloscope probe to the following pins of U8 with the audio analyzer set for the indicated frequencies. The TTL levels should be as indicated.

FREQ	PIN 5	PIN 6
0.1 kHz	low	low
1 kHz	high	low
10 kHz	low	high

If the levels are not as indicated, replace defective U8.

8. Connect the oscilloscope probe to the following pins of AR12 with the audio analyzer set for the indicated frequencies. The voltage levels should be as indicated.

FREQ	PIN 1	PIN 7
0.1 kHz	-15	-15
1 kHz	-15	0
10 kHz	0	-15

If the levels are not as indicated, replace defective AR12.

6-82. TROUBLESHOOTING, DETECTOR BOARD.

6-83. GENERAL. Procedures for checking the DETECTOR circuit board are given below. Test points and other measurement points are indicated on the schematic diagram and circuit board Figures 8-17 and 8-18.

6-84. EQUIPMENT REQUIRED. The test equipment required is listed below. See Table 5-1 for critical specifications.

OscilloscopeHP 1740A
 Audio AnalyzerBoonton 1120
 Signal Generator.....Boonton 1021
 DC voltmeter.....Fluke 8840A

6-85. PROCEDURE.

1. Turn off the instrument and remove the DETECTOR circuit board. (Green extractors) Insert the DETECTOR board into the Extender board (Grey extractors), and plug the combination back into the DETECTOR board slot. Extract the FM circuit board (Brown extractors) just far enough to disengage the circuit board connector. Turn the instrument power ON, and enter 15 MHz into the carrier FREQ display.
2. Measure the dc voltage at pin 20 of U3. The voltage should be approximately +5 volts. If not the power supply circuits or the motherboard connectors are defective.
3. Measure the dc voltage at pins 7 and 4 of U14. The voltages should be +15 and -15 volts respectively. If not the power supply circuits or the motherboard connectors are defective.
4. Measure the dc voltage at pins 7 and 1 of U23. The voltages should be +5 and -5 volts respectively. If not, troubleshoot regulator U23 using dc measurements.
5. Set the audio analyzer source to 1 kHz and 600 millivolts and connect the audio analyzer source output to the FM OUT connector on the rear panel of the Model 8201. Set the signal generator to 15 MHz, CW, at 0 dBm and connect the generator RF OUT to the RF IN connector on the Model 8201.

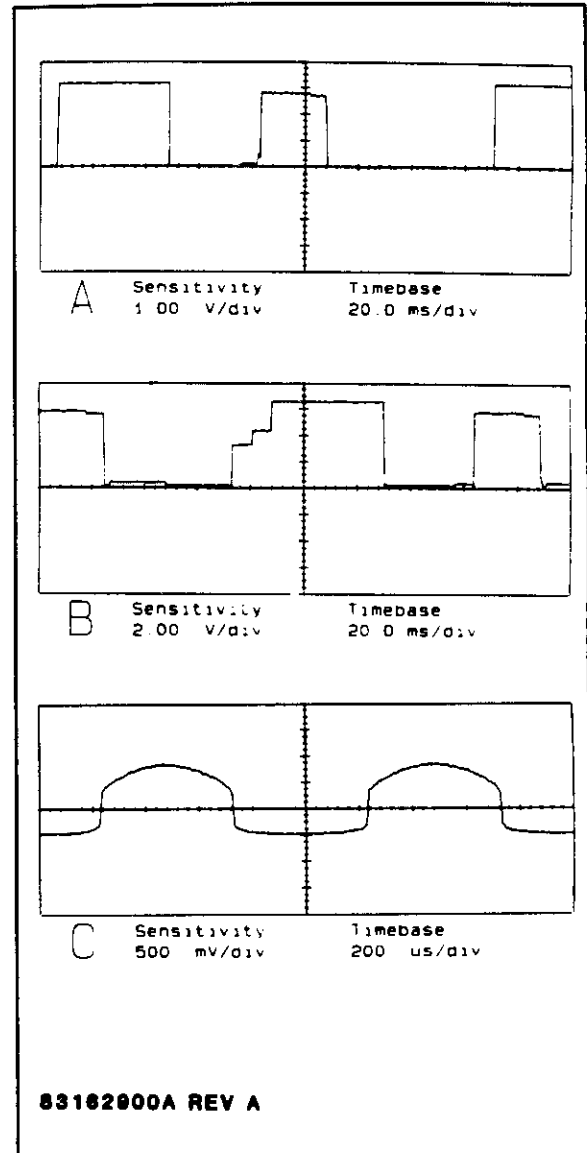


FIGURE 6-7. Detector Board Waveforms.

NOTE

For the following oscilloscope measurements, use a high impedance probe. TP1 can be used as a ground terminal.

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6. Connect the oscilloscope probe to pin 18 of the edge connector. The signal should be a sinewave with an amplitude of about 1.8 volts peak-to-peak and a period of 1 millisecond. If not, the problem is on the Filter board or the Motherboard interconnect.
7. Move the oscilloscope probe to TP5. The signal should be as in the previous step, except it is gated on and off about every 1.5 seconds. If not, check for defective switch U1, or amplifier U13, or proceed to logic troubleshooting for additional tests.
8. Move the oscilloscope probe to TP7. The signal should be as in the previous step. If not, replace defective U13.
9. Move the oscilloscope probe to TP8. The signal should be a low frequency rectangular waveform switching from ground to about + 0.8 volts at a 1.5 second rate. If not, check for defective switch U6, or amplifier U15 or U19, or proceed to logic troubleshooting for additional tests.
10. Move the oscilloscope probe to TP9. The signal should be as in the previous step. If not, check for defective switch U6, or amplifier U16 or U19, or proceed to logic troubleshooting for additional tests.
11. Measure the dc voltage at pin 1 of U7. The voltage should be 1 volt. If not, check filter R30 and C24, or the problem is on the AM board.
12. Move the oscilloscope probe to TP13. The signal should be as in Figure 6-6,A. If not, check for defective switch U7, or amplifier U22, or proceed to logic troubleshooting for additional tests.
13. Measure the dc voltages at pins 19 and 20 of the edge connector. The voltages should be about 0.210 and 0.319 volts respectively. If not, the problem is on the RF board or in the interconnecting cable.
14. Measure the dc voltages at pins 4 and 5 of U9. The voltages should be about 2.1 and 2.2 volts respectively. If not, check the resistive attenuators R33-R35, and R38, R40 and R41, or replace defective U9.
15. Move the oscilloscope probe to TP14. The signal should be as in Figure 6-6,B. If not, check for defective switch U9, or amplifier U22, or proceed to logic troubleshooting for additional tests.
16. Depress the RMS key and move the oscilloscope probe to pin 30 of the edge connector. The signal should be 5 volts peak-to-peak with a period of 1 millisecond. If not, the problem is on the Filter board.
17. Move the oscilloscope probe to pin 3 of U14. The signal should be 0.5 volts peak-to-peak. If not, check for defective switch U5, or amplifier U14, or proceed to logic troubleshooting for additional tests.
18. Move the oscilloscope probe to pin 6 of U14. The signal should be 5.6 volts peak-to-peak. If not, check for defective switch U5, or amplifier U14, or proceed to logic troubleshooting for additional tests.
19. Move the oscilloscope probe to pin 3 of U18. The signal should be 0.56 volts peak-to-peak. If not, check for defective switch U5, or amplifier U18, or refer to logic signals troubleshooting below.
20. Move the oscilloscope probe to pin 6 of U18. The signal should be 6.6 volts peak-to-peak. If not, check for defective switch U5, or amplifier U18, or proceed to logic troubleshooting for additional tests.
21. Move the oscilloscope probe to TP3. The signal should be 0.66 volts peak-to-peak. If not, check for defective switch U4, or amplifier U20, or proceed to logic troubleshooting for additional tests.
22. Move the oscilloscope probe to TP10. The signal should be 7.6 volts peak-to-peak. If not, check for defective rms converter U8, or amplifier U20, or proceed to logic troubleshooting for additional tests.
23. Move the oscilloscope probe to TP11. The signal should be about 2.8 volts dc. If not, check for defective rms converter U8, or switch U9.

24. Move the oscilloscope probe back to TP10 and enter SPCL 3 to set the 50.00 modulation range. Set the audio analyzer to the following levels and observe the resulting waveforms. The ** indication of the indication means that the voltage will be initially higher and then change to the indicated value.

Analyzer Level (millivolts)	Indication (volts peak-peak)
0	baseline noise
0.5	6
1	*6
2	*5
5	*6
10	*6
20	*5
50	*6
100	*6
200	*5
500	*6
1000	12.4

If the indications are incorrect, isolate the defective analog switch U5 or U4, or refer to logic signals troubleshooting below.

25. Set the audio analyzer to 600 millivolts and move the oscilloscope probe to pin 21 of the edge connector. The signal should be 380 millivolts peak-to-peak with a period of 1 millisecond. If not, the problem is on the Filter board.

26. Move the oscilloscope probe to pin 6 of U21. The signal should be as in Figure 6-6,C. If not, replace defective U21.

27. Move the oscilloscope probe to the cathode of CR5. The signal should be a half-wave rectified signal 380 millivolts peak with a period of 1 millisecond. If not, isolate defective component in average detector circuit using dc and waveform measurements.

28. Move the oscilloscope probe to pin 10 of U9. The voltage should be about 0.12 volts dC. If not, isolate defective component R45, C33, or U9.

6-86. LOGIC SIGNALS.

6-87. Proper operation of the DETECTOR circuits depend on correct logic levels on the following control lines:

IA2-IA7.....instrument address bus
ID0-ID7.....instrument data bus

6-88. The instrument address lines IA2-IA5 are decoded by U2 to produce latch strobes. IA7 is a write strobe and IA6 is a read strobe. Logic signals on the instrument data bus are transferred into octal latch, U3, when addresses IA2 and IA5 are low, and IA3 and IA4 are high, and IA7 goes from high to low. Similarly data is transferred into U10 when address when IA5 is low and IA2-IA4 are high, and IA7 goes from high to low. To troubleshoot the logic circuits proceed as follows:

1. With the Model 8201-S/10 powered up normally and configured as in the troubleshooting section, depress the INIT key.
2. Use the oscilloscope to monitor activity on the instrument data lines ID0-ID7 on pins 1-7 of the edge connector. All of the data lines should show activity and normal TTL levels. If not, the problem is on the CPU board or the Motherboard interconnect.

3. Set the audio analyzer level to 600 millivolts at 1 kHz, enter 15 MHz into the Model 8201 carrier FREQ display, and depress the RMS key.
4. Connect the oscilloscope probe to pin 16 (IA7) of the edge connector and set the timebase to 0.5 mSEC/DIV.
5. The signal should be a narrow positive pulse indicating a write operation to the instrument circuits. If the signal is incorrect, the problem is on the CPU board or the Motherboard interconnect.
6. Move the oscilloscope probe to pin 19 of U2 and change the audio analyzer level to 100, then 200, and back to 600 millivolts. The signal should be as in the previous step, except that the pulse is inverted. If not, replace defective U2.
7. Move the oscilloscope probe to pin 18 of U2. The signal should be as in the previous step. If not, replace defective U2.
8. Enter SPCL 3 to hold the 50.00 modulation range, then set the audio analyzer to the indicated levels, in millivolts, and note the activity on pins 2, 5, 6, 9, 12, and 15 of U3.

LEVEL	PIN 2	PIN 5	PIN 6	PIN 9	PIN 12	PIN 15
0	low	low	low	high	low	low
1	high	low	low	low	low	low
2	low	high	low	low	low	low
5	low	low	high	low	low	low
10	high	low	low	low	low	high
20	low	high	low	low	low	high
50	low	low	high	low	low	high
100	high	low	low	low	high	high
200	low	high	low	low	high	high
500	low	low	high	low	high	high
1000	low	low	high	low	high	high

If the indications are incorrect, replace defective U3.

9. Select the PEAK + - detector and move the oscilloscope probe to pin 5 of U10. The signal should be alternating between logic high and logic low with a period of about 1.5 seconds. If not, replace defective U10 or U1.
10. Move the oscilloscope probe to pin 6 of U10. The signal should be similar to the previous step. If not, replace defective U10 or U6.
11. Move the oscilloscope probe to pin 9 of U10. The signal should be similar to the previous step. If not, replace defective U10 or U7.
12. Move the oscilloscope probe to pin 12 of U10. The signal should be similar to the previous step. If not, replace defective U10 or U7.
13. Move the oscilloscope probe to pin 15 of U10. The signal should be similar to the previous step. If not, replace defective U10 or U9.
14. Move the oscilloscope probe to pin 16 of U10. The signal should be similar to the previous step. If not, replace defective U10 or U9.
15. Move the oscilloscope probe to pin 19 of U10. The signal should be similar to the previous step. If not, replace defective U10 or U9.
16. Move the oscilloscope probe to pin 2 of U10. The signal should be a logic 0 (0 volts) If not, replace defective U10 or U1.

6-89. TROUBLESHOOTING, CPU BOARD.

6-90. GENERAL. Procedures for checking the CPU circuit board are given below. Test points and other measurement points are indicated on the schematic diagram and circuit board overlay Figures 8-22 and 8-23. The CPU circuitry in the Model 8201 uses a 16-bit microprocessor in a bus-oriented system. Most of the high speed circuitry is contained on the CPU board and external signals are buffered. As a result, failures of one or more peripheral circuits will generally identify the section to troubleshoot.

6-91. EQUIPMENT REQUIRED. The test equipment required is listed below. See Table 5-1 for critical specifications. Note that for several of the tests a logic probe could be substituted for the oscilloscope.

OscilloscopeHP 1740A
 DC voltmeter.....Fluke 8840A
 Logic Analyzer.....none specified

CAUTION

When extracting or inserting the CPU board, be careful not to damage connector J2, J3, or the associated flat-cable wiring.

6-92. PROCEDURE.

1. With the instrument power off, remove the CPU board (Blue Extractors). Insert the Extender board into the CPU slot and insert the CPU board into the extender board.
2. Measure the dc voltage from the '+' terminal of BT1 to ground. The voltage should be greater than 2.8 volts. If not, proceed to BATTERY REPLACEMENT below.
3. Turn on the instrument power and depress the INIT key if the keyboard is active.
4. Measure the dc voltage at pin 28 of U10. The voltage should be +5 volts. If not, the problem is most likely in the power supply circuits, however, shorted bypass capacitors or open L2 could cause the problem.
5. Measure the dc voltage at pins 8 and 4 of U27. The voltages should be +15 and -15 volts respectively. If not, the problem is most likely in the power supply circuits, however, shorted bypass capacitors or open L1 or L3 could cause the problem.

NOTE

For the following oscilloscope measurements, use a high impedance probe with a short ground connection. A spring clip type ground connection is recommended.

6-93. CLOCK AND TIMING.

6. Connect the oscilloscope probe to pin 1 of U1. The signal should be a TTL level signal with a period of 54 nanoseconds (18.432 MHz). If not, replace defective Y1.
7. Move the oscilloscope to pin 3 of U1. The signal should be a TTL level signal with a period of 108 nanoseconds (9.21 MHz). If not, replace defective U1.
8. Move the oscilloscope to pin 6 of U1. The signal should be a TTL level signal with a period of 271 nanoseconds (3.68 MHz). If not, replace defective U1.
9. Move the oscilloscope to pin 13 of U1. The signal should be a TTL level signal with a period of 542 nanoseconds (1.84 MHz). If not, replace defective U1.

6-94. RESET and POWER FAIL.

10. Connect the oscilloscope to pin 5 of U4. The signal should be TTL logic high. If not, replace a defective U4, or U6.
11. Move the oscilloscope to pin 5 of U3. The signal should be TTL logic high. If not, replace defective U3 or U6.
12. Move the oscilloscope to pin 8 of U3. The signal should be TTL logic high. If not, replace defective U3 or U6.
13. Move the oscilloscope to pin 19 of U9. The signal should be TTL logic high. If not, replace defective U9 or U11.
14. Use a clip lead to momentarily short pin 5 of U4 to ground. Monitor the signal on pin 11 of U9. The signal should be TTL low when U4 pin 5 is ground. If not, replace defective U9.
15. Repeat the procedure but monitor the signal on pin 9 of U9. The signal should be TTL high. If not, replace defective U9.

6-95. CPU AND MEMORY.

16. If the microprocessor is halted LED DS2 will be illuminated. If this is the case a data bus fault has probably occurred. In this event a logic state analyzer is the most direct method of isolating the problem, however, parts substitution could be used as a last resort. The state of the data bus is tabulated below for the first several machine cycles. Refer to the manual for the particular logic analyzer for instructions for connecting to the DATA bus and clock signals. If data pattern errors occur the most likely problem is the eproms, however, DATA or ADDRESS bus shorts could also be the problem.

Address Bus(Hex)	D15-----D00(Binary)
0000000	0000.0000.0000.0000
0000002	1000.1000.1000.1000
0000004	0000.0100.0000.0000
0000400	0010.0000.0011.1001
0000402	1010.1010.1010.1010
0000404	0101.0101.0101.0101
0000406	0010.0000.0011.1001
0000408	1111.1111.1111.1111
000040A	0000.0000.0000.0000
000040C	0100.1110.1111.1001

17. Remove the logic analyzer, turn off the instrument power and remove the CPU board far enough to install jumper, JP2.
18. Turn on instrument power and Monitor the activity on pins 1-4, 37-40, and 18-25 U22. The signal should be a TTL signal with a period of 47.5 milliseconds. If not replace defective U22 or isolate shorted instrument address or data bus line.

6-96. A/D CONVERTER.

6-97. Proper operation of the CPU circuits is necessary for the correct operation of the A/D converter. The A/D conversion is a 13-bit successive approximation technique using a high performance 16-bit D/A converter in a software loop. To troubleshoot the A/D converter, proceed as follows:

19. Select SPCL 38 to activate the D/A converter test program.
20. Connect the oscilloscope to pin 15 of U23. The signal should be a slowly varying signal which moves from -10 to +10 volts. The oscilloscope should be dc coupled for this measurement. If not, replace defective U23.

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21. Select SPCL 39 to activate the A/D measurement test program. Connect the oscilloscope probe to pin 5 of R11. The signal should be as shown in Figure 6-8. If not replace defective U23 or U27.

22. Move the oscilloscope probe to pin 7 of U27. The signal should be negative going TTL pulses about 1 microsecond wide occurring about every 35 microseconds. If not replace defective U27.

6-98. IEEE-488 CONTROLLER.

23. Connect the bus analyzer to the IEEE-488 bus connector on the rear panel of the Model 8201. Set the analyzer as follows:

REN	ON
MEMORY	OFF
COMP	OFF
TALK	active
EXECUTE	HALT
SRQ	0
EOI	0
ATN	0

24. Connect the oscilloscope probe to pin 9 of U24. Operate bus switch 1 on the analyzer alternately from 0 to 1. The signal should alternate between 0 and +3.5 volts. If not, the problem is in the connectors or cable connecting the bus analyzer to the CPU board.

25. Move the oscilloscope probe to pin 12 of U24 and repeat the previous step. The signal should alternate between 0 and +5 volts. If not, replace defective U24 or U19.

26. Repeat the previous two steps for pins 2-8 and 19-13 of U24 using bus analyzer switches 2-8. The results should be the same. If not, replace defective U24 or U19.

27. Connect the oscilloscope probe to pin 2 of U25. Operate the REN switch on the analyzer alternately from 0 to 1. The signal should alternate between 0 and +3.5 volts. If not, the problem is in the connectors or cable connecting the bus analyzer to the CPU board.

28. Move the oscilloscope probe to pin 19 of U25 and repeat the previous step. The signal should alternate between 0 and +5 volts. If not, replace defective U19 or U25.

29. Repeat the previous two steps for pins 3, 7, 8 and 18, 14, 13 of U25 using the bus analyzer IFC, EOI, and ATN switches. The results should be the same. If not, replace defective U19 or U25.

30. Set the bus analyzer bus switches as follows:

8	7	6	5	4	3	2	1
0	1	0	1	0	0	1	0

31. Monitor the activity on pin 1 of U25 and activate the ATN line of the bus analyzer and depress the EXECUTE button. The signal should change from TTL high to low. If not, replace defective U19.

32. Monitor pin 1 of U25 and activate the bus analyzer IFC switch. Pin 1 should go high. If not, replace defective U25.

33. Set the bus analyzer bus switches as follows:

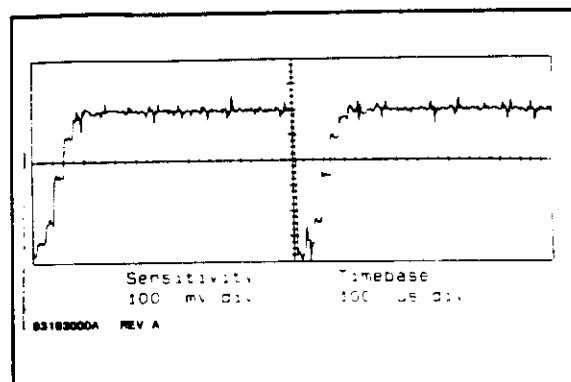


FIGURE 6-8. CPU Board Waveform.

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8	7	6	5	4	3	2	1
0	0	1	1	0	0	1	0

36. Set the REN switch ON, observe the signal on pin 39 of U19 and depress the EXECUTE key on bus analyzer. The signal should pulse low then return high. If not, troubleshoot the Display board.

6-99. BATTERY REPLACEMENT.

6-100. To replace the lithium battery proceed as follows:

1. Remove the instrument top cover as described at the beginning of this section.
2. Carefully disconnect the flat cables from J2 and J3.
3. Extract the CPU board (Blue extractors) and place the board on a flat working surface with the components facing down.
4. Use a low-wattage soldering iron and a solder suction device to remove the solder from the two large circuit pads holding the battery. Remove and discard the old battery.
5. Insert the new battery into the circuit pads, observing polarity, and solder the connections.
6. Install jumpers JP1 and JP2, then replace the CPU board into the Motherboard slot. Reconnect the flat cables to J2 and J3.
7. Turn the Model 8201 ON and observe the FREQUENCY/LEVEL display until the firmware code number and the 'CLEAR' message is displayed. This action clears the variable memory on the CPU board.
8. Turn off the Model 8201, extract the CPU board far enough to remove jumpers JP1 and JP2, then reseal the CPU board and replace the top cover.

6-101. TROUBLESHOOTING, COUNTER BOARD.

6-102. **GENERAL.** Procedures for checking the COUNTER circuit board are given below. Test points and other measurement points are indicated on the schematic diagram and circuit board overlay, Figures 8-24 through 8-27.

6-103. **EQUIPMENT REQUIRED.** The test equipment required is listed below. See Table 5-1 for critical specifications.

- Oscilloscope.....HP 1740A
- DC voltmeterFluke 8840A

6-104. PROCEDURE.

1. Turn off the instrument and remove the Counter board (Violet Extractors). Insert the Counter board into the Extender board (Grey extractors), and plug the combination back into the Counter board slot. Remove the EXT REF connection on the rear panel.
2. Turn on the instrument power and depress the INIT key if the keyboard is active.
3. Measure the dc voltage at pin 16 of U3. The voltage should be +5 volts. If not, the problem is most likely in the power supply circuits, however, shorted bypass capacitors or open L3 could cause the problem.
4. Measure the dc voltage at pins 8 and 4 of AR1. The voltages should be +15 and -15 volts respectively. If not, the problem is most likely in the power supply circuits, however, shorted bypass capacitors or open L1 or L2 could cause the problem.

NOTE

For the following oscilloscope measurements, use a high impedance probe with a short ground connection. A spring clip type ground connection is recommended.

6-105. GATE CIRCUITS.

1. Connect the oscilloscope probe to pin 3 of U20. The signal should be a TTL level signal with a period of 100 nanoseconds (10 MHz). If not, replace defective Y1 or check U20 or U4 for shorted pins.
2. Move the oscilloscope to pin 6 of U20. The signal should be a TTL signal with a period of 200 nanoseconds (5 MHz). If not, replace defective U20.
3. Move the oscilloscope to pin 9 of U20. The signal should be a TTL signal with a period of 400 nanoseconds (2.5 MHz). If not, replace defective U20.
4. Move the oscilloscope to pin 21 of the edge connector. The signal should be a dc level of about + 2.5 volts. If not, check for shorted EXT REF cable or defective U1.
5. Move the oscilloscope to pin 6 of U1. The signal should be TTL low logic level. If not, replace defective U1.
6. Move the oscilloscope to pin 8 of U1. The signal should be TTL high logic level. If not, replace defective U1 or check for shorted U4.
7. Move the oscilloscope to pin 2 of U1. The signal should be TTL low logic level. If not, replace defective U1 or check for shorted U4, C8, or open CR1.
8. Move the oscilloscope to pin 12 of U1. The signal should be TTL high logic level. If not, replace defective U1 or check for shorted U4.
9. Move the oscilloscope to pin 11 of U4. The signal should be a TTL signal with a period of 100 nanoseconds (10 MHz). If not replace defective U4.
10. Move the oscilloscope to pin 6 of U4. The signal should be as in the previous step. If not, replace defective U4 or check for shorted U5 or U9.
11. Move the oscilloscope to pin 7 of U5. The signal should be a TTL signal with a period of 10 microseconds (0.1 MHz). If not, replace defective U5.
12. Move the oscilloscope to pin 7 of U7. The signal should be a TTL signal with a period of 1 millisecond (1 kHz). If not, replace defective U7.
13. Move the oscilloscope to pin 9 of U8. The signal should be a TTL signal with a period of 10 milliseconds (0.1 kHz). If not, replace defective U8.

6-106. SOURCE SIGNALS.

1. Set the signal generator to 15 MHz, 0 dBm, and 45 kHz deviation at a 1 kHz rate.
2. Connect the RF OUT of the generator to the RF IN of the Model 8201. Key 15 MHz into the carrier FREQ display. (Ignore any frequency setting errors which may occur).
3. Connect the oscilloscope probe to pin 30 of the edge connector. The signal should be a sinewave with an amplitude of approximately 10 millivolts peak-to-peak with a period of 26 nanoseconds. If not, the problem is in the oscillator circuits or the interconnecting cable.

4. Move the oscilloscope probe to pin 11 of U1. The signal should be as in the previous step except that the amplitude should be 3 volts peak-to-peak. If not, replace defective Q1 or check for shorted C6, CR2, or U1.
5. Move the oscilloscope probe to pin 10 of U1. The signal should be as in the previous step except that the amplitude should be 3.5 volts peak-to-peak. If not, replace defective U1 or check for shorted U9.
6. Move the oscilloscope probe to pin 32 of the edge connector. The signal should be about 700 millivolts peak-to-peak with a period of 800 nanoseconds. If not, the problem is in the RF circuits or the interconnecting cable.
7. Move the oscilloscope probe to pin 3 of U9. The signal should be as in the previous step except that the amplitude should be 3.5 volts peak-to-peak. If not, replace defective Q2 or check for shorted C5 or U9.
8. Move the oscilloscope probe to pin 34 of the edge connector. The signal should be about 2.2 volts peak-to-peak with a period of 1 millisecond. If not, the problem is on the FILTER board, A6 or the Motherboard interconnect.
9. Move the oscilloscope probe to pin 7 of AR1. The signal should be as a square wave with an amplitude of 5 volts peak-to-peak and a period of 1 millisecond. If not, replace defective AR1 or check for shorted U1 or U2.
10. Move the oscilloscope probe to pin 4 of U1. The signal should be as in the previous step except that the signal swings should be TTL. If not, replace defective U1 or check for shorted U9.
11. Set the signal generator modulation rate to 10 kHz. Enter SPCL function 3 to hold the modulation range setting, then depress the audio **FREQ** key.
12. Connect the oscilloscope probe alternately to pin 2, 6 and 9 of U6. The signal should be a pair of negative TTL pulses occurring about every 1.2 seconds. If not, refer to A9, CPU board troubleshooting.
13. Move the oscilloscope probe to pin 5 of U2. The signal should be as in the previous step except that the pulses are positive going. If not, replace defective U2 or U4.
14. Move the oscilloscope probe to pin 5 of U9. The signal should be a composite TTL signal. One signal has a period of 100 microseconds and is gated by a signal with a period of 100 milliseconds. If not, replace defective U9 or U10.

6-107. COUNTER CHAIN, DECODER, and BUS BUFFERS.

1. Disconnect the Generator signal and depress the **INIT** key on the front panel of the Model 8201.
2. Use the oscilloscope to monitor the activity on the instrument data lines ID0-ID7 on pins 1-8 of the edge connector. All of the data lines should show activity and normal TTL levels. If not, the problem is on the CPU board or the Motherboard interconnect.
3. Select SPCL 36 to activate the counter test program.
4. Connect the oscilloscope to the indicated pin of U3. The strobe signal should be a negative going TTL pulse. If not, check the activity on the instrument address bus IA2-IA7 on pins 11-16 of the edge connector. The correct signals are tabulated below. If these signals are not correct, the problem is on the CPU board, otherwise replace defective U3. State of instrument address lines IA2-IA5 while IA6 is high and the corresponding strobe signal.

IA2	IA3	IA4	IA5	Strobe(U3)
low	low	low	high	pin 15
high	low	low	high	pin 14
low	high	low	high	pin 13
high	high	low	high	pin 12

State of instrument address lines IA2-IA5 while IA7 is high and the corresponding strobe signal.

IA2	IA3	IA4	IA5	Strobe(U3)
high	high	low	high	pin 7

5. Connect the oscilloscope probe to pin 11 of U10. The signal should be TTL composite signal consisting of one waveform with a period of 25 nanoseconds gated off temporarily about every 2.5 seconds. If not, replace defective U9 or U10.
6. Connect the oscilloscope to pin 13 of U10. The signal should be negative TTL pulse signal occurring about every 2.5 seconds indicating proper counter reset action. If not, check bus buffer U15 by monitoring pins 9 and 8 for activity. If these signals are not correct, the problem is most likely on the CPU board.
7. Move the oscilloscope probe to pin 2 of U11. The signal should be as in the previous step, except the pulse is positive going. If not, replace defective U11 or check for shorted U13 or U14.
8. Move the oscilloscope probe to pin 9 of U10. The signal should be TTL composite signal consisting of one waveform with a period of 50 nanoseconds gated off temporarily every 2.5 seconds. If not, replace defective U10 or check for shorted U19.
9. Move the oscilloscope probe to pin 5 of U10. The signal should be similar to the previous step, except the high frequency component of the signal is divided by two. If not, replace defective U10 or check for shorted U19.
10. Move the oscilloscope probe to pin 5 of U12. The signal should be similar to the previous step, except the high frequency component of the signal is divided by two. If not, replace defective U12 or check for shorted U19.
11. Move the oscilloscope probe to pin 9 of U12. The signal should be similar to the previous step, except the high frequency component of the signal is divided by two. If not, replace defective U12 or check for shorted U19.
12. Repeat the above step for pins 9, 7, 6, 5, 3, 2, 4, 13, 12, 14, 15, and 1 of U14. In each case the higher frequency signal component should reduce in frequency by a factor of two for each pin. If not, replace defective U14, or check for shorted U19 or U18.
13. Repeat the above step for pins 9, 7, 6, 5, 3, 2, 4, 13, 12, 14, 15, and 1 of U13. In each case the higher frequency signal component should reduce in frequency by a factor of two for each pin. If not, replace defective U13, or check for shorted U16 or U17.
14. If all of the above checks are correct, but the counter still does not operate properly, the problem is with the bus buffers U16-U19. Isolate the problem by interchanging or replacing the buffers one at a time.

6-108. CALIBRATOR CIRCUITS.

1. Connect the oscilloscope probe to pin 9 of U22. The signal should be a TTL waveform with a period of 800 nanoseconds (1.25 MHz). If not, replace defective U22.
2. Move the oscilloscope probe to pin 15 of U22. The signal should be a TTL waveform with a period of 800 microseconds (1.221 kHz). If not, replace defective U22.
3. Move the oscilloscope probe to pin 12 of U11. The signal should be as in the previous step. If not, replace defective U11 or check for shorted U24.
4. Move the oscilloscope probe to pin 11 of U23. The signal should be a complex TTL waveform with two distinct frequency components. Synchronize the oscilloscope on the negative slope of the signal and adjust the timebase to 0.2 uSEC/DIV. The display should show one signal with a period of 4 divisions and one with a period of 5 divisions. If not, replace defective U23 or check for shorted U24.
5. The signals on pins 2 and 14 of U24 control the output signals on pins 7 and 9. The logic levels and corresponding outputs are:

2	14	7	9
low	low	low	low
low	high	1.25 MHz	1.221 kHz
high	low	1.0/1.25 MHz	high
high	high	low	low

When the calibration routine is activated, the progression is from line 1 to line 2 to line 3 of the above table. Execute the calibration routine by executing SPCL function 30, and observe the results. The signals should be as indicated. If not, replace defective U24 or bus buffer U15.

6. The initial phase of calibration is the AM detector calibration. The signals indicated in the following tests are measured during this initial phase. If the tests are not completed in the time required for one AM calibration cycle, depress the INIT key and then execute SPCL function 30 to resume AM calibration.

7. Connect the oscilloscope to pin 3 of AR3. The signal should be a sinewave with an amplitude of 2 volts peak-to-peak and a period of 800 nanoseconds. If not, isolate the defective component in low-pass filter L5-L6, and C17, C18, and C20 by waveform measurements.

8. Move the oscilloscope to pin 6 of AR3. The signal should be a sinewave with an amplitude of 6.4 volts peak-to-peak and a period of 800 nanoseconds. If not, replace defective AR3.

9. Move the oscilloscope to pin 2 of U21. The signal should be as in the previous step, except the amplitude should be 4.8 volts peak-to-peak. If not, replace defective R20 or U21.

10. Move the oscilloscope to pin 15 of U21. The signal should be as in the previous step, except the amplitude should be 1.6 volts peak-to-peak. If not, replace defective R20 or U21.

11. Move the oscilloscope to pin 1 of U21. The signal should be a TTL waveform with a period of 800 microseconds. If not, check for shorted C19 or open R26 or shorted U21.

12. Move the oscilloscope to pin 3 of U21. The signal should be a sinewave with a period of 800 nanoseconds amplitude modulated by a squarewave with a period of 800 microseconds. The carrier amplitude should have two distinct levels, 1.6 and 4.8 volts peak-to-peak. If not, replace defective U21.

13. Move the oscilloscope to pin 6 of AR2. The signal should be as in the previous step, except the amplitude should be 0.4 and 1.2 volts peak-to-peak. If not, replace defective AR2.

14. If the above tests are all correct, but the problem persists, the trouble is with the RF circuits, or the interconnecting cable.

6-109. TROUBLESHOOTING, I/O BOARD.

6-110. **GENERAL.** Procedures for checking the I/O circuit board are given below. Test points and other measurement points are indicated on the schematic diagram and circuit board overlay, Figures 8-28 and 8-29.

6-111. **EQUIPMENT REQUIRED.** The test equipment required is listed below. See Table 5-1 for critical specifications.

Oscilloscope..... HP 1740A
DC voltmeter Fluke 8840A

6-112. PROCEDURE.

1. With the instrument power off, remove the top and bottom covers.

2. Remove the right side strap handle by removing two 6-32 screws holding the handle covers, and three 6-32 screws holding the handle extrusion.
3. Turn on the instrument power and depress the INIT key if the keyboard is active.
4. Measure the dc voltage at pin 40 of U3. The voltage should be +5 volts. If not, the problem is most likely in the power supply circuits, however, shorted bypass capacitors or defective power connector, J2 could cause the problem.

NOTE

For the following oscilloscope measurements, use a high impedance probe with a short ground connection.

6-113. ADDRESS DECODER.

1. Connect the oscilloscope probe to pin 1 of U1. The signal should be a series of negative going TTL pulses indicating board selection. If not, the problem is on the CPU board or the interconnecting wiring.
2. Move the oscilloscope to pins 2 and 3. Observe a TTL signal indicating activity on the CPU address bus. If not, the problem is on the CPU board or the interconnecting wiring.
3. Move the oscilloscope to TP1. The signal should be a negative going TTL pulse indicating chip select activity for U2. If not, replace defective U1.
4. Move the oscilloscope to TP3. The signal should be a negative going TTL pulse indicating chip select activity for U3. If not, replace defective U1.

6-114. DISPLAY/KEYBOARD CONTROLLERS

1. Connect the oscilloscope probe to pin 3 of U3. The signal should be a TTL logic waveform with a period of 400 nanoseconds. If not, the problem is on the CPU board or the interconnecting wiring.
2. Move the oscilloscope probe to pin 9 of U3. The signal should be a TTL low dc level indicating proper reset circuit operation. If not, the problem is on the CPU board or the interconnecting wiring.
3. Move the oscilloscope probe to pin 21 of U3. The signal should be a TTL logic waveform indicating proper operation of the CPU A1 address line. If not, the problem is on the CPU board or the interconnecting wiring.
4. Move the oscilloscope probe to pins 10 and 11 of U3. The signal should be a TTL logic waveform indicating proper operation of the CPU read and write lines. If not, the problem is on the CPU board or the interconnecting wiring.
5. Move the oscilloscope probe to pin 22 of U3. The signal should be a negative going TTL pulse indicating read and write activity. If not, the problem is in the decoder section. See above.
6. Move the oscilloscope probe to pin 22 of U2. The signal should be as in the previous step. If not, the problem is in the decoder section. See above.
7. Enter 1 GHz into the carrier FREQ display and monitor the activity on pins 23-35 of U3. The signals should be TTL logic waveforms indicating proper multiplexing of the display information. If not, replace defective U3 or check for shorted connections in J3.

NOTE

The I/O board may be removed if necessary to isolate a defective J3 or Display board.

8. Repeat the measurements of step 7 on U2. The results should be the same. If not, replace defective U2 or proceed as in the previous step.

9. Move the oscilloscope probe to pin 38 of U2 and hold down the 3 kHz low-pass key. The signal should be a negative going TTL pulse indicating correct operation of the keyboard decoder. If not, the problem is on the display or keyboard.

10. Repeat the previous step with the following pins and keys:

U2 pin number	key depressed
39	15kHz
1	20 kHz
2	50 kHz
5	220 kHz
6	QUASI-PEAK
7	RMS
8	HOLD

6-115. TROUBLESHOOTING, DISPLAY/KEYBOARD.

6-116. GENERAL. Procedures for checking the DISPLAY/KEYBOARD circuits are given below. Test points and other measurement points are indicated on the schematic diagram and circuit board overlay, Figures 8-30 through 8-35.

6-117. EQUIPMENT REQUIRED. The test equipment required is listed below. See Table 5-1 for critical specifications.

- Oscilloscope.....HP 1740A
- DC voltmeterFluke 8840A

6-118. PROCEDURE.

1. With the instrument power off, remove the top and bottom covers. Extract the CPU (blue extractors) far enough to install jumper JP2, then reseal the CPU board.

2. Remove the display and front panels as described above to gain access to the display and keyboards.

3. Turn the instrument power ON. The instrument should power up normally, and then illuminate all displays, annunciators, and keyswitch LEDs. If any of the display segments or individual LEDs are not illuminated the associated display or switch LED is most likely defective. Groups of displays with missing segments or groups of keyswitch LEDs not illuminated indicates a defective driver or decoder.

4. Turn the instrument power OFF and remove the keyboard by removing eight 6-32 screws and gently pulling the board away from the display board.

5. Turn the instrument power ON and measure the dc voltage at pin 20 of U13. The voltage should be + 5 volts. If not, the problem is most likely in the power supply circuits, however, shorted bypass capacitors or defective power connector, J4 on the I/O board could cause the problem.

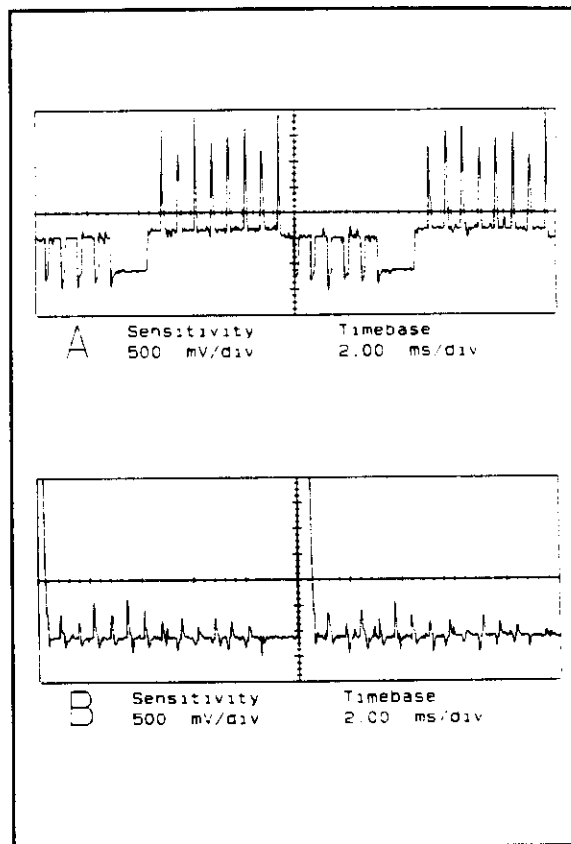


FIGURE 6-9. Display Board Waveforms.

NOTE

For the following oscilloscope measurements, use a high impedance probe with a short ground connection.

6-119. FREQUENCY/LEVEL AND AUDIO DISPLAYS.

1. Connect the oscilloscope probe to pins 1 through 8 of U1 and verify that the segment drive signals are active. If not, the problem is on the I/O board or connector P3.
2. Move the oscilloscope to pins 11-18 of U1. The signal should appear as in Figure 6-7,A. If not, replace defective U1.
3. Repeat the measurements of the previous step on U3. The results should be the same. If not, replace defective U3.
4. Move the oscilloscope probe to pin 1 of U2. The signal should be a TTL squarewave with a period of 1.3 milliseconds, indicating correct operation of the display controllers on the I/O board. If the signal is not present, the problem is on the I/O board or the connector P3.
5. Repeat the previous step for pins 2, 3, and 5 of U2. The signal is similar with a period of 2.5, 5, and 10 milliseconds respectively. If the signals are not present, the problem is on the I/O board or the connector P3.
6. Move the oscilloscope to pin 15 of U2. The signal should be a negative going TTL pulse about 0.6 milliseconds wide occurring every 10 milliseconds. If not, replace defective U2.
7. Repeat the previous step for pins 7, and 9 through 14 of U2. The results should be the same. If not, replace defective U2.
8. Repeat the previous step for pins 7, and 9 through 15 of U4. The results should be the same. If not, replace defective U4.
9. Move the oscilloscope to pin 18 of U5. The signal should be as in the previous step. If not, replace defective U5.
10. Repeat the previous step for pins 3, 5, 7, 9, 12, 14, and 16 of U5. The results should be the same. If not, replace defective U5.
11. Repeat the previous step for pins 3, 5, 7, 9, 12, 14, 16, and 18 of U6. The results should be the same. If not, replace defective U6.
12. Move the oscilloscope to pin 1 of U5. The signal should be a negative going TTL pulse 150 microseconds wide occurring every 0.64 milliseconds, indicating correct operation of the display controller blanking signal on the I/O board. If not, the problem is on the I/O board or connector, P3.
13. Move the oscilloscope to pin 18 of U7. The signal should be as in Figure 6-7,B. If not, replace defective U7.
14. Repeat the previous step for pins 11 through 17 of U7. The results should be the same. If not, replace defective U7.
15. Repeat the previous step for pins 13 through 18 of U8. The results should be the same. If not, replace defective U8.

6-120. MODULATION, SPCL/PRGM, AND KEYSWITCH LEDS.

1. Connect the oscilloscope probe to pins 1 through 8 of U9 and verify that the segment drive signals are active. If not, the problem is on the I/O board or connector P3.
2. Move the oscilloscope to pins 11-18 of U9. The signal should appear as in Figure 6-8,A. If not, replace defective U9.
3. Repeat the previous step using U11. The results should be the same. If not, replace defective U11.
4. Move the oscilloscope probe to pin 1 of U10. The signal should be a TTL squarewave with a period of 1.3 milliseconds, indicating correct operation of the display controllers on the I/O board. If the signal is not present, the problem is on the I/O board or the connector P3.
5. Repeat the previous step for pins 2, 3, and 6 of U10. The signal is similar with a period of 2.5, 5, and 10 milliseconds respectively. If the signals are not present, the problem is on the I/O board or the connector P3.

6. Move the oscilloscope to pin 15 of U10. The signal should be a negative going TTL pulse about 0.6 milliseconds wide occurring every 10 milliseconds. If not, replace defective U10.
7. Repeat the previous step for pins 7, and 9 through 14 of U10. The results should be the same. If not, replace defective U10.
8. Repeat the previous step for pins 7, and 9 through 15 of U12. The results should be the same. If not, replace defective U12.
9. Move the oscilloscope to pin 18 of U13. The signal should be as in the previous step. If not, replace defective U13.
10. Repeat the previous step for pins 3, 5, 7, 9, 12, 14, and 16 of U13. The results should be the same. If not, replace defective U13.
11. Repeat the previous step for pins 3, 5, 7, 9, 12, 14, 16, and 18 of U14. The results should be the same. If not, replace defective U14.
12. Move the oscilloscope to pin 1 of U13. The signal should be a negative going TTL pulse 150 microseconds wide occurring every 0.64 milliseconds, indicating correct operation of the display controller blanking signal on the I/O board. If not, the problem is on the I/O board or connector, P3.
13. Move the oscilloscope to pin 18 of U15. The signal should be as in Figure 6-9,B. If not, replace defective U15.
14. Repeat the previous step for pins 11 through 17 of U15. The results should be the same. If not, replace defective U15.
15. Repeat the previous step for pins 11, and 14 through 18 of U16. The results should be the same. If not, replace defective U16.
16. Replace the keyboard, but do not replace the mounting hardware at this time.

6-121. KEYBOARD.

1. Connect the oscilloscope probe to pins 1 through 8 of J1 and verify that the segment drive signals are similar to Figure 6-9,A. If not, the problem, is on the Display board or connector J1.
2. Move the oscilloscope to pins 9-13 of J1. The signal should be a appear as in Figure 6-9,B. If not, the problem is on the Display board or connector J1.
3. Move the oscilloscope to pins 1 through 8 of J2. The signal should be a negative going TTL pulse about 0.6 milliseconds wide occurring every 5 milliseconds. If not, the problem is on the Display board or connector J2.
4. Move the oscilloscope to pin 13 of J2 and depress the PRGM key. The signal should be as in the previous step while the key is depressed. If not, the keyswitch is defective.
5. Refer to the schematic diagram for the keyboard and observe the signals on the RL lines as the keyswitches are operated. When none of the keyswitches is depressed, the RL lines should be at TTL high. When the switches are depressed the strobe signal described in the previous steps should be present.
6. Replace the keyboard mounting hardware and reassemble the front panel and display windows.

Section 6

6-122. ADJUSTMENTS.

6-123 The instrument adjustment procedure is described below. The adjustment order is not critical, however, the following sequence is recommended.

6-124. **RF board Adjustments.** There are four adjustments associated with the RF circuit board. These are:

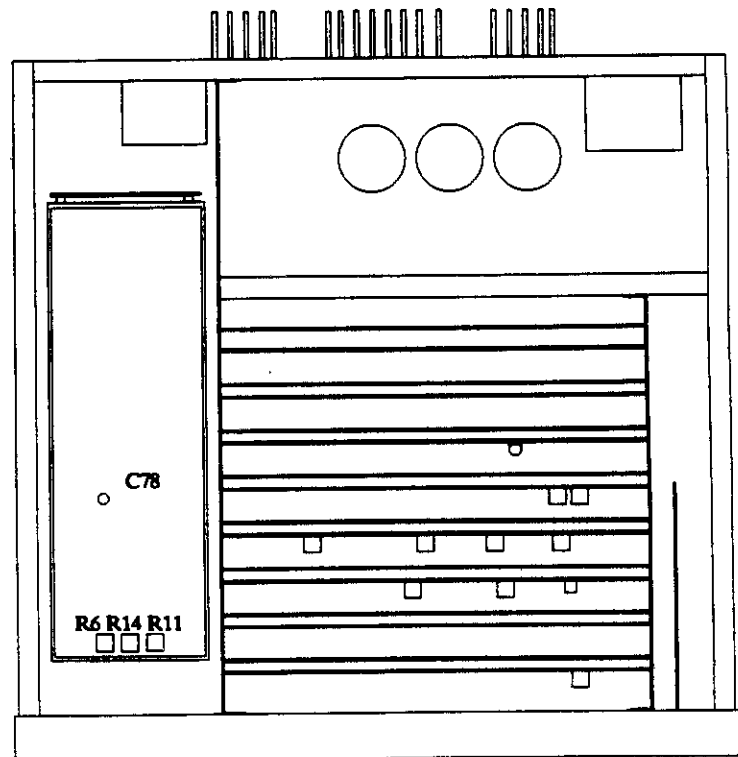
ADJUSTMENT	PURPOSE
R14	sampling bridge balance
R11	sampling bridge bias, low bands
R6.....	sampling bridge bias, high bands
C78	IF flatness

6-125. **Equipment Required.** The equipment required to make the adjustments is listed below. See Table 5-1 for critical specifications.

Low-pass Filter.....	Mini-Circuits NLP-50
Oscilloscope.....	HP 1740A
Signal Generator.....	Boonton 1021
Power Meter.....	Boonton 4200

6-126. Procedure.

1. Connect the power meter to the RF IN connector of the Model 8201 and set the carrier **FREQ** to 11.0 MHz. Adjust R14 for a minimum power indication.
2. Set the signal generator to 9.9 MHz, + 10 dBm, and about 100 kHz deviation at a 1 kHz rate. Set **AM modulation** to OFF.
3. Depress the **INIT** key and enter 9.9 MHz into the carrier **FREQ** display. Select the 300 Hz high-pass, 3 kHz low-pass, and de-emphasis OFF filters.
4. Connect the generator, through the low-pass filter, to the RF IN connector of the Model 8201.
5. Adjust the generator deviation for a Model 8201 indication of 100 +- 5 kHz deviation.
6. Set the oscilloscope to 0.05 V/DIV and 0.5 mSEC/DIV and connect the Model 8201 AF OUT to the vertical input of the oscilloscope using a shielded BNC cable.
7. Depress the **AM** key and adjust R11 for minimum peak-to-peak deflection on the oscilloscope.
8. Change the generator and Model 8201 frequency to 18.5 MHz.
9. Adjust C78 for minimum peak-to-peak deflection on the oscilloscope.
10. Change the generator and Model 8201 frequency to 10.02 MHz.



Maintenance

11. Adjust R6 for minimum peak-to-peak deflection on the oscilloscope. Note R6 may be at or near one end when the deflection is minimum.

6-127. **Oscillator Board Adjustments.** There are three adjustments on the Oscillator circuit board. These are:

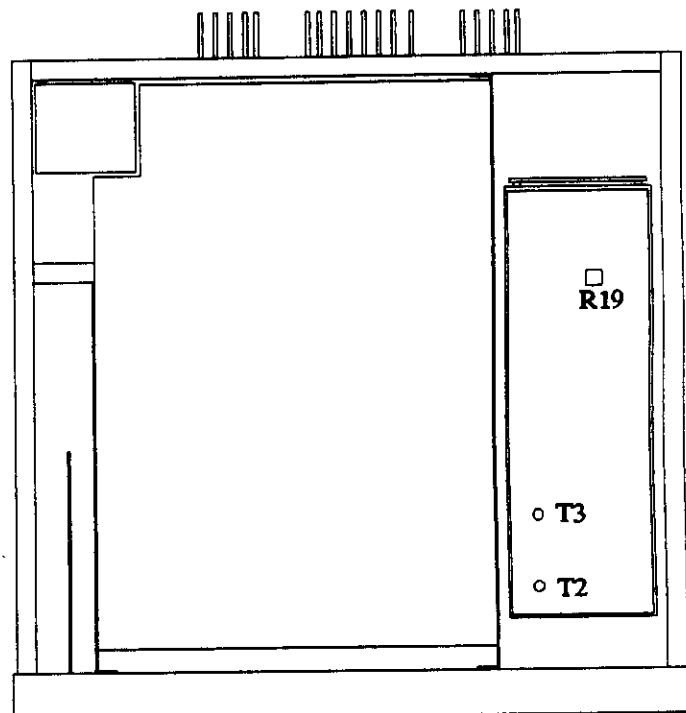
ADJUSTMENT	PURPOSE
T2.....	Oscillator 1 tuning
T3.....	Oscillator 2 tuning
R19	Discriminator centering

6-128. **Equipment Required.** The equipment required to make the adjustments is listed below. See Table 5-1 for critical specifications.

Signal Generator	Boonton 1021
DC voltmeter	Fluke 8840A

6-129. **Procedure.**

1. Select SPCL 37 to activate the local oscillator test program. Depress the DEL(↑) key until the modulation display reads "0 -- LO".
2. Use a nonmetallic screw driver to adjust the slug in T2 until the FREQUENCY/LEVEL display indicates 19.9 + - 0.05 MHz.
3. Depress the DEL(↑) key until the modulation display reads "1 -- LO".
4. Use a nonmetallic screw driver to adjust the slug in T3 until the FREQUENCY/LEVEL display indicates 23.8 + - 0.05 MHz.
5. Depress the LCL/INIT key, enter 15 MHz into the carrier FREQ display, and connect the signal generator RF OUT to the Model 8201 RF IN connector.
6. Set the generator frequency to 1.211 MHz CW and 0 dBm.
7. Monitor the dc voltage at TP1 and adjust R19 for an indication of 0 + - 0.02 volts.



83165600A

6-130. **AM Board Adjustments.** There is one adjustment on the AM circuit board. This is:

ADJUSTMENT	PURPOSE
R85	AM detector offset

6-131. **Equipment Required.** No additional equipment is required to make the adjustment.

6-132. **Procedure.**

1. Power on the Model 8201 and depress the INIT key.

2. Enter 15 MHz into the carrier FREQ display and depress the LEVEL key.
3. Observe the CARRIER display and adjust R85 full clockwise, and then counter-clockwise for an indication of - 70.8 dBm. Note that the indication will jump in approximately 1 dB increment during the adjustment.

6-133. **Distortion Analyzer Board Adjustments.** There are two adjustments on the DISTORTION ANALYZER circuit board. These are:

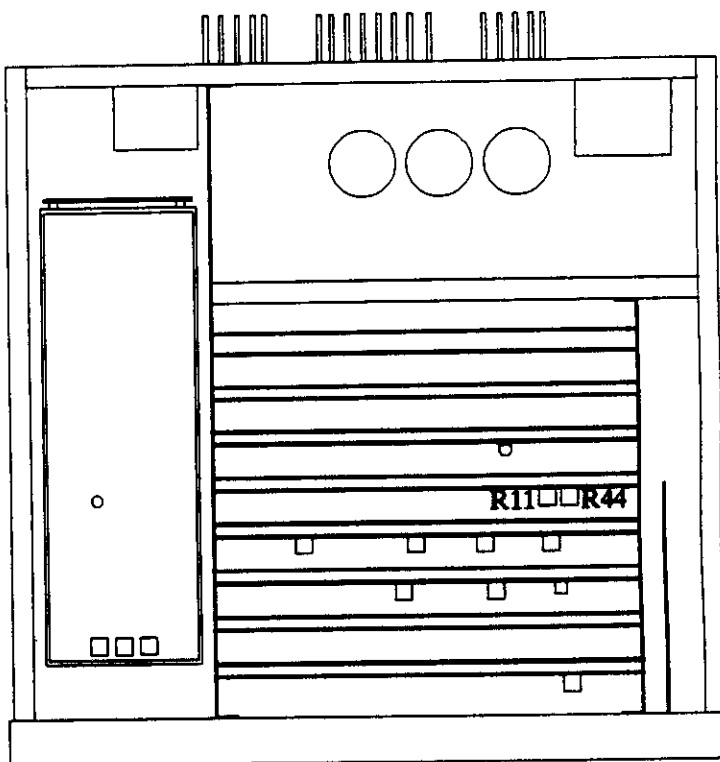
ADJUSTMENT	PURPOSE
R11	Balance offset
R44	Tune offset

6-134. **Equipment Required.** The equipment required to make the adjustments is listed below. See Table 5-1 for critical specifications.

Audio Analyzer	Bornton 1120
Wave Analyzer	HP3581A

6-135. **Procedure.**

1. With the instrument power off, extract the FM board (Brown extractors) only far enough to disconnect the card-edge connector.
2. Set the audio analyzer source to 600 millivolts at a 1 kHz rate.
3. Connect the audio analyzer source output to the FM OUT connector on the rear panel of the Model 8201.
4. Turn on the instrument power and depress the INIT key.
5. Enter 15 MHz into the carrier FREQ display and depress the DIST key.
6. Connect the wave analyzer to the DIST OUT connector on the rear panel of the Model 8201.
7. Set the wave analyzer controls as follows:



SCALE:	90 dB
FREQUENCY:	1000 Hz
AMPLITUDE REF LEVEL:	NORMAL
INPUT SENSITIVITY:	-60 dB
SWEEP MODE:	OFF
RESOLUTION BANDWIDTH:	3 Hz

8. Observe the wave analyzer, and alternately adjust R11 and R44 for a minimum indication. The null should be greater than 100 dB (-60 dB reference plus a -40 dB scale indication).

9. Turn the instrument power OFF and install the FM board into the appropriate Motherboard connector.

R85

6-136. Detector Board Adjustments. There is one adjustment on the DETECTOR circuit board. This is:

ADJUSTMENT	PURPOSE
C23	RMS detector frequency response

6-137. Equipment Required. The equipment required to make the adjustments is listed below. See Table 5-1 for critical specifications.

Audio Analyzer	Boonton 1120
DC voltmeter	Fluke 8840A

6-138. Procedure.

1. With the instrument power off, extract the FM board (Brown extractors) only far enough to disconnect the card-edge connector.

3. Set the audio analyzer to 600 millivolts at a 1 kHz rate.

4. Connect the audio analyzer source to the FM OUT connector on the rear panel of the Model 8201.

5. Turn on the instrument power and depress the INTT key.

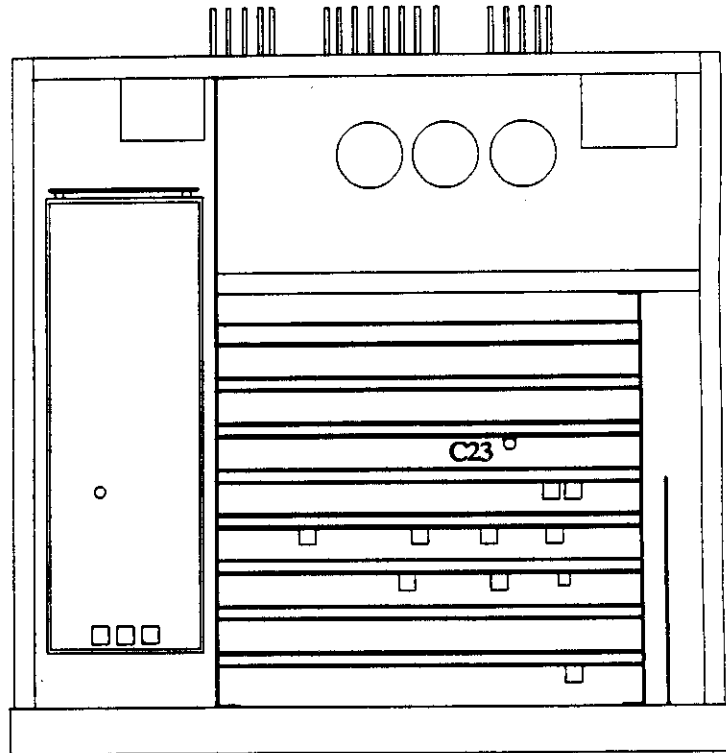
6. Execute SPCL function 18, enter 15 MHz into the carrier FREQ display, and select the 220 kHz low-pass filter. When the MODULATION display settles, select the RATIO % display mode.

7. Set the audio analyzer to 100 kHz and note the modulation ratio indication.

8. Change the audio analyzer frequency back to 1 kHz and select the RMS detector. Depress the RATIO key twice to restore the 100.0 % indication.

9. Set the audio analyzer to 100 kHz and adjust C23 until the ratio indication on the Model 8201 display is 100.0%.

10. Turn the instrument power OFF, remove the audio analyzer connection, and reseal the FM board into the motherboard connector.



6-139. Optional Filter Board Adjustments. There are four adjustments on the OPTIONAL FILTER circuit board. These are:

ADJUSTMENT	PURPOSE
R5	LOOP-THRU filter gain adjust
R8	CCITT bandpass filter gain adjust
R10	CCIR bandpass filter gain adjust
R13	C-MESSAGE bandpass filter gain adjust
R11	CCIR response

6-140. Equipment Required. The equipment required to make the adjustments is listed below. See Table 5-1 for critical specifications.

Audio AnalyzerBoonton 1120

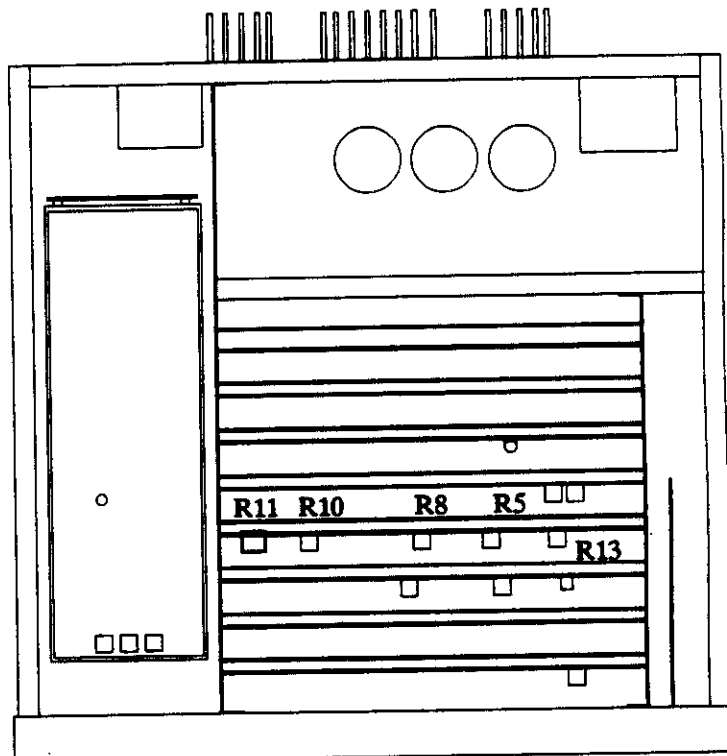
6-141. Procedure.

1. With the instrument power off, extract the FM board (Brown extractors) only far enough to disconnect the card-edge connector.
2. Set the audio analyzer to 600 millivolts at a 1 kHz rate.
3. Connect the audio analyzer source to the FM OUT connector on the rear panel of the Model 8201.
4. Turn on the instrument power and depress the INIT key.
5. Execute SPCL function 18, enter 15 MHz into the FREQUENCY/LEVEL display and select the 220 kHz low-pass filter, and the RMS detector.
6. When the MODULATION display settles, set the audio analyzer to 1 kHz (800 Hz for CCITT), and select the RATIO % display mode.
6. Depress the ALT and appropriate high-pass key to select the filter.
7. Adjust R5 for THRU, R8 for CCITT, R10 for CCIR, or R13 for C-MESSAGE for an indication of 100.0 %.

NOTE

Complete the following steps for the CCIR filter only.

8. Depress the RATIO key on the Modulation Analyzer to disable this function.
9. Set the audio analyzer to 6.300 kHz and adjust the Analyzer Source LEVEL for an indication of about 49 kHz deviation with the CCIR filter active.
10. Depress the Modulation Meter RATIO and dB/dBm keys to establish a 0.0 dB reference.
11. Change the Analyzer Source frequency to 1.000 kHz, then adjust R11 on the CCIR filter board for an indication of -12.20 +/- 0.05 dB.
12. Change the Analyzer Source frequency back to 6.300 kHz. If the display is not 0.00 +/- 0.05 dB, repeat steps 9 through 13.



Maintenance

6-142. **Optional 50 MHz Calibrator Adjustment.** There is one adjustment on the 50 MHZ CALIBRATOR assembly. This is:

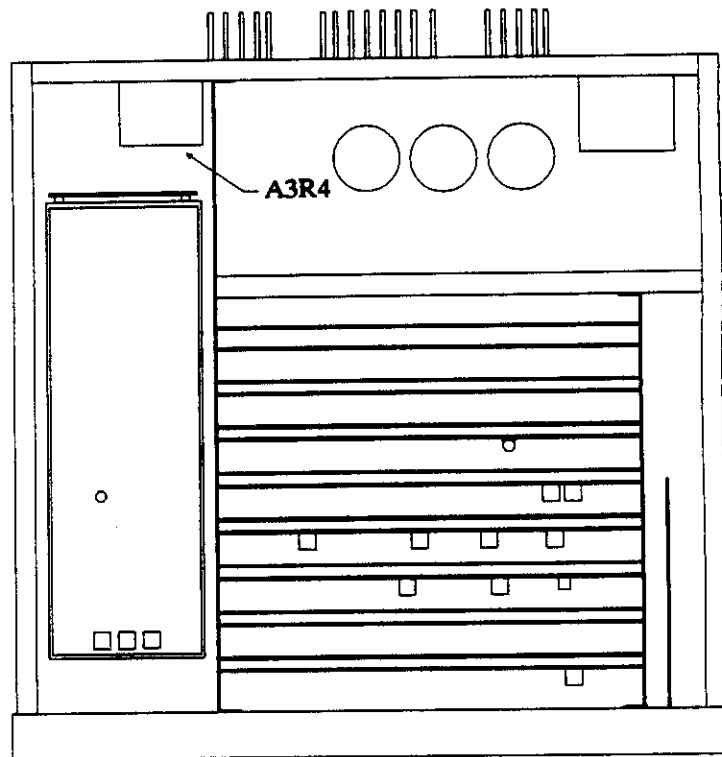
ADJUSTMENT	PURPOSE
R4	Output power level adjust

6-143. **Equipment Required.** The equipment required to make the adjustments is listed below. See Table 5-1 for critical specifications.

Milliwatt Test Set **W&G EPM-1 with TK-10**

6-144. **Procedure.**

1. Connect the EPM-1 probe to the Milliwatt Test Set reference output with the range set to 0 dBm and resistance set to 50 ohms. Adjust the calibration control for a zero indication.
2. Power on the Modulation Analyzer and allow at least 30 minutes for warmup.
3. Connect the EPM-1 probe to the PWR REF output on the rear panel of the Modulation Analyzer.
3. Adjust R4 until the Milliwatt Test Set indicates 0.0 dBm.



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SECTION VII PARTS LIST

7-1. INTRODUCTION.

7-2. The replaceable parts for the Model 8201 are listed in Table 7-2. The replaceable parts list contains the reference symbol, description, manufacturer, and both the BEC and manufacturer part numbers. Table 7-1 lists the manufacturer's federal supply code numbers.

TABLE 7-1. MANUFACTURERS FEDERAL SUPPLY CODE NUMBERS.

00853	Sangamo Electronics	31935	Siemens
00213	Nytronics	31918	ITT Schadow, Inc.
00241	Fenwall Electronics	32293	Intersil, Inc.
01121	Allen Bradley	32575	AMP
01295	Texas Instruments	32997	Bourns
02114	Ferroxcube Corp.	33297	NEC
02735	RCA Solid State Division	33883	RMC
03888	Pyrofilm (KDI)	34078	Midwest Microwave
03911	Clairex Corporation	34371	Harris Semiconductor
04222	AVX Ceramics Company	4S177	International Manufacturing Services
04713	Motorola Semiconductor	50316	Minis Systems Inc.
04901	Boonton Electronics Corporation	51406	Murata Corporation of America
06383	Panduit Corporation	51640	Analog Devices, Inc.
06665	Precision Monolithics	54420	Dage - MTI
06776	Robinson Nugent, Inc.	54426	Buss Fuses
07263	Fairchild Semiconductor	54473	Panasonic
11961	Semicon	55153	Dielectric Labs Inc.
13812	Dialco Division of Amperex	56289	Sprague Electric Company
13919	Burr Brown Corporation	57582	Kahgan Electronics Corporation
14655	Cornell-Dubilier	59474	Jeffers Electronics Inc.
14674	Corning Glass	59660	Tusonix
14752	Electro Cube, Inc.	60395	XICOR
15542	Mini Circuits Labs.	61637	Kemet - Union Carbide
15546	Centralab	61935	Schurter
17117	Electronics Molding Co.	64537	Pyrofilm (KDI)
17856	Siliconix, Inc.	71450	CTS Corporation
18324	Signetics Corporation	73138	Beckman Instruments, Helipot Division
19505	Applied Eng'r. Products	81654	Monitor Products
19701	Mepco Electra	82389	Switchcraft
20307	Arco - Micronics	91293	Johanson
24226	Gowanda Electronics	91637	Dale Electronics
24253	Pomona	95077	Solitron Microwave
24931	Specialty Connector	95348	Gordos Corporation
27014	National Semiconductor	95721	Quality Components Corporation
27264	Molex, Inc.	98291	Sealectro Corporation
27735	F-Dyne Electronics	S4217	United Chemicon, Inc.
28480	Hewlett-Packard Corporation	TOSH	Toshiba America, Inc.
29996	American Technical Ceramics	HITAC	Hitachi America, Inc.
31313	Components Corporation	NDK	NDK Inc.
31781	EDAC	ARMT	Aromat Corporation

TABLE 7-2. Model 8201 Parts List.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR PART NO.	QTY	BEC PART NO.
99402300A		REV: A*	MODEL 8201		
A1	PWA '8201' MOTHER	04901	08251903A	1	08251903A
A2	'8200' RF HOUSING ASSY	04901	08250502A	1	08250502A
A3	50 MHZ CALIBRATOR ASSY	04901	08254200A	1	08254200A
A4	PWA '8200' FM	04901	08252200A	1	08252200A
A5	PWA '8200' AM	04901	08251300B	1	08251300B
A6	PWA '8201' FILTER	04901	08265300A	1	08265300A
A7	PWA '8201' DISTORTION ANALYZER	04901	08252001A	1	08252001A
A8	PWA '8201' DETECTOR	04901	08262201A	1	08262201A
A9	PWA '8201' CPU	04901	08262101A	1	08262101A
A10	PWA '8200' COUNTER	04901	08251600B	1	08251600B
A11	PWA '8200-S/10' I/O	04901	08257500A	1	08257500A
A12	PWA '8200' DISPLAY	04901	08251800B	1	08251800B
A13	PWA '8201' KEYBOARD	04901	08251703A	1	08251703A
A14	PWA EXTENDER 36 PIN	04901	08252300A	1	08252300A
A15	PWA OPTIONAL FILTER	04901	08262400A	1	08262400A
A22	'8201' FRAME ASSY	04901	08265103A	1	08265103A
A23	'8201' REAR PANEL ASSEMBLY	04901	08250704A	1	08250704A
A25	'8201' SUB PANEL ASSEMBLY	04901	08265500A	1	08265500A
A30	PROTECT/ATTN HOUSING	04901	08265700A	1	08265700A
AT1	ATTENUATOR 3dB PAD 444-3	34078	444-3	1	56202300A
W1	CABLE ASSY SEMIFLEX SMA	04901	57231604A	1	57231604A
W2	CABLE ASSY COAX RG316/U 19.25L	04901	572215000	1	572215010
W3	CABLE ASSY COAX RG316/U 19.25L	04901	572213000	1	572213000
W4	CABLE ASSY COAX RG316/U 17.25L	04901	572214000	1	572214000
W5	CABLE ASSY COAX RG316/U 18.50L	04901	572212000	1	572212000
W6	CABLE ASSY COAX RG316/U 9.75L	04901	572206000	1	572206000
W7	CABLE ASSY FLAT 24 CKT 9.00 L	04901	92017600A	1	92017600A
W8	CABLE ASSY FLAT 26 CKT 18.50L	04901	92019400A	1	92019400A
A1					
08251903A		REV:	PWA '8201' MOTHER		
A1W1	CABLE ASSY WIRE 22GA 2C 6.500L	04901	571206000	1	571206000
A1W6	CABLE ASSY WIRE 22GA 2C 11.00L	04901	571206000	1	571206000
AR2	IC TL072CP DUAL OP AMP	01295	TL072CP	1	535092000
AR3	IC 356P OP AMP	04713	LF356N	1	535040000
C1	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C2-3	CAP EL 220uF 20% 50V	S4217	SM-50-VB-220	2	283359000
C4-5	CAP CER 0.1uF 20% 25V	51406	DD312E10Y5P104M25V	2	224364000
C6	CAP EL 26000uF 20% 16V	56289	622D263M016AC2A	1	283340000
C7	CAP CER 0.1uF 20% 25V	51406	DD312E10Y5P104M25V	1	224364000
C8	CAP EL 4500uF 20% 35V	56289	622D452M035AA2A	1	283336000
C10	CAP EL 4500uF 20% 35V	56289	622D452M035AA2A	1	283339000
C11	CAP CER 0.001uF 10% 100V	04222	SR151C102KAA	1	224270000
C13	CAP TANT 10uF 20% 25V	56289	196D106X0025KA1	1	283293000
C14	CAP EL 100uF 20% 25V	S4217	SM-25-VB-101M	1	283334000
C15	CAP MICA 270pF 5% 50V	57582	KD5271J101	1	205045000
C16	CAP CER 0.1uF 20% 25V	51406	DD312E10Y5P104M25V	1	224364000
C18-19	CAP TANT 10uF 20% 25V	56289	196D106X0025KA1	2	283293000
C21	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR PART NO.	QTY	BEC PART NO.
C22	CAP TANT 10uF 20% 25V	56289	196D106X0025KA1	1	283293000
C24	CAP CER 0.01uF 20% 500V	33883	BGP Z5U W/FDCL	1	224271000
C25	CAP TANT 10uF 10% 35V	56289	196D106X903PE4	1	283353000
CR2	DIODE BRIDGE FWLD-50	11961	FWLA-50	1	532028000
CR3-6	DIODE SIG 1N4001	04713	1N4001	4	530151000
CR7	DIODE ZENER 1N5242B 12V 5%	04713	1N5242B	1	530148000
CR8	DIODE SIG 1N4001	04713	1N4001	1	530151000
CR9	DIODE ZENER 1N5242B 12V 5%	04713	1N5242B	1	530148000
CR10-13	DIODE SIG 1N4001	04713	1N4001	4	530151000
CR14	DIODE ZENER 1N5242B 12V 5%	04713	1N5242B	1	530148000
CR15	DIODE SIG 1N4001	04713	1N4001	1	530151000
DS1-5	LED YELLOW DIFF 5082-4684	28480	HLMP-1401	5	536034000
J1	CONN M 03 CKT ST .1CT	06383	MFSS100-3-C-A	1	477364000
J2-3	HEADER 3 PIN STRAIGHT .156 SPA	06383	HPSS156-3-C	2	477343000
J4	CONN M 24 CKT HDR DBL ROW .1CT	06776	NSH-24DB-S2-TG	1	47742224A
J6-15	CONNECTOR "SMB"	19505	209	10	477317000
J16-18	CONN M 05 CKT ST POLZ .1CT	06383	HPSS100-5-C	3	477382000
Q1	TRANS FET 2N7018 PWRMOS P-CHAN	17856	2N7018	1	52816300A
R5	RES MF 301 OHM 1% 1/4W	19701	5043ED301R0F	1	341248000
R7	RES NETWORK 10K .1% 1.5W 16pin	73138	666-3R10KD	1	345010000
R9	RES MF 1.50K 1% 1/4W	19701	5043ED1K500F	1	341317000
R10-11	RES MF 600 OHM 0.25% 1/8W	64537	PME55-T2	2	324215000
R14	RES MF 14.0K 1% 1/4W	19701	5043ED14K00F	1	341414000
R15-16	RES MF 1.65K 1% 1/4W	19701	5043ED1K650F	2	341321000
R17-18	RES MF 6.81K 1% 1/4W	19701	5043ED6K810F	2	341380000
R19	RES MF 47.5K 1% 1/4W	19701	5043ED47K50F	1	341465000
R20	RES MF 100 OHM 1% 1/4W	19701	5043ED100R0F	1	341200000
U1	IC 74HCT273	01295	SN74HCT273N	1	534377000
U2	IC 74HCT138 1 OF 8 DECODER	01295	74HCT138N	1	534375000
U8	IC REF-01CP VOLTAGE REFERENCE	08665	REF-01CP	1	535118000
U9	IC 74HCT273	01295	SN74HCT273N	1	534377000
U10	IC 419 ANALOG SWITCH	17856	DG-419-DJ	1	53452400A
XA4-10	CONNECTOR 36 PIN	31781	306-036-521-102	6	479338000
XA15	CONNECTOR 36 PIN	31781	306-036-521-102	1	479338000
XAR2-3	SOCKET IC 8 PIN	06776	ICN-083-S3-G	2	473041000
XU1	SOCKET IC 20 PIN	06776	ICN-203-S3-G	1	473065000
XU2	SOCKET IC 16 PIN	06776	ICN-163-S3-G	1	473042000
XU8	SOCKET IC 8 PIN	06776	ICN-083-S3-G	1	473041000
XU9	SOCKET IC 16 PIN	06776	ICN-163-S3-G	1	473042000
XU10	SOCKET IC 8 PIN	06776	ICN-083-S3-G	1	473041000

A2		082505000	REV: D*	'8200' RF HOUSING ASSY	A2
A2A1	PWA '8201' RF	04901	08251202A	1	08251202A
A2A2	PWA '8200' OSCILLATOR	04901	08251100B	1	08251100B
A2A3	PWA '8200' CONNECTOR	04901	08252500A	1	08252500A
A2W1	CABLE ASSY WIRE 24GA 8C VAR. L	04901	571198000	1	571198000
A2W2	CABLE ASSY WIRE 24GA 5C 3.50L	04901	571199000	1	571199000
A2W3	CABLE ASSY WIRE 24GA 2C 5.25L	04901	571195000	1	571195000
A2W4	CABLE ASSY WIRE 24GA 2C 9.0L	04901	571195000	1	571198000
A2W5	CABLE ASSY WIRE 24GA 9C 5.0L	04901	571197000	1	571197000
FL1-15	CAP FT 3000pF 100V	32575	856617-1	15	227123000
J1	CONNECTOR SMA	95077	SF-2950-606	1	479440000
J2-5	CONNECTOR "SMB" 50 OHM	19505	2019-7511-000	4	477305000

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR. PART NO.	QTY	BEC PART NO.
A2A1					
08251200B		REV: F*	PWA '8200' RF		
AR1	IC 5534AN OP AMP	18324	NE5534AN	1	535061000
AR2	IC 356P OP AMP	04713	LF356N	1	535040000
C1	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C2	CAP MICA 12pF 5% 300V	57582	KD5120J301	1	205005000
C3	CAP TANT 1.0uF 10% 35V ONLY	56289	198D106X0025KA1	1	283216000
C4	CAP MICA 100pF 5% 300V	20307	DM5-FC101J	1	205006000
C5	CAP TANT 1.0uF 10% 35V ONLY	56289	198D106X0035HA1	1	283216000
C6	CAP MICA 100pF 5% 300V	20307	DM5-FC101J	1	205006000
C7	CAP MICA 12pF 5% 300V	57582	KD5120J301	1	205005000
C8	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C9	CAP MICA 8.0pF 10% 300V	57582	KD5080D301	1	205001000
C10	CAP CER CHIP 680pF 10% 50V	81637	C1210C881K5XAH	1	224377000
C11	CAP CER CHIP 270pF 10% 50V	81637	C1210C271K5XAC	1	224388000
C12	CAP EL 10uF 20% 25V	84217	SM-25-VB-10-M	1	283336000
C13	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C14	CAP EL 10uF 20% 25V	84217	SM-25-VB-10-M	1	283336000
C15	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C16	CAP MICA 680pF 5% 300V	57582	KD15681J301	1	200112000
C17	CAP EL 10uF 20% 25V	84217	SM-25-VB-10-M	1	283336000
C18-20	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	3	224268000
C21	CAP MICA 270pF 5% 50V	57582	KD5271J101	1	205045000
C22	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C23-24	CAP EL 10uF 20% 25V	84217	SM-25-VB-10-M	2	283336000
C25	CAP EL 100uF 20% 25V	84217	SM-25-VB-100-M	1	283334000
C26	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C28-30	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	3	224268000
C31	CAP EL 10uF 20% 25V	84217	SM-25-VB-10-M	1	283336000
C32	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C33	CAP EL 10uF 20% 25V	84217	SM-25-VB-10-M	1	283336000
C34-37	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	4	224268000
C38-39	CAP MICA 270pF 5% 50V	57582	KD5271J101	2	205045000
C40-41	CAP MICA 47pF 5% 300V	20307	DM5-EC470J	2	205018000
C42-43	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C44	CAP MICA 100pF 5% 300V	20307	DM5-FC101J	1	205006000
C45	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C46-47	CAP MICA 390pF 5% 500V	57582	KD15391J501	2	200108000
C48-49	CAP MICA 75pF 5% 300V	57582	KD5750J301	2	205043000
C50	CAP EL 10uF 20% 25V	84217	SM-25-VB-10-M	1	283336000
C51-52	CAP MICA 270pF 5% 50V	57582	KD5271J101	2	205045000
C53-54	CAP MICA 51pF 5% 300V	57582	KD5810J301	2	205020000
C55-56	CAP EL 10uF 20% 25V	84217	SM-25-VB-10-M	2	283336000
C57	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C58	CAP MICA 300pF 1% 50V	57582	KD5301F101	1	205051000
C59	CAP TANT 10uF 20% 25V	56289	198D106X0025KA1	1	283293000
C60	CAP CER 0.01uF 10% 100V	04222	SR201C103KAA	1	224269000
C61	CAP TANT 10uF 20% 25V	56289	198D106X0025KA1	1	283293000

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR. PART NO.	QTY	BEC PART NO.
C62	CAP MICA 1000pF 1% 100V	51406	DM15-102F	1	200113000
C63	CAP EL 100uF 20% 25V	S4217	SM-25-VB-100-M	1	283334000
C64	CAP MICA 300pF 1% 50V	57582	KD5301F101	1	205051000
C65	CAP EL 100uF 20% 25V	S4217	SM-25-VB-100-M	1	283334000
C66	CAP CER 0.1uF 20% 50V	04222	SF215E104MAA	1	224268000
C67	CAP TANT 1.0uF 10% 35V ONLY	56289	196D105X9035HA1	1	283216000
C68	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	1	283336000
C69-71	CAP CER 0.1uF 20% 50V	04222	SF215E104MAA	3	224268000
C73-74	CAP CER 0.1uF 20% 50V	04222	SF215E104MAA	1	224268000
C76	CAP CER CHIP 220pF 10% 50V	61637	CX1210C221K5XAC	1	224220000
C77	CAP CER CHIP 270pF 10% 50V	61637	C1210C271K5XAC	1	224388000
C78	CAP VAR CER 3-10pF 250V	91283	9372	1	281014000
C79	CAP TANT 10uF 20% 25V	56289	196D106X0025KA1	1	283293000
C80	CAP MICA 100pF 5% 300V	20307	DM5-FC101J	1	205006000
C81	CAP MICA 270pF 5% 50V	57582	KD5271J101	1	205045000
CR1	DIODE HSCH1001 (1N6263)	28480	HSCH-1001	1	530174000
CR2A	DIODE 5082-2815 MATCHED QUAD	28480	5082-2815	1	530903000
CR2B	DIODE 5082-2815 MATCHED QUAD	28480	5082-2815	1	530903000
CR2C	DIODE 5082-2815 MATCHED QUAD	28480	5082-2815	1	530903000
CR2D	DIODE 5082-2815 MATCHED QUAD	28480	5082-2815	1	530903000
CR3	DIODE HSCH1001 (1N6263)	28480	HSCH-1001	1	530174000
CR4	DIODE SIG 5082-0180	28480	5082-100	1	530168000
CR5	DIODE HSCH1001 (1N6263)	28480	HSCH-1001	1	530174000
CR6-16	DIODE SIG 1N914	01295	1N914	11	530056000
J1	CONNECTOR 50 OHM	19505	225	1	479387000
J2	HEADER 2 PIN RT ANGLE	06383	HFA5100-2-C	1	477387000
J3	HEADER 10 PIN STRAIGHT	06383	HPSS100-10-C	1	477381000
J4	CONN M 2 CKT ST .1CT	27264	22-10-2021	1	477381000
J5	HEADER 5 PIN STRAIGHT .1 SPACE	06383	HPSS100-5-C	1	477382000
K1	RELAY SPDT FORM "C" 5V DIP	95348	835C-1	1	471034000
L1	INDUCTOR 33uH 5%	59474	4465-2K	1	400310000
L2	INDUCTOR 68uH 10%	24226	10/682	1	400411000
L3	INDUCTOR 39uH 10%	24286	10/392	1	400387000
L4	INDUCTOR 7.5 uH 10%	24226	10M751K	1	400433000
L5	INDUCTOR 15uH 10%	24226	10M152K	1	400373000
L6	INDUCTOR 68uH 10%	24286	10/682	1	400411000
L7	INDUCTOR 39uH 10%	24286	10/392	1	400387000
L8	INDUCTOR 7.5 uH 10%	24226	10M751K	1	400433000
L9	INDUCTOR 15uH 10%	24226	10M152K	1	400373000
L10-11	INDUCTOR 5.6uH 10%	24226	15/561	2	400308000
L12	INDUCTOR 150uH 5%	59474	1315-16J	1	400415000
L13	INDUCTOR 5.6uH 10%	24226	15/561	1	400308000
L14	INDUCTOR 150uH 5%	59474	1315-16J	1	400415000
L15	INDUCTOR VK200/20-4B	02114	VK-200-20/4B	1	400406000
Q1	TRANS NPN MPS-6507	04713	MPS6507	1	528070000
Q2	TRANS FET 2N4416 N-CHAN	04713	2N4416	1	528072000
Q3	TRANS NPN 2N3866	04713	2N3866	1	528116000
Q4	TRANS PNP 2N3906	04713	2N3906	1	528076000
Q5-6	TRANS NPN 2N3904	04713	2N3904	2	528071000

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR. PART NO.	QTY	BEC PART NO.
Q7	TRANS PNP 2N3906	04713	2N3906	1	528078000
Q8	TRANS NPN 2N3904	04713	2N3904	1	528071000
Q9	TRANS PNP 2N3906	04713	2N3906	1	528078000
Q10-11	TRANS NPN 2N3904	04713	2N3904	2	528071000
Q12	TRANS PNP 2N3906	04713	2N3906	1	528078000
Q13	TRANS NPN 2N3886	04713	2N3886	1	528118000
Q14	TRANS PNP 2N4403	04713	2N4403	1	528122000
R1	RES CHIP 300 OHM 5% 1/2W	50316	WA-7PG-301-J-S	1	339995000
R2	RES CHIP 18 OHM 5% 1/2W	50316	WA-7PG-180JS	1	339998000
R3	RES MF 200 OHM 1% 1/4W	19701	5043ED200R0F	1	341229000
R4	RES CHIP 300 OHM 5% 1/2W	50316	WA-7PG-301-J-S	1	339995000
R5	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	1	341400000
R6	RES VAR 50K 10% 0.5W	73138	72PR50K	1	311393000
R7	RES MF 511 OHM 1% 1/4W	19701	5043ED511R0F	1	341268000
R8	RES COMP 6.8K 5% 1/8W	01121	BB8825	1	331102000
R9-10	RES COMP 100 OHM 5% 1/8W	01121	BB1015	2	331058000
R11	RES VAR 50K 10% 0.5W	73138	72PR50K	1	311393000
R12	RES COMP 6.8K 5% 1/8W	01121	BB8825	1	331102000
R13	RES COMP 10K 5% 1/8W	01121	BB1035	1	331106000
R14	RES VAR 10K 10% 0.5W	73138	72PR10K	1	311328000
R15	RES CHIP 100 OHM 5% 1/2W	50316	WA-7PS-101JS	1	339999000
R16	RES COMP 5.1K 5% 1/8W	01121	BB8125	1	331099000
R17	RES COMP 6.8K 5% 1/8W	01121	BB8825	1	331102000
R18	RES CHIP 100 OHM 5% 1/2W	50316	WA-7PS-101JS	1	339999000
R19	RES COMP 6.8K 5% 1/8W	01121	BB8825	1	331102000
R20-21	RES COMP 100 OHM 5% 1/8W	01121	BB1015	2	331058000
R22	RES MF 332 OHM 1% 1/4W	19701	5043ED332R0F	1	341250000
R23	RES COMP 1K 5% 1/8W	01121	BB1025	1	331082000
R24	RES MF 3.92K 1% 1/4W	19701	5043ED3K920F	1	341357000
R25	RES MF 22.1 OHM 1% 1/4W	19701	5043ED22R10F	1	341133000
R26	RES COMP 20K 5% 1/8W	01121	BB2035	1	331113000
R27	RES MF 33.2 OHM 1% 1/4W	19701	5043ED33R20F	1	341150000
R28	RES MF 7.50K 1% 1/4W	19701	5043ED7K500F	1	341384000
R29	RES MF 100 OHM 1% 1/4W	19701	5043ED100R0F	1	341200000
R30	RES MF 511 OHM 1% 1/4W	19701	5043ED511R0F	1	341268000
R31	RES MF 22.1 OHM 1% 1/4W	19701	5043ED22R10F	1	341133000
R32	RES MF 511 OHM 1% 1/4W	19701	5043ED511R0F	1	341268000
R33-35	RES COMP 47 OHM 5% 1/8W	01121	BB4705	3	331060000
R36	RES MF 22.1 OHM 1% 1/4W	19701	5043ED22R10F	1	341133000
R37	RES COMP 100 OHM 5% 1/8W	01121	BB1015	1	331058000
R38	RES COMP 47 OHM 5% 1/8W	01121	BB4705	1	331060000
R39	RES MF 900 OHM 0.1% 1/8W	64537	PME55-T2	1	324235000
R40	RES MF 100 OHM 0.1% 1/8W	64537	PME55-T2	1	324118000
R41	RES MF 100 OHM 1% 1/4W	19701	5043ED100R0F	1	341200000
R42	RES COMP 47 OHM 5% 1/8W	01121	BB4705	1	331060000
R43	RES MF 100 OHM 1% 1/4W	19701	5043ED100R0F	1	341200000
R44	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R45	RES MF 3.92K 1% 1/4W	19701	5043ED3K920F	1	341357000
R46	RES MF 392 OHM 1% 1/4W	19701	5043ED392R0F	1	341257000
R47	RES MF 20.0K 1% 1/4W	19701	5043ED20K00F	1	341429000
R48	RES MF 7.50K 1% 1/4W	19701	5043ED7K500F	1	341384000

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR. PART NO.	QTY	BEC PART NO.
R49	RES MF 511 OHM 1% 1/4W	19701	5043ED511R0F	1	341268000
R50	RES MF 22.1 OHM 1% 1/4W	19701	5043ED22R10F	1	341133000
R51	RES MF 511 OHM 1% 1/4W	19701	5043ED511R0F	1	341268000
R52	RES MF 15.0 OHM 1% 1/4W	19701	5043ED15R00F	1	341117000
R53	RES COMP 47 OHM 5% 1/8W	01121	BB4705	1	331060000
R54	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R55	RES COMP 47 OHM 5% 1/8W	01121	BB4705	1	331050000
R56	RES MF 22.1 OHM 1% 1/4W	19701	5043ED22R10F	1	341133000
R58	RES MF 432 OHM 1% 1/4W	19701	5043ED432R0F	1	341261000
R58	RES COMP 510 OHM 5% 1/8W	01121	BB5115	1	331075000
R63	RES MF 365 OHM 1% 1/4W	19701	5043ED365R0F	1	341254000
R64	RES MF 432 OHM 1% 1/4W	19701	5043ED432R0F	1	341261000
R65	RES MF 825 OHM 1% 1/4W	19701	5043ED825R0F	1	341268000
R66-69	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	4	341300000
R70	RES MF 4.99K 1% 1/4W	19701	5043ED4K990F	1	341367000
R71	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R72	RES MF 39.2K 1% 1/4W	19701	5043ED39K20F	1	341457000
R73	RES MF 100 OHM 1% 1/4W	19701	5043ED100R0F	1	341200000
R74	RES MF 22.1 OHM 1% 1/4W	19701	5043ED22R10F	1	341133000
R75-76	RES MF 2.00K 1% 1/4W	19701	5043ED2K000F	2	341329000
R77	RES MF 68.1 OHM 1% 1/4W	19701	5043ED68R10F	1	341180000
T1	TRANSFORMER BAL T1-1-X85	15542	T1-1	1	410089000
T2	TRANSFORMER RF PULSE	04901	41009000B	1	41009000B
TP1-6	TERMINAL WIRE LOOP TEST POINT	31313	TP-103-02	6	48330600A
U1	IC 74F74PC DUAL D FLIP FLOP	07283	74F74PC	1	534367000
U2	IC 74S00 POS NAND-GATE	01295	SN74S00N	1	534082000
U3	IC 74FO0PC NAND GATE	07263	74FO0PC	1	534366000
U4	IC 13201N ANALOG SWITCH	27014	LF13201N	1	535106000
U5	IC 74LS139 DECODE/MULTIPXR	01295	SN74LS139N	1	534188000
U6	IC 74LS290 DEC CTR	01295	SN74LS290N	1	534328000
U7	IC 13201N ANALOG SWITCH	27014	LF13201N	1	535106000
U8	IC 1355P OP AMP	04713	MC1355P	1	535038000
U9	IC 74LS163 4 BIT COUNTER	01295	SN74LS163AN	1	534279000
XAR1-2	SOCKET IC 8 PIN	06776	ICN-083-S3-G	2	473041000
XK1	SOCKET IC 14 PIN	06776	ICN-143-S3-G	1	473019000
XQ2	SOCKET TRANSISTOR 4 PIN	17117	7004-285-5	1	473051000
XU1-3	SOCKET IC 14 PIN	06776	ICN-143-S3-G	3	473019000
XU4-5	SOCKET IC 16 PIN	06776	ICN-163-S3-G	2	473042000
XU6	SOCKET IC 14 PIN	06776	ICN-143-S3-G	1	473019000
XU7	SOCKET IC 16 PIN	06776	ICN-163-S3-G	1	473042000
XU8	SOCKET IC 14 PIN	06776	ICN-143-S3-G	1	473019000
XU9	SOCKET IC 16 PIN	06776	ICN-163-S3-G	1	473042000
A2A2					
08251100B REV: DC PWA '8200' OSCILLATOR A2A2					
AR1	IC 324N QUAD OP AMP	27014	LM324N	1	535068000
AR2-3	IC 356P OP AMP	04713	LF356N	2	535040000
AR4	IC TL072CP DUAL OP AMP	01295	TL072CP	1	535092000
AR5	IC 356P OP AMP	04713	LF356N	1	535040000
C1	CAP MICA 250pF 5% 50V	57582	KD251J101	1	205037000
C2	CAP EL 100uF 20% 25V	S4217	SM-25-VB-100-M	1	283334000

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR. PART NO.	QTY	BEC PART NO.
C3-4	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	2	283336000
C5	CAP MICA 150pF 5% 100V	57582	KD5151J101	1	205009000
C6	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C7	CAP CER 22pF 2% 500V	55153	C17AH220G4TXL	1	224384000
C8	CAP EL 100uF 20% 25V	S4217	SM-25-VB-100-M	1	283334000
C9	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C10	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	1	283336000
C11	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C12	CAP MPC 1.0uF 10% 50V	14752	652A-1-A-105K	1	234152000
C13	CAP CER 360pF 5% 200V	14752	C17AH361J8TXL	1	224387000
C14	CAP MICA 250pF 5% 50V	57582	KD251J101	1	205037000
C15	CAP MICA 100pF 5% 300V	20307	DM5-FC101J	1	205008000
C16	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C17	CAP CER 10pF 2% 500V	55153	C17AH100G4TXL	1	224383000
C18	CAP CER 0.01uF 10% 100V	04222	SR201C103KAA	1	224269000
C19	CAP EL 100uF 20% 25V	S4217	SM-25-VB-100-M	1	283334000
C20	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C21	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	1	283336000
C22	CAP CER 300pF 5% 200V	55153	C17AH301J8TXL	1	224386000
C23-24	CAP MICA 250pF 5% 50V	57582	KD251J101	2	205037000
C25	CAP CER 0.01uF 10% 100V	04222	SR201C103KAA	1	224269000
C26	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C27	CAP CER 3.3pF +0.25pF 500V	55153	C17AH3R3C4TXL	1	224381000
C28	CAP EL 100uF 20% 25V	S4217	SM-25-VB-100-M	1	283334000
C29-31	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	3	224268000
C32	CAP CER 220pF 2% 200V	55153	C17AH221G6TXL	1	224385000
C33	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C34	CAP MICA 250pF 5% 50V	57582	KD251J101	1	205037000
C35	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	1	283336000
C36	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C37-38	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	2	283336000
C39	CAP MICA 100pF 5% 300V	20307	DM5-FC101J	1	205008000
C40	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C41	CAP CER 0.001uF 10% 100V	04222	SR151C102KAA	1	224270000
C42	CAP CER CHIP 1.2pF 0.1pF 500V	55153	C17AH1R2B4TXL	1	22439100A
C43	CAP EL 100uF 20% 25V	S4217	SM-25-VB-100-M	1	283334000
C44	CAP MPC 1.0uF 10% 50V	14752	652A-1-A-105K	1	234152000
C45	CAP MICA 47pF 5% 300V	20307	DM5-EC470J	1	205018000
C46	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C47	CAP CER 220pF 2% 200V	55153	C17AH221G6TXL	1	224385000
C48	CAP TANT 10uF 10% 35V	56289	198D108X903PE4	1	283353000
C49	CAP MICA 100pF 5% 300V	20307	DM5-FC101J	1	205008000
C50	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	1	283336000
C51	CAP CER 5.0pF +0.25pF 100V	59660	0835-306-P3K0-509C	1	22439000A
CR1	DIODE SIG 1N914	01295	1N914	1	530058000
CR2-3	DIODE HSCH1001 (1N6263)	28480	HSCH-1001	2	530174000
CR4	DIODE PIN 5082-3188	28480	5082-3188	1	530185000
CR9	DIODE PIN 5082-3188	28480	5082-3188	1	530185000
CR10-17	DIODE VARACTOR MV2115 SEL IFF	04713	MV2115	8	530770000
CR18	DIODE SIG 1N914	01295	1N914	1	530058000

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR. PART NO.	QTY	BEC PART NO.
CR18-20	DIODE HSCH1001 (1N6263)	28480	HSCH-1001	2	530174000
CR21	DIODE PIN 5082-3188	28480	5082-3188	1	530165000
CR22-24	DIODE VARACTOR MV2115 SEL ITF	04713	MV2115	3	530770000
CR25	DIODE PIN 5082-3188	28480	5082-3188	1	530165000
CR26-28	DIODE VARACTOR MV2115 SEL ITF	04713	MV2115	3	530770000
CR29	DIODE SIG 1N914	01295	1N914	1	530058000
CR30-31	DIODE HSCH1001 (1N6263)	28480	HSCH-1001	2	530174000
CR32	DIODE PIN 5082-3188	28480	5082-3188	1	530165000
CR33-34	DIODE VARACTOR MV2115 SEL ITF	04713	MV2115	2	530770000
CR35	DIODE PIN 5082-3188	28480	5082-3188	1	530165000
CR36-37	DIODE SIG 1N914	01295	1N914	2	530058000
CR38-39	DIODE VARACTOR MV2115 SEL ITF	04713	MV2115	2	530770000
CR40	DIODE SIG 1N914	01295	1N914	1	530058000
CR41-42	DIODE HSCH1001 (1N6263)	28480	HSCH-1001	2	530174000
CR43	DIODE PIN 5082-3188	28480	5082-3188	1	530165000
CR44-45	DIODE VARACTOR MV2115 SEL ITF	04713	MV2115	2	530770000
CR46	DIODE PIN 5082-3188	28480	5082-3188	1	530165000
CR47-48	DIODE VARACTOR MV2115 SEL ITF	04713	MV2115	2	530770000
DS1	PHOTO MOD CLM6500	03911	CLM6500	1	325016000
DS2-5	LED RED DIFF 5082-4684	28480	HLMP-1301	4	536024000
J1	HEADER 10 PIN STRAIGHT	06383	HPSS100-10-C	1	477381000
J2	HEADER 5 PIN STRAIGHT .1 SPACE	06383	HPSS100-5-C	1	477382000
L1-3	INDUCTOR 5.6uH 10%	24226	15/561	3	400308000
L4	INDUCTOR 0.82uH 10%	59474	4425-5K	1	400293000
L5	INDUCTOR 330 uH 10%	24226	10/333	1	400442000
L6	INDUCTOR 39uH 10%	24266	10/392	1	400387000
L7	INDUCTOR 33uH 5%	59474	4485-2K	1	400310000
L8	INDUCTOR 39uH 10%	24266	10/392	1	400387000
L9	INDUCTOR 0.82uH 10%	59474	4425-5K	1	400293000
L11	INDUCTOR 39uH 10%	24266	10/392	1	400387000
L12	INDUCTOR 33uH 5%	59474	4485-2K	1	400310000
L13	INDUCTOR 39uH 10%	24266	10/392	1	400387000
L14	INDUCTOR 0.82uH 10%	59474	4425-5K	1	400293000
L16	INDUCTOR 39uH 10%	24266	10/392	1	400387000
L17	INDUCTOR 33uH 5%	59474	4485-2K	1	400310000
L18	INDUCTOR 39uH 10%	24266	10/392	1	400387000
L19	INDUCTOR 4.7uH 10%	24226	10/471	1	400384000
L20	INDUCTOR 0.82uH 10%	59474	4425-5K	1	400293000
L22-23	INDUCTOR 39uH 10%	24266	10/392	2	400387000
L24	INDUCTOR 33uH 5%	59474	4485-2K	1	400310000
L25	INDUCTOR 39uH 10%	24266	10/392	1	400387000
L26	INDUCTOR 5.6uH 10%	24226	15/561	1	400308000
P1	CONNECTOR "SMA" 50 OHM	98291	52-051-0000	1	477304000
Q1	TRANS FET 2N4416 N-CHAN	04713	2N4416	1	528072000
Q2	TRANS NPN MPS-6507	04713	MPS6507	1	528070000
Q3-4	TRANS FET 2N4416 N-CHAN	04713	2N4416	2	528072000
Q5	TRANS NPN MPS-6507	04713	MPS6507	1	528070000
Q6	TRANS FET 2N4221A N-CHAN	27014	2N4221A	1	528063000
Q7	TRANS PNP 2N4403	04713	2N4403	1	528122000
Q8	TRANS NPN 2N4401	04713	2N4401	1	528121000
Q9	TRANS PNP 2N4403	04713	2N4403	1	528122000

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR. PART NO.	QTY	BEC PART NO.
R1	RES MF 51.1K 1% 1/4W	19701	5043ED51K10F	1	341468000
R2	RES MF 243 OHM 1% 1/4W	19701	5043ED243R0F	1	341237000
R3	RES MF 1.50K 1% 1/4W	19701	5043ED1K500F	1	341317000
R4	RES MF 1.21K 1% 1/4W	19701	5043ED1K210F	1	341308000
R5	RES MF 3.32K 1% 1/4W	19701	5043ED3K320F	1	341350000
R6	RES MF 1.82K 1% 1/4W	19701	5043ED1K820F	1	341325000
R7	RES MF 150 OHM 1% 1/4W	19701	5043ED150R0F	1	341217000
R8	RES MF 475 OHM 1% 1/4W	19701	5043ED475R0F	1	341265000
R9	RES MF 909 OHM 1% 1/4W	09701	5043ED909R0F	1	341292000
R10	RES MF 100 OHM 1% 1/4W	19701	5043ED100R0F	1	341200000
R11	RES MF 51.1K 1% 1/4W	19701	5043ED51K10F	1	341468000
R12	RES MF 243 OHM 1% 1/4W	19701	5043ED243R0F	1	341237000
R13	RES MF 1.21K 1% 1/4W	19701	5043ED1K210F	1	341308000
R14	RES MF 150 OHM 1% 1/4W	19701	5043ED150R0F	1	341217000
R15	RES MF 24.9K 1% 1/4W	19701	RN55D-2492-F	1	341438000
R16	RES MF 4.75K 1% 1/4W	19701	5043ED4K750F	1	341365000
R17	RES MF 51.1K 1% 1/4W	19701	5043ED51K10F	1	341468000
R18	RES MF 8.25K 1% 1/4W	19701	5043ED8K250F	1	341369000
R19	RES VAR 5K 10% 0.5W	73138	72PR5K	1	311308000
R20	RES MF 243 OHM 1% 1/4W	19701	5043ED243R0F	1	341237000
R21	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	1	341400000
R22-23	RES MF 5.11K 1% 1/4W	19701	5043ED5K110F	2	341366000
R24	RES MF 2.00K 1% 1/4W	19701	5043ED2K000F	1	341329000
R25	RES MF 1.21K 1% 1/4W	19701	5043ED1K210F	1	341308000
R26	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R27	RES MF 100 OHM 1% 1/4W	19701	5043ED100R0F	1	341200000
R28	RES MF 150 OHM 1% 1/4W	19701	5043ED150R0F	1	341217000
R29	RES MF 4.99K 1% 1/4W	19701	5043ED4K990F	1	341367000
R30	RES MF 5.11K 1% 1/4W	19701	5043ED5K110F	1	341368000
R31	RES MF 392K 1% 1/4W	19701	5043ED392K0F	1	341557000
R32	RES MF 475 OHM 1% 1/4W	19701	5043ED475R0F	1	341265000
R33	RES MF 1.82K 1% 1/4W	19701	5043ED1K820F	1	341325000
R34	RES MF 3.32K 1% 1/4W	19701	5043ED3K320F	1	341350000
R35	RES MF 15.0K 1% 1/4W	19701	5043ED15K00F	1	341417000
R36	RES MF 51.1K 1% 1/4W	19701	5043ED51K10F	1	341468000
R37	RES MF 4.99K 1% 1/4W	19701	5043ED4K990F	1	341367000
R38	RES MF 1.50K 1% 1/4W	19701	5043ED1K500F	1	341317000
R39	RES MF 4.99K 1% 1/4W	19701	5043ED4K990F	1	341367000
R40	RES MF 243 OHM 1% 1/4W	19701	5043ED243R0F	1	341237000
R41	RES MF 1.10K 1% 1/4W	19701	5043ED1K100F	1	341304000
R42	RES MF 14.0K 1% 1/4W	19701	5043ED14K00F	1	341414000
R43	RES NETWORK 10K 0.5% 1/2W	73138	604-3-R10K-D	1	345041000
R44	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R45	RES MF 1.21K 1% 1/4W	19701	5043ED1K210F	1	341308000
R46	RES MF 51.1K 1% 1/4W	19701	5043ED51K10F	1	341468000
R47	RES MF 150 OHM 1% 1/4W	19701	5043ED150R0F	1	341217000
R48	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	1	341400000
R51	RES MF 133 OHM 1% 1/4W	19701	5043ED133R0F	1	341212000
R52	RES MF 1.00M 1% 1/4W	14674	5043ED1M000F	1	341600000
R53	RES MF 100 OHM 1% 1/4W	19701	5043ED100R0F	1	341200000
R54	RES NETWORK 470 OHM 2% 1.1W	71450	750-81-R470	1	345018000

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR. PART NO.	QTY	BEC PART NO.
R55	RES MF 1.82K 1% 1/4W	19701	5043ED1K620F	1	341320000
T1	TRANSFORMER RF T4-1-X65	15542	T4-1	1	410087000
T2-4	OSC TRANSFORMER	04901	400431000	3	400431000
T5	OSC TRANSFORMER	04901	400430000	1	400430000
U1	IC 74LS138 DECDR/MPX	01295	SN74LS138N	1	534246000
U2	IC 74LS122 MONOSTABLE MULTVBT	01295	SN74LS122N	1	534280000
U3	IC 4052B MULTIPLEXER	02735	CD4052BE	1	534140000
XAR1	SOCKET IC 14 PIN	06776	ICN-143-S3-G	1	473019000
XAR2-5	SOCKET IC 8 PIN	06776	ICN-083-S3-G	4	473041000
XDS1/1	SOCKET STRIP 2 PIN	04901	473074000	1	473074000
XDS1/2	SOCKET STRIP 2 PIN	04901	473074000	1	473074000
XQ1	SOCKET TRANSISTOR 4 PIN	17117	7004-285-5	1	473051000
XQ3-4	SOCKET TRANSISTOR 4 PIN	17117	7004-285-5	2	473051000
XQ6	SOCKET TRANSISTOR 4 PIN	17117	7004-285-5	1	473051000
XU1	SOCKET IC 16 PIN	06776	ICN-163-S3-G	1	473042000
XU2	SOCKET IC 14 PIN	06776	ICN-143-S3-G	1	473019000
XU3	SOCKET IC 16 PIN	06776	ICN-163-S3-G	1	473042000
A2A3					
08252500A		REV: AB	PWA '8200' CONNECTOR		
J1	SOCKET IC 24 PIN	06776	ICN-246-S4-G	1	473043000
A4					
08252200A		REV: F*	PWA '8200' FM		
AR1	IC 301A OP AMP	27014	LM301AN	1	535012000
AR2	IC 358P OP AMP	27014	LF358N	1	535040000
AR3	IC 5534AN OP AMP	18324	NE5534AN	1	535081000
C1	CAP MICA 250pF 5% 50V	57582	KD251J101	1	205037000
C2-3	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	2	283336000
C4	CAP MICA 8.0pF 10% 300V	57582	KD5080D301	1	205001000
C5	CAP MICA 91pF 5% 300V	14655	CD6FC910J	1	205021000
C6	CAP MICA 8.0pF 10% 300V	57582	KD5080D301	1	205001000
C7	CAP MICA 20pF 5% 300V	14655	CD5CC200J	1	205017000
C8	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C9	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	1	283336000
C10	CAP MICA 100pF 1% 500V	14655	CD15FD101F	1	200045000
C11	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C12	CAP EL 100uF 20% 25V	S4217	SM-25-VB-101M	1	283334000
C13	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C14-15	CAP CER 0.01uF 10% 100V	04222	SR201C103KAA	2	224268000
C16	CAP MICA 33pF 5% 300V	20307	DM5-EC330J	1	205010000
C17	CAP EL 100uF 20% 25V	S4217	SM-25-VB-101M	1	283334000
C18	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	1	283336000
C19	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C20-21	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	2	283336000
C22-23	CAP CER 0.01uF 10% 100V	04222	SR201C103KAA	2	224268000
C24	CAP EL 100uF 20% 25V	S4217	SM-25-VB-101M	1	283334000
C25	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR. PART NO.	QTY	BEC PART NO.
C26	CAP TANT 10uF 20% 25V	56289	196D106X0025KA1	1	283293000
C27	CAP MICA 680pF 1% 300V	14655	CD15FC681F03	1	200015000
C28	CAP MICA 36pF 5% 300V	14655	CD5EC360J	1	205003000
C29	CAP MICA 680pF 1% 300V	14655	CD15FC681F03	1	200015000
C30-31	CAP CER 0.01uF 10% 100V	04222	SR201C103KAA	2	224269000
C32	CAP MICA 680pF 5% 300V	57582	KD15681J301	1	200112000
C33	CAP MICA 500pF 1% 500V	14655	CD15FD501F	1	200123000
C34	CAP TANT 100uF 20% 20V	56289	196D107X0020TE4	1	283313000
C35	CAP EL 100uF 20% 25V	S4217	SM-25-VB-101M	1	283334000
C36	CAP MICA 1000pF 1% 100V	51406	DM15-102F	1	200113000
C37-38	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	2	224269000
C39	CAP MICA 330pF 5% 50V	14655	CD5FY331J	1	205029000
C40	CAP TANT 10uF 20% 25V	56289	196D106X0025KA1	1	283293000
C41	CAP MICA 330pF 5% 50V	14655	CD5FY331J	1	205029000
C42	CAP MICA 1000pF 1% 100V	51406	DM15-102F	1	200113000
C43	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224269000
C44	CAP MICA 200pF 1% 100V	14655	CD5FA201F	1	205041000
C45	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	1	283336000
C46-47	CAP TANT 100uF 20% 20V	56289	196D107X0020TE4	2	283313000
C48	CAP MICA 27pF 5% 300V	14655	CD5EC270J	1	205009000
C49	CAP CER 0.01uF 10% 100V	04222	SR201C103KAA	1	224269000
C50	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224269000
C51	CAP MICA 130pF 5% 100V	14655	CD5FA131J	1	205011000
C52	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224269000
C53-54	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	2	283336000
C55	CAP MICA 20pF 5% 300V	14655	CD5CC200J	1	205017000
CR1-3	DIODE SIG 1N914	01295	1N914	3	530058000
L1-2	INDUCTOR 5.6uH 10%	24226	15/561	2	400308000
L3	INDUCTOR 33uH 5%	59474	4465-2K	1	400310000
L4	INDUCTOR 15uH 10%	59474	4445-4K	1	400302000
L5	INDUCTOR 750uH 5%	24226	19/753J	1	400443000
L6	COIL ASSY 902uH (ALT.-000)8200	04901	40043901A	1	40043901A
L7	INDUCTOR 5.6uH 10%	24226	15/561	1	400308000
L8	INDUCTOR 120uH 10%	24226	10/123	1	400413000
L9	COIL ASSY 1450uH (ALT-000)8200	04901	40044001A	1	40044001A
L10	COIL ASSY 902uH (ALT.-000)8200	04901	40043901A	1	40043901A
L11	INDUCTOR 5.6uH 10%	24226	15/561	1	400308000
Q1	TRANS FET SD215EE N-CHAN	17856	SD215DE	1	528120000
Q2	TRANS PNP 2N3906	04713	2N3906	1	528076000
Q3	IC 3054 ARRAY	02735	CA3054	1	535111000
Q4-5	TRANS NPN 2N3904	04713	2N3904	2	528071000
Q6	TRANS PNP 2N3906	04713	2N3906	1	528076000
Q7	TRANS NPN 2N3904	04713	2N3904	1	528071000
Q8	IC 3054 ARRAY	02735	CA3054	1	535111000
Q9	TRANS PNP 2N3906	04713	2N3906	1	528076000
Q10	TRANS FET SD215EE N-CHAN	17856	SD215DE	1	528120000
Q11-13	TRANS PNP 2N3906	04713	2N3906	3	528076000
Q14-16	TRANS PNP 2N4403	04713	2N4403	3	528122000
R1	RES MF 475 OHM 1% 1/4W	19701	5043ED475R0F	1	341265000
R2	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	1	341400000

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR PART NO.	QTY	BEC PART NO.
R3	RES MF 511 OHM 1% 1/4W	19701	5043ED511R0F	1	341268000
R4	RES MF 2.61K 1% 1/4W	19701	5043ED2K619F	1	341340000
R5-7	RES MF 511 OHM 1% 1/4W	19701	5043ED511R0F	3	341268000
R8-9	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	2	341400000
R10	RES MF 2.21K 1% 1/4W	19701	5043ED2K210F	1	341333000
R11	RES MF 68.1 OHM 1% 1/4W	19701	5043ED68R10F	1	341180000
R12	RES MF 511 OHM 1% 1/4W	19701	5043ED511R0F	1	341268000
R13	RES MF 750 OHM 1% 1/4W	19701	5043ED750R0F	1	341284000
R14	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	1	341400000
R15	RES MF 4.99K 1% 1/4W	19701	5043ED4K990F	1	341367000
R16	RES MF 681 OHM 1% 1/4W	19701	5043ED681R0F	1	341280000
R17	RES MF 511 OHM 1% 1/4W	19701	5043ED511R0F	1	341268000
R18-19	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	2	341400000
R20	RES MF 2.00K 1% 1/4W	19701	5043ED2K000F	1	341329000
R21	RES MF 511 OHM 1% 1/4W	19701	5043ED511R0F	1	341268000
R22	RES MF 200 OHM 1% 1/4W	19701	5043ED200R0F	1	341229000
R23-24	RES MF 511 OHM 1% 1/4W	19701	5043ED511R0F	2	341268000
R25-26	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	2	341400000
R27	RES MF 2.21K 1% 1/4W	19701	5043ED2K210F	1	341333000
R28	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	1	341400000
R29	RES MF 681 OHM 1% 1/4W	19701	5043ED681R0F	1	341280000
R30	RES MF 4.99K 1% 1/4W	19701	5043ED4K990F	1	341367000
R31	RES MF 68.1 OHM 1% 1/4W	19701	5043ED68R10F	1	341180000
R32-34	RES MF 511 OHM 1% 1/4W	19701	5043ED511R0F	3	341268000
R35-36	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	2	341400000
R37-39	RES MF 511 OHM 1% 1/4W	19701	5043ED511R0F	3	341268000
R40-41	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	2	341400000
R42	RES MF 2.21K 1% 1/4W	19701	5043ED2K210F	1	341333000
R43	RES MF 511 OHM 1% 1/4W	19701	5043ED511R0F	1	341268000
R44	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	1	341400000
R45	RES MF 3.92K 1% 1/4W	19701	5043ED3K920F	1	341357000
R46	RES MF 68.1 OHM 1% 1/4W	19701	5043ED68R10F	1	341180000
R47-48	RES MF 511 OHM 1% 1/4W	19701	5043ED511R0F	2	341268000
R49-50	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	2	341400000
R51	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R52	RES MF 182 OHM 1% 1/4W	19701	RN55D-1820-F	1	341225000
R53-54	RES MF 332 OHM 1% 1/4W	19701	5043ED332R0F	2	341250000
R55-56	RES MF 511 OHM 1% 1/4W	19701	5043ED511R0F	2	341268000
R57-58	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	2	341400000
R59	RES MF 2.21K 1% 1/4W	19701	5043ED2K210F	1	341333000
R60	RES MF 511 OHM 1% 1/4W	19701	5043ED511R0F	1	341268000
R61	RES MF 499 OHM 1% 1/4W	19701	5043ED499R0F	1	341267000
R62	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R63	RES MF 3.74K 1% 1/4W	19701	5043ED3K740F	1	341355000
R64	RES MF 511 OHM 1% 1/4W	19701	5043ED511R0F	1	341268000
R65-66	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	2	341400000
R67	RES MF 68.1 OHM 1% 1/4W	19701	5043ED68R10F	1	341180000
R68	RES MF 332 OHM 1% 1/4W	19701	5043ED332R0F	1	341250000
R69	RES MF 221 OHM 1% 1/4W	19701	5043ED221R0F	1	341233000

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR PART NO.	QTY	BEC PART NO.
R70	RES MF 88.1 OHM 1% 1/4W	19701	5043ED68R10F	1	341180000
R71	RES MF 499 OHM 1% 1/4W	19701	5043ED499R0F	1	341267000
R72	RES MF 9.09K 1% 1/4W	19701	5043ED9K090F	1	341382000
R73	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R74	RES MF 511 OHM 1% 1/4W	19701	5043ED511R0F	1	341268000
R75	RES MF 88.1 OHM 1% 1/4W	19701	5043ED68R10F	1	341180000
R76	RES MF 5.62K 1% 1/4W	19701	5043ED5K620F	1	341372000
R77	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R78	RES MF 432 OHM 1% 1/4W	19701	5043ED432R0F	1	341261000
R79	RES MF 88.1 OHM 1% 1/4W	19701	5043ED68R10F	1	341180000
R80-83	RES MF 3.32K 1% 1/4W	19701	5043ED3K320F	4	341350000
R84-85	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	2	341300000
R86	RES MF 1.82K 1% 1/4W	19701	5043ED1K820F	1	341325000
R87-88	RES MF 3.32K 1% 1/4W	19701	5043ED3K320F	2	341350000
R89	RES MF 681 OHM 1% 1/4W	19701	5043ED681R0F	1	341280000
U1	IC 74F74PC DUAL D FLIP FLOP	07263	74F74PC	1	534367000
XAR1-3	SOCKET IC 8 PIN	05776	ICN-083-S3-G	3	473041000
XQ1	SOCKET TRANSISTOR 4 PIN	17117	7004-265-5	1	473051000
XQ2	SOCKET TRANSISTOR 3 CIR TO-18	EMC	7003-265-5	1	47307800A
XQ3	SOCKET IC 14 PIN	05776	ICN-143-S3-G	1	473019000
XQ4-7	SOCKET TRANSISTOR 3 CIR TO-18	EMC	7003-265-5	4	47307800A
XQ8	SOCKET IC 14 PIN	05776	ICN-143-S3-G	1	473019000
XQ9	SOCKET TRANSISTOR 3 CIR TO-18	EMC	7003-265-5	1	47307800A
XQ10	SOCKET TRANSISTOR 4 PIN	17117	7004-265-5	1	473051000
XQ11-13	SOCKET TRANSISTOR 3 CIR TO-18	EMC	7003-265-5	3	47307800A
XU1	SOCKET IC 14 PIN	05776	ICN-143-S3-G	1	473019000
A5					
08251300B REV: CB PWA '8200' AM					
AR1	IC TL072CP DUAL OP AMP	01295	TL072CP	1	535092000
AR2	IC 318N OP AMP	27014	LM318N	1	535031000
AR3	IC 356P OP AMP	27014	LF356N	1	535040000
C1	CAP MICA 100pF 1% 300V	14655	CD5FC101F	1	205039000
C2	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	1	283336000
C3	CAP EL 100uF 20% 25V	S4217	SM-25-VB-101M	1	283334000
C4	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	1	283336000
C5	CAP EL 100uF 20% 25V	S4217	SM-25-VB-101M	1	283334000
C6	CAP CER 0.1uF 20% 50V	04222	SF215E104MAA	1	224268000
C7	CAP MICA 180pF 1% 100V	14655	CD5FA181F	1	205040000
C8	CAP TANT 1.0uF 10% 35V ONLY	56289	196D105X9035HA1	1	283216000
C9	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	1	283336000
C10	CAP MICA 100pF 1% 300V	14655	CD5FC101F	1	205039000
C11-12	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	2	283336000
C13	CAP CER 0.1uF 20% 50V	04222	SF215E104MAA	1	224268000
C14	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	1	283336000
C15	CAP TANT 1.0uF 10% 35V ONLY	56289	196D105X9035HA1	1	283216000
C16-18	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	3	283336000
C19	CAP MICA 470pF 5% 300V	14655	CD15-471J03	1	200028000

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR PART NO.	QTY	BEC PART NO.
C20-21	CAP TANT 1.0uF 10% 35V ONLY	56289	196D105X9035HA1	2	283216000
C22	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C23	CAP CER 0.01uF 10% 100V	04222	SR201C103KAA	1	224268000
C24	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	1	283336000
C25	CAP MPC 0.1uF 2% 50V	14752	652A-1-A-104G	1	234139000
C26	CAP CER 1.0uF 20% 50V	04222	SR306E105MAA	1	224264000
C27	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C28	CAP MPC 0.1uF 2% 50V	14752	652A-1-A-104G	1	234139000
C29	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C30	CAP TANT 1.0uF 10% 35V ONLY	56289	196D105X9035HA1	1	283216000
C31	CAP COMP 0.27pF 10% 500V	95721	TYPE MC	1	218006000
C32	CAP TANT 1.0uF 10% 35V ONLY	56289	196D105X9035HA1	1	283216000
C33	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	1	283336000
C34	CAP TANT 1.0uF 10% 35V ONLY	56289	196D105X9035HA1	1	283216000
C35	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	1	283336000
C36	CAP TANT 1.0uF 10% 35V ONLY	56289	196D105X9035HA1	1	283216000
C37	CAP MICA 1000pF 1% 100V	51406	DM15-102F	1	200113000
C38-39	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	2	283336000
C40	CAP TANT 1.0uF 10% 35V ONLY	56289	196D105X9035HA1	1	283216000
C41	CAP TANT 10uF 20% 25V	56289	196D106X0025KA1	1	283293000
C42	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C43	CAP CER 1.0uF 20% 50V	04222	SR306E105MAA	1	224264000
C44	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C45	CAP MICA 20pF 5% 300V	14655	CD5CC200J	1	205017000
C47	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C48	CAP MICA 20pF 5% 300V	14655	CD5CC200J	1	205017000
C50	CAP MICA 300pF 1% 50V	57582	KD5301F101	1	205051000
C51	CAP MICA 1000pF 1% 100V	51406	DM15-102F	1	200113000
C52	CAP MICA 300pF 5% 50V	14655	CD5FY301J	1	205028000
C53	CAP MICA 1000pF 1% 100V	51406	DM15-102F	1	200113000
C54	CAP MICA 300pF 5% 50V	14655	CD5FY301J	1	205028000
C56	CAP MICA 300pF 1% 50V	57582	KD5301F101	1	205051000
C57	CAP MICA 15pF 5% 300V	14655	CD5CC150J	1	205035000
C58	CAP TANT 1.0uF 10% 35V ONLY	56289	196D105X9035HA1	1	283216000
C59-60	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	2	224268000
C61	CAP EL 100uF 20% 25V	S4217	SM-25-VB-101M	1	283334000
C62	CAP MICA 75pF 5% 300V	57582	KD5750J301	1	205043000
CR1-5	DIODE SIG 1N914	01295	1N914	5	530058000
CR6a-6b	DIODE 5082-2815 MATCHED PAIR	28480	5082-2815 MATCH PAIR	1	53091100A
DS1-2	PHOTO MOD CLM8500	03911	CLM8500	2	325016000
L1-3	INDUCTOR 5.6uH 10%	24226	15/561	3	400308000
L4	INDUCTOR 33uH 5%	59474	4465-2K	1	400310000
L5-6	INDUCTOR 47uH 5%	24226	15/472J	2	400320000
L7-8	INDUCTOR 5.6uH 10%	24226	15/561	2	400308000
L9	INDUCTOR 1800uH 5%	59474	1312-25J	1	400434000
L10	COIL ASSY 902uH (ALT.-000)8200	04901	40043901A	1	40043901A
L11	COIL ASSY 1450uH (ALT.-000)8200	04901	40044001A	1	40044001A
L12	COIL ASSY 902uH (ALT.-000)8200	04901	40043901A	1	40043901A
Q1	TRANS PNP 2N3906	04713	2N3906	1	528076000
Q2	TRANS NPN 2N3053	04713	2N3053	1	528123000

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR PART NO.	QTY	BEC PART NO.
Q3-4	TRANS PNP 2N3906	04713	2N3906	2	528076000
Q5-6	TRANS NPN 2N3904	04713	2N3904	2	528071000
Q7	TRANS NPN 2N4401	04713	2N4401	1	528121000
Q8-10	TRANS FET 2N4416 N-CHAN	04713	2N4416	3	528072000
Q11	TRANS NPN 2N4401	04713	2N4401	1	528121000
Q12	TRANS NPN 2N3904	04713	2N3904	1	528071000
Q13-14	TRANS PNP 2N3906	04713	2N3906	2	528076000
Q15-17	TRANS NPN 2N3904	04713	2N3904	3	528071000
Q18-20	TRANS PNP 2N3906	04713	2N3906	3	528076000
Q21	TRANS NPN 2N3904	04713	2N3904	1	528071000
Q22	TRANS NPD 5564	27014	NPD5564	1	528148000
R1	RES MF 511 OHM 1% 1/4W	19701	5043ED511R0F	1	341268000
R2	RES MF 2.49K 1% 1/4W	19701	5043ED2K490F	1	341338000
R3	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	1	341400000
R4-5	RES MF 15.0K 1% 1/4W	19701	5043ED15K00F	2	341417000
R6	RES MF 562 OHM 1% 1/4W	19701	5043ED562R0F	1	341272000
R7	RES MF 511 OHM 1% 1/4W	19701	5043ED511R0F	1	341268000
R8	RES MF 3.32K 1% 1/4W	19701	5043ED3K320F	1	341350000
R9	RES MF 1.50K 1% 1/4W	19701	5043ED1K500F	1	341317000
R10	RES MF 5.36K 1% 1/4W	19701	5043ED5K360F	1	341370000
R11	RES MF 7.50K 1% 1/4W	19701	5043ED7K500F	1	341384000
R12	RES MF 5.11K 1% 1/4W	19701	5043ED5K110F	1	341368000
R13	RES MF 47.5 OHM 1% 1/4W	19701	5043ED47R50F	1	341165000
R14	RES MF 332 OHM 1% 1/4W	19701	5043ED332R0F	1	341250000
R15	RES MF 47.5 OHM 1% 1/4W	19701	5043ED47R50F	1	341165000
R16	RES MF 3.32K 1% 1/4W	19701	5043ED3K320F	1	341350000
R17	RES MF 511 OHM 1% 1/4W	19701	5043ED511R0F	1	341268000
R18	RES MF 75.0 OHM 1% 1/4W	19701	5043ED75R00F	1	341184000
R19	RES MF 1.50K 1% 1/4W	19701	5043ED1K500F	1	341317000
R20-21	RES MF 47.5 OHM 1% 1/4W	19701	5043ED47R50F	2	341165000
R22	RES MF 511 OHM 1% 1/4W	19701	5043ED511R0F	1	341268000
R23	RES MF 1.50K 1% 1/4W	19701	5043ED1K500F	1	341317000
R24	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	1	341400000
R25	RES MF 9.31K 1% 1/4W	19701	5043ED9K310F	1	341393000
R26	RES MF 14.0K 1% 1/4W	19701	5043ED14K00F	1	341414000
R27	RES MF 49.9K 1% 1/4W	19701	5043ED49K90F	1	341467000
R28	RES MF 75.0K 1% 1/4W	19701	5043ED75K00F	1	341484000
R29	RES MF 100K 1% 1/4W	19701	5043ED100K0F	1	341500000
R30	RES MF 499K 1% 1/4W	19701	5043ED499K0F	1	341567000
R31	RES MF 267K 1% 1/4W	19701	5043ED267K0F	1	341541000
R32	RES MF 9.31K 1% 1/4W	19701	5043ED9K310F	1	341393000
R33	RES MF 75.0K 1% 1/4W	19701	5043ED75K00F	1	341484000
R34	RES MF 267K 1% 1/4W	19701	5043ED267K0F	1	341541000
R35	RES MF 499K 1% 1/4W	19701	5043ED499K0F	1	341567000
R36	RES MF 14.0K 1% 1/4W	19701	5043ED14K00F	1	341414000
R37	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R38	RES MF 3.01K 1% 1/4W	19701	5043ED3K010F	1	341348000
R39	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	1	341400000
R40-41	RES MF 511 OHM 1% 1/4W	19701	5043ED511R0F	2	341268000

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR PART NO.	QTY	BEC PART NO.
R42	RES MF 9.09K 1% 1/4W	19701	5043ED9K090F	1	341392000
R43	RES MF 2.00K 1% 1/4W	19701	5043ED2K000F	1	341329000
R44	RES MF 3.32K 1% 1/4W	19701	5043ED3K320F	1	341350000
R45	RES MF 1.50K 1% 1/4W	19701	5043ED1K500F	1	341317000
R46	RES MF 11.0K 1% 1/4W	19701	5043ED11K00F	1	341404000
R47-48	RES MF 47.5 OHM 1% 1/4W	19701	5043ED47R50F	2	341165000
R49	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	1	341400000
R50	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R51	RES MF 3.01K 1% 1/4W	19701	5043ED3K010F	1	341346000
R52	RES MF 47.5 OHM 1% 1/4W	19701	5043ED47R50F	1	341165000
R53-54	RES MF 511 OHM 1% 1/4W	19701	5043ED511R0F	2	341268000
R55	RES MF 2.00K 1% 1/4W	19701	5043ED2K000F	1	341329000
R56	RES MF 22.1 OHM 1% 1/4W	19701	5043ED22R10F	1	341133000
R57	RES MF 8.25K 1% 1/4W	19701	5043ED8K250F	1	341388000
R58	RES MF 511 OHM 1% 1/4W	19701	5043ED511R0F	1	341268000
R59	RES MF 1.62K 1% 1/4W	19701	5043ED1K620F	1	341320000
R60	RES MF 3.32K 1% 1/4W	19701	5043ED3K320F	1	341350000
R61	RES MF 4.75K 1% 1/4W	19701	5043ED4K750F	1	341365000
R62	RES MF 3.32K 1% 1/4W	19701	5043ED3K320F	1	341350000
R63	RES MF 8.25K 1% 1/4W	19701	5043ED8K250F	1	341388000
R64-65	RES MF 47.5 OHM 1% 1/4W	19701	5043ED47R50F	2	341165000
R66-67	RES MF 221 OHM 1% 1/4W	19701	5043ED221R0F	2	341233000
R68	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R69	RES MF 47.5 OHM 1% 1/4W	19701	5043ED47R50F	1	341165000
R70	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	1	341400000
R71	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R72	RES MF 47.5 OHM 1% 1/4W	19701	5043ED47R50F	1	341165000
R73	RES MF 9.09K 1% 1/4W	19701	5043ED9K090F	1	341392000
R74	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	1	341400000
R75	RES MF 9.09K 1% 1/4W	19701	5043ED9K090F	1	341392000
R76	RES MF 47.5 OHM 1% 1/4W	19701	5043ED47R50F	1	341165000
R77-79	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	3	341400000
R80	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R81	RES MF 12.7K 1% 1/4W	19701	5043ED12K70F	1	341410000
R82	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R83-84	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	2	341400000
R85	RES VAR 100K 10% 0.5W	73138	72XWR100K	1	311377000
R86	RES MF 301K 1% 1/4W	19701	5043ED301K0F	1	341546000
R87	RES COMP 4.7M 5% 1/4W	01121	CB4755	1	343665000
R88	RES MF 511 OHM 1% 1/4W	19701	5043ED511R0F	1	341268000
TP1-5	TERMINAL WIRE LOOP TEST POINT	31313	TP-103-02	5	48330600A
U1	IC 74HCT273	01295	SN74HCT273N	1	534377000
U2	D/A CONVERTER DAC-08EP	06665	DAC-08EP	1	421037000
XDS1/1	SOCKET STRIP 2 PIN	04901	473074000	1	473074000
XDS1/2	SOCKET STRIP 2 PIN	04901	473074000	1	473074000
XDS2/1	SOCKET STRIP 2 PIN	04901	473074000	1	473074000
XDS2/2	SOCKET STRIP 2 PIN	04901	473074000	1	473074000
XU1	SOCKET IC 20 PIN	06776	ICN-203-S3-G	1	473065000

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR PART NO.	QTY	BEC PART NO.
A6					
08265300A	REV: A*	PWA '8201' FILTER			
AR1	IC OP37EP OP AMP	08885	OP37EP	1	53521400A
AR2-4	IC 310N OP AMP	27014	LM310N	3	535035000
AR5	IC 357N OP AMP	27014	LF357N	1	535098000
AR6	IC TL072CP DUAL OP AMP	01295	TL072CP	1	535092000
AR7-8	IC 310N OP AMP	27014	LM310N	2	535035000
AR9	IC TL072CP DUAL OP AMP	01295	TL072CP	1	535092000
AR10	IC 310N OP AMP	27014	LM310N	1	535035000
AR11	IC 5534AN OP AMP	18324	NE5534AN	1	535061000
AR12	IC 358P OP AMP	27014	LF358N	1	535040000
AR13	IC TL072CP DUAL OP AMP	01295	TL072CP	1	535092000
C1-2	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	2	283336000
C3	CAP EL 100uF 20% 25V	S4217	SM-25-VB-101M	1	283334000
C4	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C5(SEL)	CAP MICA 820pF 5% 300V	14855	CD15FC821J03	1	200110000
C5	CAP MICA 910pF 5% 100V	57582	KD15911J101	1	200125000
C6	CAP MICA 1000pF 1% 100V	51406	DM15-102F	1	200113000
C7	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C8	CAP MICA 180pF 1% 100V	14855	CD5FA181F	1	205040000
C9	CAP MICA 470pF 1% 500V	14855	CD15FD471F03	1	200050000
C10-11	CAP MPC 0.01uF 2% 50V	14752	852A-1A-103G	2	234142000
C12	CAP MICA 1000pF 1% 100V	51406	DM15-102F	1	200113000
C13	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C14	CAP MICA 470pF 1% 500V	14855	CD15FD471F03	1	200050000
C15-16	CAP TANT 100uF 20% 10V	58289	198D107X0010PE4	2	283291000
C17	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C18	CAP MICA 7pF 5% 300V	14855	CD5CC070J	1	205030000
C19-20	CAP MPC 0.1uF 2% 50V	14752	852A-1-A-104G	2	234139000
C21	CAP MPC 0.01uF 2% 50V	14752	852A-1A-103G	1	234142000
C22-23	CAP MPC 0.1uF 2% 50V	14752	852A-1-A-104G	2	234139000
C24	CAP MPC 0.01uF 2% 50V	14752	852A-1A-103G	1	234142000
C25-26	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	2	224268000
C27-28	CAP MPC 0.01uF 2% 50V	14752	852A-1A-103G	2	234142000
C29	CAP MPC 0.047uF 2% 50V	14752	852A-1-A473G	1	234144000
C30	CAP EL 100uF 20% 25V	S4217	SM-25-VB-101M	1	283334000
C31	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C32	CAP MICA 1000pF 1% 100V	51406	DM15-102F	1	200113000
C33	CAP MICA 240pF 1% 500V	00853	D10FD241F	1	200124000
C34	CAP MICA 1000pF 1% 100V	51406	DM15-102F	1	200113000
C35	CAP MICA 200pF 2% 500V	14855	CD15FD201G	1	200053000
C36	CAP MICA 100pF 1% 300V	14855	CD5FC101F	1	205039000
C37	CAP MICA 120pF 1% 50V	20307	DM5-FY121F	1	205050000
C38	CAP MICA 100pF 1% 300V	14855	CD5FC101F	1	205039000
C39	CAP MICA 1000pF 1% 100V	51406	DM15-102F	1	200113000
C40	CAP MICA 470pF 1% 500V	14855	CD15FD471F03	1	200050000
C41	CAP MICA 75pF 1% 300V	20307	DM5-EC750F	1	205056000
C42-43	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	2	283336000
C44-45	CAP MICA 1000pF 1% 100V	51406	DM15-102F	2	200113000

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFRG PART NO.	QTY	BEC PART NO.
C46-47	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	2	224268000
C48	CAP EL 100uF 20% 25V	S4217	SM-25-VB-101M	1	283334000
C49-51	CAP MPC 0.01uF 2% 50V	14752	652A-1A-103G	3	234142000
C52	CAP MPC 0.1uF 2% 50V	14752	652A-1-A-104G	1	234139000
C53	CAP MPC 0.01uF 2% 50V	14752	652A-1A-103G	1	234142000
C54-55	CAP MPC 0.1uF 2% 50V	14752	652A-1-A-104G	2	234139000
C56	CAP MICA 22pF 5% 300V	14655	CD5CC220J	1	205036000
C57	CAP MICA 150pF 5% 100V	57582	KD5151J101	1	205009000
C58	CAP MICA 5.0pF 10% 300V	14655	CD5CC050D	1	205000000
CR1-3	DIODE SIG 1N914	01295	1N914	3	530058000
CR4-5	DIODE SIG FDH-300	07263	FDH300	2	530052000
CR7-8	DIODE SIG 1N914	01295	1N914	3	530058000
K1-3	RELAY DUAL FORM "C" 12V	ARMT	TQ2E-12V	3	47106100A
L1-3	INDUCTOR 5.6uH 10%	24226	15/561	3	400306000
L4	COIL ASSY 2270 uH	04901	40043701A	1	40043701A
L5	COIL ASSY 3641 uH	04901	40043801A	1	40043801A
L6	COIL ASSY 2270 uH	04901	40043701A	1	40043701A
Q1	TRANS NPN 2N3904	04713	2N3904	1	528071000
R1	RES MF 662 OHM 1% 1/4W	19701	5043ED562R0F	1	341272000
R2	RES MF 619 OHM 1% 1/4W	19701	5043ED619R0F	1	341278000
R3	RES MF 7.50K 1% 1/4W	19701	5043ED7K500F	1	341384000
R4	RES MF 619 OHM 1% 1/4W	19701	5043ED619R0F	1	341278000
R6	RES MF 619 OHM 1% 1/4W	19701	5043ED619R0F	1	341278000
R7	RES MF 7.50K 1% 1/4W	19701	5043ED7K500F	1	341384000
R8	RES MF 619 OHM 1% 1/4W	19701	5043ED619R0F	1	341278000
R9-10	RES MF 9.000K 0.1% 1/4W	64537	PME55-T2	2	324354000
R11-12	RES MF 1.000K 0.1% 1/8W	03888	PME55-T2	1	324241000
R13	RES MF 9.000K 0.1% 1/4W	64537	PME55-T2	2	324354000
R15	RES MF 100 OHM 1% 1/4W	19701	5043ED100R0F	1	341200000
R17	RES MF 1.000K 0.1% 1/8W	03888	PME55-T2	1	324241000
R19	RES MF 26.7 OHM 1% 1/4W	19701	5043ED026R7F	1	341141000
R20	RES MF 26.7K 1% 1/4W	19701	5043ED26K70F	1	341441000
R21	RES MF 105K 1% 1/4W	19701	5043ED105K0F	1	341502000
R22	RES MF 2.67K 1% 1/4W	19701	5043ED2K670F	1	341341000
R23	RES MF 10.5K 1% 1/4W	19701	5043ED10K50F	1	341402000
R24	RES MF 2.61K 1% 1/4W	19701	5043ED2K619F	1	341340000
R25	RES MF 10.5K 1% 1/4W	19701	5043ED10K50F	1	341402000
R26	RES MF 6.19K 1% 1/4W	19701	5043ED6K190F	1	341378000
R27	RES MF 536K 1% 1/4W	19701	RN55D-5363-F	1	341570000
R28	RES MF 53.6K 1% 1/4W	19701	5043ED53K60F	1	341470000
R29	RES MF 1.13K 1% 1/4W	19701	5043ED1K130F	1	341305000
R30	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R31	RES MF 3.65K 1% 1/4W	19701	5043ED3K650F	1	341354000
R32	RES MF 26.7K 1% 1/4W	19701	5043ED26K70F	1	341441000
R33	RES MF 182K 1% 1/4W	19701	5043ED182K0F	1	341525000
R34	RES MF 80.00K 0.1% 1/8W	64537	PME55-T9	1	32592000A
R35	RES MF 11.5K 1% 1/4W	19701	5043ED11K50F	1	341406000

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR PART NO.	QTY	BEC PART NO.
R36	RES MF 16.5K 1% 1/4W	19701	5043ED16K50F	1	341421000
R37	RES MF 73.2K 1% 1/4W	19701	5043ED73K20F	1	341483000
R38	RES MF 80.00K 0.1% 1/8W	64537	PME55-T9	1	32562000A
R39	RES MF 4.87K 1% 1/4W	19701	5043ED4K870F	1	341366000
R40	RES MF 80.00K 0.1% 1/8W	64537	PME55-T9	1	32562000A
R41	RES MF 9.78K 1% 1/4W	19701	5043ED9K780F	1	341395000
R42	RES MF 48.7K 1% 1/4W	19701	5043ED48K70F	1	341466000
R43	RES MF 5.78K 1% 1/4W	19701	5043ED5K780F	1	341373000
R44	RES MF 2.49K 1% 1/4W	19701	5043ED2K490F	1	341338000
R45	RES MF 4.99K 1% 1/4W	19701	5043ED4K990F	1	341367000
R46-47	RES MF 7.50K 1% 1/4W	19701	5043ED7K500F	2	341384000
R48	RES MF 243K 1% 1/4W	19701	5043ED243K0F	1	341537000
R49	RES MF 3.920K 0.1% 1/8W	64537	PME55-T2	1	324311000
R50	RES MF 56.2K 0.1% 1/8W	64537	PME55-T2	1	324448000
R51	RES MF 11.5K 1% 1/4W	19701	5043ED11K50F	1	341406000
R52	RES MF 48.7K 1% 1/4W	19701	5043ED48K70F	1	341466000
R53	RES MF 1.54K 1% 1/4W	19701	5043ED1K540F	1	341318000
R54	RES MF 2.21K 1% 1/4W	19701	5043ED2K210F	1	341333000
R55	RES MF 600 OHM 0.25% 1/8W	64537	PME55-T2	1	324215000
R56	RES MF 4.99K 1% 1/4W	19701	5043ED4K990F	1	341367000
R57-58	RES MF 243 OHM 1% 1/4W	19701	5043ED243R0F	1	341237000
U1	IC 74HCT138 1 OF 8 DECODER	01295	74HCT138N	1	534375000
U2	IC 74HCT273	01295	SN74HCT273N	1	534377000
U3	IC 6208 4 CHAN DIF MULTPXR	32293	IH6208CPE	1	534266000
U4-5	IC 6108 CMOS CHAN MULTPXR	32293	IH6108CPE	2	534265000
U6	IC 74HCT273	01295	SN74HCT273N	1	534377000
U7	IC 6108 CMOS CHAN MULTPXR	32293	IH6108CPE	1	534265000
U8-9	IC ANALOG SWITCH DG419	17856	DG419	2	53452400A
XAR1-13	SOCKET IC 8 PIN	06776	ICN-083-S3-G	13	473041000
XU8-U9	SOCKET IC 8 PIN	06776	ICN-083-S3-G	2	473041000
XU1	SOCKET IC 16 PIN	06776	ICN-163-S3-G	1	473042000
XU2	SOCKET IC 20 PIN	06776	ICN-203-S3-G	1	473065000
XU3-5	SOCKET IC 16 PIN	06776	ICN-163-S3-G	3	473042000
XU6	SOCKET IC 20 PIN	06776	ICN-203-S3-G	1	473065000
XU7	SOCKET IC 16 PIN	06776	ICN-163-S3-G	1	473042000
A7					
08252001A REV: A PWA '8200' DISTORTION ANALYZER					
AR1	IC 356P OP AMP	04713	LF356N	1	535040000
AR2	IC 5532A DUAL OP AMP 8 DIP	01295	NE5532AP	1	53512100A
AR3	IC TL072CP DUAL OP AMP	01295	TL072CP	1	535092000
AR4	IC OP-07EP OP AMP	06665	OP-07EP	1	535110000
AR5	IC 393 OP AMP	27014	LM393N	1	535107000
AR7-8	IC TL072CP DUAL OP AMP	01295	TL072CP	2	535092000
AR9	IC 5532A DUAL OP AMP 8 DIP	01295	NE5532AP	1	53512100A
AR10	IC TL072CP DUAL OP AMP	01295	TL072CP	1	535092000
AR11	IC OP-07EP OP AMP	06665	OP-07EP	1	535110000
AR12	IC 393 OP AMP	27014	LM393N	1	535107000
C1	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR PART NO.	QTY	BEC PART NO.
C2	CAP MICA 250pF 1% 50V	14655	CD5FY251F	1	205034000
C3-6	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	4	224268000
C7	CAP MPC 0.22uF 2% 50V	14752	652A-1-A224G	1	234167000
C8	CAP MICA 75pF 5% 300V	57582	KD5750J301	1	205043000
C9	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C12	CAP MICA 1000PF 1% 50V	51406	DM15-102F	1	200113000
C13-14	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	2	224268000
C15	CAP MICA 500pF 1% 500V	14655	CD15FD501F	1	200123000
C16	CAP TANT 10uF 20% 25V	56289	196D106X0025KA1	1	283293000
C17	CAP TANT 100uF 20% 10V	56289	196D107X0010PE4	1	283291000
C19	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C20	CAP MPC 0.22uF 2% 50V	14752	652A-1-A224G	1	234167000
C21-22	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	2	283336000
C23	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C24	CAP MICA 1000PF 1% 50V	51406	DM15-102F	1	200113000
C25-26	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	2	283336000
C27	CAP EL 100uF 20% 25V	S4217	SM-25-VB-100-M	1	283334000
C28	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	1	283336000
CR1-2	DIODE SIG 1N914	01295	1N914	2	530058000
CR4-5	DIODE SIG 1N5713	28480	1N5713	2	530161000
J1	CONN M 2 CKT ST .1CT	27264	22-10-2021	1	477381000
L1-2	INDUCTOR 5.6uH 10%	24226	15/561	2	400308000
L3	INDUCTOR VK200/20-4B	02114	VK-200-20/4B	1	400409000
P1	SHUNT 2 CIRCUIT	27264	15-38-1024	1	483253000
Q1-10	TRANS FET 2N5653	SEMI,	2N5653	10	528058000
R1	RES MF 100K 1% 1/4W	19701	5043ED100K0F	1	341500000
R2	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R3	RES MF 1.82K 1% 1/4W	19701	5043ED1K820F	1	341325000
R4	RES MF 600 OHM 0.25% 1/8W	64537	PME55-T2	1	324215000
R5	RES MF 33.2K 1% 1/4W	19701	5043ED33K20F	1	341450000
R6	RES MF 100K 1% 1/4W	19701	5043ED100K0F	1	341500000
R7-8	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	2	341400000
R9	RES NETWORK 100K 2% 1.5W	71450	750-61-R100K	1	345032000
R10	RES MF 100K 1% 1/4W	19701	5043ED100K0F	1	341500000
R11	RES VAR 10K 10% 0.5W	73138	72XWR10K	1	311348000
R12	RES MF 100K 1% 1/4W	19701	5043ED100K0F	1	341500000
R13	RES MF 48.7K 1% 1/4W	19701	5043ED48K70F	1	341486000
R14	RES MF 10.0 OHM 1% 1/4W	19701	5043ED10R00F	1	341100000
R15	RES MF 2.00K 1% 1/4W	19701	5043ED2K000F	1	341329000
R16	RES MF 619K 1% 1/4W	19701	RN55D-6193-F	1	341576000
R17	RES MF 6.19K 1% 1/4W	19701	5043ED6K190F	1	341378000
R18	RES MF 68.1K 1% 1/4W	19701	5043ED68K10F	1	341480000
R19	RES MF 4.99K 1% 1/4W	19701	5043ED4K990F	1	341367000
R20	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	1	341400000
R23-24	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	2	341400000
R26	RES MF 5.11K 1% 1/4W	19701	5043ED5K110F	1	341368000
R27	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	1	341400000
R28	RES MF 5.11K 1% 1/4W	19701	5043ED5K110F	1	341368000
R29	RES MF 15.0K 1% 1/4W	19701	5043ED15K00F	1	341417000

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR. PART NO.	QTY	BEC PART NO.
R30	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R31	RES MF 14.0K 1% 1/4W	19701	5043ED14K00F	1	341414000
R32	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	1	341400000
R33	RES MF 150K 1% 1/4W	19701	5043ED150K0F	1	341517000
R34	RES MF 2.00K 1% 1/4W	19701	5043ED2K000F	1	341329000
R35	RES MF 4.99K 1% 1/4W	19701	5043ED4K990F	1	341357000
R36	RES MF 100K 1% 1/4W	19701	5043ED100K0F	1	341500000
R37	RES MF 14.0K 1% 1/4W	19701	5043ED14K00F	1	341414000
R38	RES MF 619K 1% 1/4W	19701	RN55D-6193-F	1	341576000
R39	RES MF 6.19K 1% 1/4W	19701	5043ED6K190F	1	341376000
R40	RES MF 68.1K 1% 1/4W	19701	5043ED68K10F	1	341480000
R41	RES MF 10.0 OHM 1% 1/4W	19701	5043ED10R00F	1	341100000
R42	RES MF 48.7K 1% 1/4W	19701	5043ED48K70F	1	341466000
R43	RES MF 100K 1% 1/4W	19701	5043ED100K0F	1	341500000
R44	RES VAR 10K 10% 0.5W	73138	72XWR10K	1	311348000
R45	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	1	341400000
R46	RES MF 100K 1% 1/4W	19701	5043ED100K0F	1	341500000
R48	RES MF 100K 1% 1/4W	19701	5043ED100K0F	1	341500000
R49	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	1	341400000
R50	RES MF 2.43K 1% 1/4W	19701	RN55D-2431-F	1	341337000
R51	RES MF 100K 1% 1/4W	19701	5043ED100K0F	1	341500000
R52	RES MF 3.01K 1% 1/4W	19701	5043ED3K010F	1	341348000
R53-54	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	2	341400000
R55	RES MF 12.7K 1% 1/4W	19701	5043ED12K70F	1	341410000
R56	RES MF 3.32K 1% 1/4W	19701	5043ED3K320F	1	341350000
R57	RES MF 100K 1% 1/4W	19701	5043ED100K0F	1	341500000
R58	RES NETWORK 100K 2% 1.5W	71450	750-81-R100K	1	345032000
R59-64	RES MF 100K 1% 1/4W	19701	5043ED100K0F	6	341500000
R65	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R66	RES MF 4.32K 1% 1/4W	19701	5043ED4K320F	1	341361000
R67	RES MF 881 OHM 1% 1/4W	19701	5043ED681R0F	1	341280000
TP1-4	TERMINAL WIRE LOOP TEST POINT	31313	TP-103-02	4	48330600A
U1	IC 13333 ANALOG SWITCH LF	27014	LF13333N	1	535095000
U2	IC 74HCT138 1 OF 8 DECODER	01295	74HCT138N	1	534375000
U3	IC 7528 CMOS 8 BIT DAC	51640	AD7528JN	1	535108000
U6-7	IC 4200ANB RC	07933	RC4200ANB	2	535083000
U8	IC 74HCT273	01295	SN74HCT273N	1	534377000
XAR1-5	SOCKET IC 8 PIN	06776	ICN-083-S3-G	5	473041000
XAR7-12	SOCKET IC 8 PIN	06776	ICN-083-S3-G	6	473041000
XU1-2	SOCKET IC 16 PIN	06776	ICN-163-S3-G	2	473042000
XU3	SOCKET IC 20 PIN	06776	ICN-203-S3-G	1	473065000
XU6-7	SOCKET IC 8 PIN	06776	ICN-083-S3-G	2	473041000
XU8	SOCKET IC 20 PIN	06776	ICN-203-S3-G	1	473065000

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR. PART NO.	QTY	BEC PART NO.
A8					
08262201A REV: AA PWA '8201' DETECTOR					
C1	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	1	283336000
C2	CAP EL 100uF 20% 25V	S4217	SM-25-VB-101M	1	283334000
C3	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	1	283336000
C4-5	CAP TANT 100uF 20% 10V	56289	196D107X0010PE4	2	283291000
C6	CAP TANT 10uF 20% 25V	56289	196D108X0025KA1	1	283293000
C7	CAP MICA 5.0pF 10% 300V	14655	CD5CC050D	1	205000000
C8	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C9	CAP TANT 56uF 10% 6V	56289	196D566X9006KA1	1	283228000
C10-11	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	2	283336000
C12	CAP EL 47uF 20% 50V	S4217	SM50VB47	1	283358000
C13	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	1	283336000
C14-15	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	2	224268000
C16	CAP MICA 5.0pF 10% 300V	14655	CD5CC050D	1	205000000
C17-18	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	2	283336000
C19	CAP TANT 56uF 10% 6V	56289	196D566X9006KA1	1	283228000
C20-21	CAP MPC 0.1uF 2% 50V	14752	652A-1-A-104G	2	234139000
C22	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	1	283336000
C23	CAP VAR CER 5.1-50pF 250V GRN	52789	GKR50000	1	281006000
C24	CAP TANT 1.0uF 10% 35V ONLY	56289	196D105X9035HA1	1	283216000
C25	CAP TANT 56uF 10% 6V	56289	196D566X9006KA1	1	283228000
C26	CAP TANT 2.2uF 20% 35V	61637	T368B225M035ASC2513	1	283317000
C27-30	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	4	224268000
C31	CAP CER 0.001uF 10% 100V	04222	SR151C102KAA	1	224270000
C32-34	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	3	224268000
C35	CAP TANT 10uF 20% 25V	56289	196D108X0025KA1	1	283293000
C36	CAP TANT 100uF 20% 10V	56289	196D107X0010PE4	1	283291000
C37	CAP CER 0.022uF 10% 50V	61637	C052K223K5X5CA	1	224302000
C38	CAP MICA 12pF 5% 300V	57582	KD5120J301	1	205005000
C39	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C40-41	CAP MPC 1.0uF 10% 50V	14752	652A-1-A-105K	2	234152000
C42	CAP TANT 56uF 10% 6V	56289	196D566X9006KA1	1	283228000
CR1-2	DIODE HSCH1001 (1N6263)	28480	HSCH-1001	2	530174000
CR3-4	DIODE SIG FDH-300	07263	FDH300	2	530052000
CR5-10	DIODE SIG 1N914	01295	1N914	6	530058000
JP1	WIRE BARE SOLID 24 AWG	04901	920148240	1	920148240
L1-3	INDUCTOR 5.6uH 10%	24226	15/561	3	400308000
R1	RES MF 5.000K 0.1% 1/8W	64537	PME55-T2	1	324328000
R2	RES MF 3.000K 0.1% 1/8W	64537	PME55-T2	1	324300000
R3-4	RES MF 1.000K 0.1% 1/8W	03888	PME55-T2	2	324241000
R5	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	1	341400000
R6	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R7	RES MF 10.5K 1% 1/4W	19701	5043ED10K50F	1	341402000
R8	RES MF 9.000K 0.1% 1/4W	64537	PME55-T2	1	324354000
R9	RES MF 1.000K 0.1% 1/8W	03888	PME55-T2	1	324241000
R11	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	1	341400000
R12	RES MF 301 OHM 1% 1/4W	19701	5043ED301R0F	1	341248000

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR PART NO.	QTY	BEC PART NO.
R13	RES MF 75.0K 1% 1/4W	19701	5043ED75K00F	1	341484000
R14	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R15	RES MF 11.0K 1% 1/4W	19701	5043ED11K00F	1	341404000
R16	RES MF 10.5K 1% 1/4W	19701	5043ED10K50F	1	341402000
R17	RES MF 11.0K 1% 1/4W	19701	5043ED11K00F	1	341404000
R18	RES MF 9.000K 0.1% 1/4W	64537	PME55-T2	1	324354000
R19	RES MF 1.000K 0.1% 1/8W	03888	PME55-T2	1	324241000
R20	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R21	RES MF 22.1K 1% 1/4W	19701	RN55D-2212-F	1	341433000
R22	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R23	RES MF 200 OHM 1% 1/4W	19701	5043ED200R0F	1	341229000
R24	RES MF 22.1K 1% 1/4W	19701	RN55D-2212-F	1	341433000
R25	RES MF 200 OHM 1% 1/4W	19701	5043ED200R0F	1	341229000
R26	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R27	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	1	341400000
R28	RES MF 10.5K 1% 1/4W	19701	5043ED10K50F	1	341402000
R29	RES MF 4.99K 1% 1/4W	19701	5043ED4K990F	1	341367000
R30	RES MF 47.5K 1% 1/4W	19701	5043ED47K50F	1	341465000
R31	RES MF 4.99K 1% 1/4W	19701	5043ED4K990F	1	341367000
R32-33	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	2	341400000
R34	RES MF 12.1K 1% 1/4W	19701	5043ED12K10F	1	341408000
R35	RES MF 2.49K 1% 1/4W	19701	5043ED2K490F	1	341338000
R36-38	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	3	341400000
R39	RES MF 2.67K 1% 1/4W	19701	5043ED2K670F	1	341341000
R40	RES MF 33.2K 1% 1/4W	19701	5043ED33K20F	1	341450000
R41	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	1	341400000
R42	RES MF 2.49K 1% 1/4W	19701	5043ED2K490F	1	341338000
R43	RES MF 20.0K 1% 1/4W	19701	5043ED20K00F	1	341429000
R44	RES MF 4.99K 1% 1/4W	19701	5043ED4K990F	1	341367000
R45	RES MF 100K 1% 1/4W	19701	5043ED100K0F	1	341500000
R46	RES MF 750K 1% 1/4W	19701	5043ED750K0F	1	341584000
R47	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	1	341400000
R48	RES MF 100 OHM 1% 1/4W	19701	5043ED100R0F	1	341200000
R49	RES MF 10.5K 1% 1/4W	19701	5043ED10K50F	1	341402000
R50	RES NETWORK 3.3K 2% 2W	73138	694-3-R10K-D	1	345017000
R53	RES MF 750K 1% 1/4W	19701	5043ED750K0F	1	341584000
R54	RES MF 2.43K 1% 1/4W	19701	RN55D-2431-F	1	341337000
R55	RES NETWORK 10K 0.5% 1/2W	73138	694-3-R10K-D	1	345041000
R56	RES COMP 2.0M 5% 1/4W	01121	CB2055	1	343629000
R57-59	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	3	341400000
R60	RES MF 100K 1% 1/4W	19701	5043ED100K0F	1	341500000
R61	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R62	RES MF 1.82K 1% 1/4W	19701	5043ED1K820F	1	341325000
R63-64	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	2	341400000
R65	RES MF 2.00K 1% 1/4W	19701	5043ED2K000F	1	341329000
R66	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R67	RES MF 499 OHM 1% 1/4W	19701	5043ED499R0F	1	341267000
R68	RES MF 402K 1% 1/4W	19701	5043ED402K0F	1	341558000
R69	RES MF 2.00K 1% 1/4W	19701	5043ED2K000F	1	341329000
R70	RES MF 49.9K 1% 1/4W	19701	5043ED499K0F	1	341487000
R71	RES MF 38.3K 1% 1/4W	19701	5043ED38K30F	1	341456000

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR PART NO.	QTY	BEC PART NO.
R72	RES MF 619K 1% 1/4W	19701	5043ED819K0F	1	341578000
R73	RES MF 200K 1% 1/4W	19701	5043ED200K0F	1	341528000
U1	IC 13333 ANALOG SWITCH LF	27014	LF13333N	1	535095000
U2	IC PEEL DETECTOR 8220	04901	53469600A	1	53469600A
U3	IC 74HCT273	01295	SN74HCT273N	1	534377000
U4	IC 13202N 4 NOR OPEN SW	27014	LF13202N	1	534252000
U5	IC 13333 ANALOG SWITCH LF	27014	LF13333N	1	535095000
U6-7	IC 4052B MULTIPLEXER	02735	CD4052BE	2	534140000
U8	IC AD536 TRUE RMS/DC CONV	51640	AD636AJD	1	535105000
U9	IC 6108 CMOS CHAN MULTPXR	32293	IH6108CPE	1	534285000
U10	IC 74HCT273	01295	SN74HCT273N	1	534377000
U11	IC 356P OP AMP	27014	LF356N	1	535040000
U12	IC TL072CP DUAL OP AMP	01295	TL072CP	1	535092000
U13	IC TL074CN OP AMP QUAD	01295	TL074CN	1	535082000
U14	IC HA3-2625-5 OP AMP	34371	HA3-2625-5	1	53511800A
U15-16	IC 3080E OP AMP	02735	CA3080E	2	535091000
U17	IC TL074CN OP AMP QUAD	01295	TL074CN	1	535082000
U18	IC HA3-2625-5 OP AMP	34371	HA3-2625-5	1	53511800A
U19	IC TL072CP DUAL OP AMP	01295	TL072CP	1	535092000
U20	IC 5534AN OP AMP	18324	NE5534AN	1	535061000
U21	IC 5534AN OP AMP	18324	NE5534AN	1	535061000
U22-23	IC TL072CP DUAL OP AMP	01295	TL072CP	2	535092000
XU1	SOCKET IC 16 PIN	06776	ICN-163-S3-G	1	473042000
XU2-3	SOCKET IC 20 PIN	06776	ICN-203-S3-G	2	473065000
XU4-7	SOCKET IC 16 PIN	06776	ICN-163-S3-G	4	473042000
XU8	SOCKET IC 14 PIN	06776	ICN-143-S3-G	1	473019000
XU9	SOCKET IC 16 PIN	06776	ICN-163-S3-G	1	473042000
XU10	SOCKET IC 20 PIN	06776	ICN-203-S3-G	1	473065000
XU11-12	SOCKET IC 8 PIN	06776	ICN-083-S3-G	2	473041000
XU13	SOCKET IC 14 PIN	06776	ICN-143-S3-G	1	473019000
XU14-16	SOCKET IC 8 PIN	06776	ICN-083-S3-G	3	473041000
XU17	SOCKET IC 14 PIN	06776	ICN-143-S3-G	1	473019000
XU18-23	SOCKET IC 8 PIN	06776	ICN-083-S3-G	6	473041000
A9					
08262101A REV: A PWA '8201' CPU					
BT1	CELL LITHIUM 3V	54473	BR2325-1HB	1	556007000
C1	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C2	CAP TANT 4.7uF 10% 10V	56289	196D475X9010HA1	1	283228000
C3-9	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	7	224268000
C10	CAP TANT 10uF 20% 25V	56289	196D106X0025KA1	1	283293000
C11-14	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	4	224268000
C15	CAP EL 100uF 20% 25V	S4217	SM-25-VB-101M	1	283334000
C16-18	CAP TANT 10uF 20% 25V	56289	196D106X0025KA1	3	283293000
C19	CAP MICA 330pF 5% 50V	14655	CD5FY331J	1	205029000
CR1-2	DIODE SIG 1N914	01295	1N914	2	530059000
CR3	DIODE HSCH1001 (1N6263)	28480	HSCH-1001	1	530174000
DS1	LED YELLOW DIFF 5082-4684	28480	HLMP-1401	1	536034000

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR PART NO.	QTY	BEC PART NO.
DS2	LED RED DIFF HLMP-8820	28480	HLMP-8820	1	536028000
J1	CONN M 40 CKT HDR DBL ROW .1CT	06776	NSH-40DB-S2-TG	1	47742240A
J2-3	CONN M 26 CKT HDR DBL ROW .1CT	06776	NSH-26DB-S2-TG	2	47742226A
JP1-3	SHUNT 2 CIRCUIT	27264	15-38-1024	3	483253000
L1	INDUCTOR 5.6uH 10%	24226	15/561	1	400308000
L2	INDUCTOR VK200/20-4B	02114	VK-200-20/4B	1	400409000
L3	INDUCTOR 5.6uH 10%	24226	15/561	1	400308000
Q1	TRANS PNP 2N4403	04713	2N4403	1	528122000
R1	RES NETWORK 3.3K 2% 1.5W 10pin	71450	750-101-R3.3K	1	345030000
R2	RES MF 100 OHM 1% 1/4W	19701	5043ED100R0F	1	341200000
R3	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R4-5	RES MF 332 OHM 1% 1/4W	19701	5043ED332R0F	2	341250000
R6	RES MF 1.21K 1% 1/4W	19701	5043ED1K210F	1	341308000
R8	RES MF 3.32K 1% 1/4W	19701	5043ED3K320F	1	341350000
R10	RES NETWORK 3.3K 2% 0.9W 6pin	71450	750-81-R3.3K	1	34504500A
R11	RES NETWORK 10K 0.5% 1/2W	73138	694-3-R10K-D	1	345041000
R12	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R13	RES MF 3.32K 1% 1/4W	19701	5043ED3K320F	1	341350000
U1	IC 74LS390 DU DEC CTR	01295	SN74LS390N	1	534329000
U2	IC PAL V3 DTACK '8220'	04901	53459900A	1	53459900A
U3	IC 74HCT03 QUAD 2 INPUT NAND	18324	74HCT03N	1	53444212A
U4	IC 7705 SUPPLY VOLTAGE SUPVR	01295	TL7705ACP	1	53442200A
U5	IC 74LS148 8 TO 3 LINE ENCODER	01295	SN74LS148N	1	534234000
U6	IC 74HCT02 QUAD 2 INPUT NOR	18324	74HCT02N	1	53444211A
U7	IC 74F139 DUAL 1 OF 4 DECODER	07283	74F139PC	1	53448000A
U8	IC 68HC000CP	HITAC	HD68HC000CP-10	1	53449200A
U9	IC PEEL PROG CPU '8220'	04901	53456400A	1	53456400A
U10	IC EPROM PROG 8201 (II)	04901	53469800A	1	53469800A
U11	IC PEEL 153 PROG '8201/20'	04901	53454900B	1	53454900B
U12	IC 7673 AUTO BATTERY BACKUP SW	32293	ICL7673CPA	1	53448500A
U13	IC AD581JH VOLT REF	51640	AD581JH	1	535053000
U14	IC EPROM PROG 8201 (I)	04901	53469700A	1	53469700A
U15	IC TC 85257 PL-10	TOSH	TC55257APL-10	1	53449400A
U16	IC 74LS541 OCTAL BUFFER	01295	SN74LS541N	1	534381000
U17	IC TC 85257 PL-10	TOSH	TC55257APL-10	1	53449400A
U18	IC74LS245 OCT BUS TRANSCEIVER	01295	SN74LS245N	1	53437200A
U19	IC 6914ANL IEEE BUS PROCESSOR	01295	TMS9914ANL	1	534288000
U20	IC 74LS367 HEX BUFF DRYR	01295	SN74LS367N	1	534257000
U21	IC74LS245 OCT BUS TRANSCEIVER	01295	SN74LS245N	1	53437200A
U22	IC 82C55 INTERFACE	34371	CP82C55A	1	53441100A
U23	IC DAC725JP DUAL D/A CONVERTER	13919	DAC725JP	1	53514500A
U24	IC 75160 IEEE BUS TRANSCEIVER	01295	SN75160BN	1	534286000
U25	IC 75161 IEEE BUS TRANSCEIVER	01295	SN75161BN	1	534287000
U26	IC EEPROM X24C16 2Kx8	60395	X24C16-P	1	53449500A
U27	IC 311N OP AMP COMPARATOR	27014	LM311N	1	535034000
XJP3	CONN M 2 CKT ST .1CT	27264	22-10-2021	1	477361000
XJP1/2	CONN M 04 CKT HDR DBL ROW .1CT	06776	NSH-04DB-S2-TG	1	47742204A

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR PART NO.	QTY	BEC PART NO.
XU1	SOCKET IC 16 PIN	06776	ICN-163-S3-G	1	473042000
XU2	SOCKET IC 20 PIN	06776	ICN-203-S3-G	1	473065000
XU3	SOCKET IC 14 PIN	06776	ICN-143-S3-G	1	473019000
XU4	SOCKET IC 8 PIN	06776	ICN-083-S3-G	1	473041000
XU5	SOCKET IC 16 PIN	06776	ICN-163-S3-G	1	473042000
XU6	SOCKET IC 14 PIN	06776	ICN-143-S3-G	1	473019000
XU7	SOCKET IC 16 PIN	06776	ICN-163-S3-G	1	473042000
XU8	SOCKET IC 68 PIN CHIP CARRIER	32575	641749-2	1	47308168A
XU9	SOCKET IC 20 PIN	06776	ICN-203-S3-G	1	473065000
XU10	SOCKET IC 28 PIN	06776	ICN-286-S4-TG	1	473044000
XU11	SOCKET IC 20 PIN	06776	ICN-203-S3-G	1	473065000
XU12	SOCKET IC 8 PIN	06776	ICN-083-S3-G	1	473041000
XU13	SOCKET TRANSISTOR 3 CIR TO-18	06776	SD-5173-N	1	47307800A
U14-15	SOCKET IC 28 PIN	06776	ICN-286-S4-TG	2	473044000
XU16	SOCKET IC 20 PIN	06776	ICN-203-S3-G	1	473065000
XU17	SOCKET IC 28 PIN	06776	ICN-286-S4-TG	1	473044000
XU18	SOCKET IC 20 PIN	06776	ICN-203-S3-G	1	473065000
XU19	SOCKET IC 40 PIN	06776	ICN-406-S4-TG	1	473052000
XU20	SOCKET IC 16 PIN	06776	ICN-163-S3-G	1	473042000
XU21	SOCKET IC 20 PIN	06776	ICN-203-S3-G	1	473065000
XU22	SOCKET IC 40 PIN	06776	ICN-406-S4-TG	1	473052000
XU23	SOCKET IC 28 PIN	06776	ICN-286-S4-TG	1	473044000
XU24-25	SOCKET IC 20 PIN	06776	ICN-203-S3-G	2	473065000
XU26-27	SOCKET IC 8 PIN	06776	ICN-083-S3-G	2	473041000
XY1	SOCKET IC 14 PIN	06776	ICN-143-S3-G	1	473019000
Y1	CRYSTAL OSC 18.432 MHz TTL DIP	NDK	TD1100C18.432	1	54790502A
A10					
06251600B REV: E* PWA '8200' COUNTER					
AR1	IC TL372CP OP AMP	01295	TLC372CP	1	535118000
AR2	IC HA3-2625-5 OP AMP	34371	HA3-2625-5	1	53511900A
AR3	IC 318N OP AMP	27014	LM318N	1	535031000
C1-2	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	2	283336000
C3	CAP EL 100uF 20% 25V	S4217	SM-25-VB-100-M	1	283334000
C4	CAP TANT 1.0uF 10% 35V ONLY	56286	196D105X9036HA1	1	283216000
C5	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C6	CAP CER 0.001uF 10% 100V	04222	SR151C102KAA	1	224270000
C7	CAP EL 100uF 20% 25V	S4217	SM-25-VB-100-M	1	283334000
C8	CAP MICA 250pF 5% 50V	57582	KD251J101	1	205037000
C9-15	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	7	224268000
C16	CAP MICA 10pF 5% 300V	14655	CD5WCC100J	1	205002000
C17	CAP MICA 300pF 5% 50V	14655	CD5FY301J	1	205026000
C18	CAP MICA 500pF 1% 300V	14655	CD15FC561F	1	200091000
C19	CAP CER 0.001uF 10% 100V	04222	SR151C102KAA	1	224270000
C20	CAP MICA 300pF 5% 50V	14655	CD5FY301J	1	205026000
C21	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C22	CAP MICA 3.0pF +0.5pF 300V	14655	CD5CC0300	1	205013000
C23	CAP MICA 100pF 1% 300V	14655	CD5FC101F	1	205039000
CR1	DIODE SIG 1N914	01295	1N914	1	530058000
CR2	DIODE HSCH1001 (1N6263)	28480	HSCH-1001	1	530174000

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR PART NO.	QTY	BEC PART NO.
DS1-2	LED RED DIFF 5082-4684	28480	HLMP-1301	2	536024000
L1-2	INDUCTOR 5.6uH 10%	24228	15/851	2	400308000
L3	INDUCTOR VK200/20-4B	02114	VK-200-20/4B	1	400409000
L5-6	INDUCTOR 82uH 5%	59474	1315-10J	2	400318000
Q1	TRANS NPN MPS-8507	04713	MPS8507	1	528070000
Q2	TRANS NPN 2N3904	04713	2N3904	1	528071000
R1-2	RES MF 332 OHM 1% 1/4W	19701	5043ED332R0F	2	341250000
R3	RES MF 475 OHM 1% 1/4W	19701	5043ED475R0F	1	341265000
R4	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R5	RES MF 100K 1% 1/4W	19701	5043ED100K0F	1	341500000
R6	RES MF 811 OHM 1% 1/4W	19701	5043ED511R0F	1	341268000
R7	RES MF 86.2 OHM 1% 1/4W	19701	5043ED56R20F	1	341172000
R8-9	RES MF 100 OHM 1% 1/4W	19701	5043ED100R0F	2	341200000
R10-11	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	2	341400000
R12	RES MF 30.1K 1% 1/4W	19701	5043ED30K10F	1	341448000
R13	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R14	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	1	341400000
R15	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R16	RES MF 811 OHM 1% 1/4W	19701	5043ED511R0F	1	341268000
R17	RES MF 881 OHM 1% 1/4W	19701	5043ED881R0F	1	341280000
R18	RES MF 511 OHM 1% 1/4W	19701	5043ED511R0F	1	341268000
R19	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R20	RES NETWORK 800 OHM 0.5% 0.5W	73138	694-3-R500D	1	345035000
R21	RES MF 2.00K 1% 1/4W	19701	5043ED2K000F	1	341329000
R22-23	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	2	341300000
R24-25	RES MF 484 OHM 1% 1/4W	19701	5043ED484R0F	2	341264000
R26	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	1	341400000
R29	RES MF 20.0K 1% 1/4W	19701	5043ED20K00F	1	341429000
R30	RES MF 4.75K 1% 1/4W	19701	5043ED4K750F	1	341365000
U1	IC 74F04 HEX INVERTER	07283	74F04PC	1	534365000
U2	IC 74LS74 FLIP FLOP	01295	SN74LS74N	1	534157000
U3	IC 74HCT138 1 OF 8 DECODER	01295	74HCT138N	1	534375000
U4	IC 74LS00 2 INP POS NAND	01295	SN74LS00N	1	534167000
U5	IC 74LS490 DUAL DEC COUNTER	18324	N74LS490N	1	534238000
U6	IC 74LS74 FLIP FLOP	01295	SN74LS74N	1	534157000
U7	IC 74LS490 DUAL DEC COUNTER	18324	N74LS490N	1	534238000
U8	IC 74LS290 DEC CTR	01295	SN74LS290N	1	534328000
U9	IC 74F151PC	07283	74F151PC	1	534374000
U10	IC 74F74PC DUAL D FLIP FLOP	07283	74F74PC	1	534367000
U11	IC 4049A HEX BUFF	02735	CD4049AE	1	534172000
U12	IC 74F74PC DUAL D FLIP FLOP	07283	74F74PC	1	534367000
U13-14	IC 4040B COUNTER/DIVIDER	02735	CD4040BE	2	534275000
U15	IC 74HCT273	01295	SN74HCT273N	1	534377000
U16-19	IC 74HCT244	01295	74HCT244	4	534378000
U20	IC 74LS74 FLIP FLOP	01295	SN74LS74N	1	534157000
U21	IC 13333 ANALOG SWITCH LF	27014	LF13333N	1	535095000
U22	IC 4040B COUNTER/DIVIDER	02735	CD4040BE	1	534275000
U23	IC 74LS163 4 BIT COUNTER	01295	SN74LS163AN	1	534279000
U24	IC 74LS153 4-1 LINE DATA SEL	01295	SN74LS153N	1	534278000
XU1-2	SOCKET IC 14 PIN	06776	ICN-143-S3-G	2	473019000

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR. PART NO.	QTY	BEC PART NO.
XU3	SOCKET IC 16 PIN	06776	ICN-163-S3-G	1	473042000
XU4	SOCKET IC 14 PIN	06776	ICN-143-S3-G	1	473019000
XU5	SOCKET IC 16 PIN	06776	ICN-163-S3-G	1	473042000
XU6	SOCKET IC 14 PIN	06776	ICN-143-S3-G	1	473019000
XU7	SOCKET IC 16 PIN	06776	ICN-163-S3-G	1	473042000
XU8	SOCKET IC 14 PIN	06776	ICN-143-S3-G	1	473019000
XU9	SOCKET IC 16 PIN	06776	ICN-163-S3-G	1	473042000
XU10	SOCKET IC 14 PIN	06776	ICN-143-S3-G	1	473019000
XU11	SOCKET IC 16 PIN	06776	ICN-163-S3-G	1	473042000
XU12	SOCKET IC 14 PIN	06776	ICN-143-S3-G	1	473019000
XU13-14	SOCKET IC 16 PIN	06776	ICN-163-S3-G	2	473042000
XU20	SOCKET IC 14 PIN	06776	ICN-143-S3-G	1	473019000
XU21-24	SOCKET IC 16 PIN	06776	ICN-163-S3-G	4	473042000
Y1	OSC CRYSTAL 10 MHz	27802	CO-251-B16	1	547904000
A11					
08257500A REV: BB PWA '8200-S10' I/O					
C1	CAP EL 100uF 20% 25V	S4217	SM-25-VB-100-M	1	283334000
C2-4	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	3	224268000
DS1-2	LED RED DIFF HLMP-6620	28480	HLMP-6620	2	536027000
J1	CONN M 25 CKT HDR DBL ROW .1CT	06776	NSH-26DB-S2-TG	1	47742228A
J2	CONNECTOR HEADER 2 PIN RT ANG	06383	HPAS156-2-C	1	477365000
J3	CONN F 50 CKT DBL ROW .1CT	32575	102695-3	1	479439000
J4	HEADER 5 PIN RT ANGLE	06383	HPAS156-5-C or D	1	477341000
R1-2	RES NETWORK 3.3K 2% 1.5W 10pin	71450	750-101-R3.3K	2	345030000
U1	IC 74F139 DUAL 1 OF 4 DECODER	07263	74F139PC	1	53448000A
U2-3	IC 82C79P-2 KEYBD/DISP INTERFACE	TOSH	TM82C79P-2	2	53454700A
U4	IC 74HCT04 HEX INVERTER	02736	CD74HCT04E	1	53444213A
XU1	SOCKET IC 16 PIN	06776	ICN-163-S3-G	1	473042000
XU2-3	SOCKET IC 40 PIN	06776	ICN-406-S4-TG	2	473052000
XU4	SOCKET IC 14 PIN	06776	ICN-143-S3-G	1	473019000
A12					
08251800B REV: CB PWA '8200' DISPLAY					
C1-2	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	2	224268000
C3-4	CAP EL 100uF 20% 25V	S4217	SM-25-VB-100-M	2	283334000
C5	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
C6	CAP EL 100uF 20% 25V	S4217	SM-25-VB-100-M	1	283334000
DS1	DISPLAY NUMERIC 5082-7651	28480	5082-7651-S02	1	536811000
DS2	LED LIGHT BAR MOD HLMP-2620	28480	HLMP-2620	1	536027000
DS3-11	DISPLAY NUMERIC 5082-7651	28480	5082-7651-S02	9	536811000
DS12	LED LIGHT BAR MOD HLMP-2620	28480	HLMP-2620	1	536027000
DS13-18	DISPLAY NUMERIC 5082-7651	28480	5082-7651-S02	6	536811000
DS19-20	LED LIGHT BAR MOD HLMP-2620	28480	HLMP-2620	2	536027000
DS21-22	DISPLAY NUMERIC 5082-7651	28480	5082-7651-S02	2	536811000
DS23	LED LIGHT BAR MOD HLMP-2620	28480	HLMP-2620	1	536027000
P1-2	CONNECTOR 20 PIN STRAIGHT	27264	22-03-2201	2	477397000
P3	CONN M 50 CKT HDR DBL ROW .1CT	32575	102692-4	1	477384000
R1-4	RES NETWORK 22 OHM +2 OHM 2W	01121	316B-220	4	345034000

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR. PART NO.	QTY	BEC PART NO.
U1	IC ULN2803A TRANSISTOR ARRAY	56289	ULN2803A	1	534274000
U2	IC 74LS138 DECDR/MPX	01295	SN74LS138N	1	534246000
U3	IC ULN2803A TRANSISTOR ARRAY	56289	ULN2803A	1	534274000
U4	IC 74LS138 DECDR/MPX	01295	SN74LS138N	1	534246000
U5-6	IC 74HCT244	01295	74HCT244	2	534376000
U7-8	IC UDN2585A	56289	UDN2585A	2	534392000
U9	IC ULN2803A TRANSISTOR ARRAY	56289	ULN2803A	1	534274000
U10	IC 74LS138 DECDR/MPX	01295	SN74LS138N	1	534246000
U11	IC ULN2803A TRANSISTOR ARRAY	56289	ULN2803A	1	534274000
U12	IC 74LS138 DECDR/MPX	01295	SN74LS138N	1	534246000
U13-14	IC 74HCT244	01295	74HCT244	2	534376000
U15-16	IC UDN2585A	56289	UDN2585A	2	534392000
U17	IC 74LS138 DECDR/MPX	01295	SN74LS138N	1	534246000
XDS1	SOCKET IC 14 PIN	06776	ICN-143-WB-G	1	473068000
XDS2	SOCKET IC 16 PIN	06776	ICN-163-WB-TG	1	473047000
XDS3-11	SOCKET IC 14 PIN	06776	ICN-143-WB-G	9	473068000
XDS12	SOCKET IC 16 PIN	06776	ICN-163-WB-TG	1	473047000
XDS13-16	SOCKET IC 14 PIN	06776	ICN-143-WB-G	6	473068000
XDS19-20	SOCKET IC 16 PIN	06776	ICN-163-WB-TG	2	473047000
XDS21-22	SOCKET IC 14 PIN	06776	ICN-143-WB-G	2	473068000
XDS23	SOCKET IC 16 PIN	06776	ICN-163-WB-TG	1	473047000
XU1	SOCKET IC 18 PIN	06776	ICN-183-S3-TG	1	473045000
XU3	SOCKET IC 18 PIN	06776	ICN-183-S3-TG	1	473045000
XU5-6	SOCKET IC 20 PIN	06776	ICN-203-S3-G	2	473069000
XU7-9	SOCKET IC 18 PIN	06776	ICN-183-S3-TG	3	473045000
XU11	SOCKET IC 18 PIN	06776	ICN-183-S3-TG	1	473045000
XU13-14	SOCKET IC 20 PIN	06776	ICN-203-S3-G	2	473069000
XU15-16	SOCKET IC 18 PIN	06776	ICN-183-S3-TG	2	473045000
A13					
08251703A REV: A* PWA '8201' KEYBOARD					
J1-2	CONNECTOR 20 PIN	27264	22-02-2205	2	479399000
S1	SWITCH PUSH BUTTON W/LED	31918	200480	1	465293000
S2-3	SWITCH PUSH BUTTON W/O LED	31918	200330	2	465294000
S4-9	SWITCH PUSH BUTTON W/LED	31918	200480	6	465293000
S10-11	SWITCH PUSH BUTTON W/O LED	31918	200330	2	465294000
S12-17	SWITCH PUSH BUTTON W/LED	31918	200480	6	465293000
S19-21	SWITCH PUSH BUTTON W/LED	31918	200480	3	465293000
S22-25	SWITCH PUSH BUTTON W/O LED	31918	200330	4	465294000
S26-28	SWITCH PUSH BUTTON W/LED	31918	200480	3	465293000
S29-32	SWITCH PUSH BUTTON W/O LED	31918	200330	4	465294000
S33-35	SWITCH PUSH BUTTON W/LED	31918	200480	3	465293000
S36-39	SWITCH PUSH BUTTON W/O LED	31918	200330	4	465294000
S40-42	SWITCH PUSH BUTTON W/LED	31918	200480	3	465293000
S44-47	SWITCH PUSH BUTTON W/O LED	31918	200330	4	465294000
S48-50	SWITCH PUSH BUTTON W/LED	31918	200480	3	465293000
S52-55	SWITCH PUSH BUTTON W/O LED	31918	200330	4	465294000
S56-58	SWITCH PUSH BUTTON W/LED	31918	200480	3	465293000
S60-61	SWITCH PUSH BUTTON W/LED	31918	200480	2	465293000

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR. PART NO.	QTY	BEC PART NO.
A23					
08250704A	REV: A*	'8201' REAR PANEL ASSY			
A27	'8220' HEAT SINK ASSY	04901	08250803A	1	08250803A
C3	CAP MICA 680pF 5% 300V	57582	KD16681J301	1	200112000
F1	FUSE 0.75 AMP 250V MDL SLO BLO	54426	MDL-3/4	1	545533000
FL1	FILTER LINE	56289	3JX5421A	1	439004000
J5-9	CONN COAX BNC	54420	UG-625B/U	5	479123000
T1	TRANSFORMER POWER	04901	44609600B	1	44609600B
S2	SWITCH DUAL SLIDE DPDT-DPDT	82389	47206LFR	1	465279000
W9	CABLE ASSY FLAT 24 CKT 14.75 L	04901	92017700A	1	92017700A
W10	CABLE ASSY WIRE 22GA 3C 14.00L	04901	57121701A	1	57121701A
W11	CABLE ASSY COAX RG316/U 22.50L	04901	57223611A	1	57223611A
W12	CABLE ASSY COAX RG316/U 18.25L	04901	57223608A	1	57223608A
W13	CABLE ASSY COAX RG316/U 25.75L	04901	57223610A	1	57223610A
W14	CABLE ASSY COAX RG316/U 28.00L	04901	57223609A	1	57223609A
W15	CABLE ASSY COAX RG316/U 20.25L	04901	57223612A	1	57223612A
W17	CABLE ASSY WIRE 24GA 4C 7.75L	04901	57120100B	1	57120100B
W19-20	CABLE ASSY WIRE 20GA 1C 10.50L	04901	57121801A	2	57121801A
XF1B	FUSE CARRIER GRAY 1/4 x 1-1/4	61935	FEK031.1666	1	482114000
XF1A	FUSE HOLDER	61935	FEU031.1673	1	482117000
A25					
08266500A	REV: AA	'8201' SUB PANEL ASSY			
A12	PWA '8200' DISPLAY	04901	08251800B	1	08251800B
A13	PWA '8201' KEYBOARD	04901	08251703A	1	08251703A
A28	POWER SWITCH ASSY	04901	082531000	1	082531000
C1	CAP MICA 430pF 1% 500V	14655	CD15FD431FD3	1	200037000
C2	CAP MICA 470pF 1% 500V	14655	CD15FD471FD3	1	200060000
J2	CONNECTOR RF FUSE ASSY	04901	082042000	1	082042000
J3	CONNECTOR *SMB* 50 OHM	19505	2019-7511-000	1	477305000
L1	INDUCTOR ASSY 330 uH	04901	400441000	1	400441000
A27					
08250803A	REV: A*	'8220' HEAT SINK ASSY			
A27W2	CABLE ASSY WIRE 24GA 5C 4.50L	04901	57127401A	1	57127401A
A27W3	CABLE ASSY WIRE 24GA 5C 4.50L	04901	57127402A	1	57127402A
A27W4	CABLE ASSY WIRE 24GA 5C 6.50L	04901	57127403A	1	57127403A
C9	CAP TANT 1.0uF 10% 35V ONLY	56289	196D105X9036HA1	1	283216000
C20	CAP CER 0.01uF 20% 500V	33883	BGP Z5U W/FDCL	1	224271000
C26	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	1	224268000
CR1	DIODE BRIDGE 15A 50V	11961	SDA-980-1	1	532030000
L4	IC 323K REGULATOR	27014	LM323K	1	535024000
U5	IC UA7805UC VOLT REG	07263	uA7805UC	1	53511700A
U6	IC UA79M06AUC VOLT REG	07263	uA79M06AUC	1	535093000
U7	IC UA7805UC VOLT REG	07263	uA7805UC	1	53511700A
W18	CABLE ASSY WIRE 22GA 3C 5.00L	04901	57121703A	1	57121703A

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR PART NO.	QTY	BEC PART NO.
XU4	SOCKET TRANSISTOR PWR TO-3	06778	MP-3452G	1	47308000A
A28					
082531000 REV: CA '8200' POWER SWITCH ASSY					
J1	CONN COAX BNC	54420	UG-625B/U	1	479123000
S1	SWITCH ROCKER DPDT	13812	572-2121-0103-010	1	466288000
W16	CABLE ASSY WIRE 24GA 4C 16.15L	04901	57120000B	1	57120000B
A3, OPTION					
08254200A REV: AA '8200' CALIBRATOR ASSY					
C6	CAP FT 1000pF 20% 500V	59660	2499-003-X5S0102M	1	227105000
J10	CONNECTOR TYPE "N"	24253	4889	1	47945500A
04313101A REV: A* PWA '4300' 50 MHz GENERATOR; Model: 4200A,S17					
AR1	IC 301A OP AMP	27014	LM301AN	1	535012000
C1	CAP CER 470pF 10% 500V	33883	TYPE JF	1	224219000
C2	CAP MICA 100pF 5% 300V	20307	DM5-FC101J	1	205008000
C3	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	1	283338000
C4	CAP VAR CER 3.5-18pF 250V	91293	9373	1	281011000
C5	CAP CER 1000pF 10% 800V	16546	CE-102	1	224310000
C7	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	1	283338000
C8	CAP CER 0.01uF 100V	33883	BT Z5U	1	224119000
C9	CAP MICA 36pF 5% 300V	14655	CD5EC360J	1	205003000
C10	CAP MICA 200pF 5% 100V	14655	CD5FA201J	1	205024000
C11	CAP MICA 10pF 5% 300V	14655	CD5WCC100J	1	205002000
C12	CAP VAR CER 3.5-18pF 250V	91293	9373	1	281011000
CR1-2	DIODE HSCH1001 (1N6263)	28480	HSCH-1001	2	530174000
CR3	DIODE MV-1650	04713	MV1650	1	530762000
L1	INDUCTOR 4.7uH 10%	24226	10/471	1	400384000
L2	INDUCTOR 0.56uH 10%	24226	10/560	1	400382000
L3	INDUCTOR 0.033uH 10%	04901	400388000	1	400388000
Q1	TRANS NPN 2N3604	04713	2N3604	1	528071000
R1	RES MF 1.50K 1% 1/4W	19701	5043ED1K500F	1	341317000
R2-3	RES MF 100K 1% 1/4W	19701	5043ED100K0F	2	341500000
R4	RES VAR 1K 10% 0.5W	32997	3299X-1-102	1	311410000
R6	RES MF 100K 1% 1/4W	19701	5043ED100K0F	1	341500000
R7	RES MF 2.43K 1% 1/4W	19701	RN55D-2431-F	1	341337000
R8-9	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	2	341300000
R10	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	1	341400000
R11	RES MF 5.11K 1% 1/4W	19701	5043ED5K110F	1	341368000
R12	RES MF 1.21K 1% 1/4W	19701	5043ED1K210F	1	341308000
R13	RES MF 1.30K 1% 1/4W	19701	5043ED1K300F	1	341311000
R14	RES MF 75.0 OHM 1% 1/4W	19701	5043ED75R00F	1	341184000
R15	RES MF 50.00 OHM 0.1% 1/4W	64537	PME55-T9	1	325818000
U1	IC AD581JH VOLT REF	51640	AD581JH	1	535053000

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR PART NO.	QTY	BEC PART NO.
A15, OPTION					
08262400A REV: AB PWA '8220' FILTER OPTION					
C1	CAP MPC 0.022uF 2% 50V	14752	652A-1-A223G	1	234188000
C2-3	CAP EL 10uF 20% 25V	84217	SM-25-VB-10-M	2	283338000
C4	CAP EL 100uF 20% 25V	84217	SM-25-VB-101M	1	283334000
CR1-2	DIODE SIG 1N914	01295	1N914	2	530058000
CR3-4	DIODE SIG FDH-300	07263	FDH300	2	530052000
J1-2	CONNECTOR "SMB"	19505	209	2	477317000
J3	CONN M 09 CKT ST POLZ .1CT	06383	HPSS100-9-C	1	477374000
L1-3	INDUCTOR 5.6uH 10%	24226	15/561	3	400308000
P11-40	SOCKET SPRING COMPONENT LEAD	32575	1-332070-7	30	479333000
R1	RES MF 1.00M 1% 1/4W	19701	5043ED1M000F	1	341600000
R2	RES MF 600 OHM 0.25% 1/8W	84537	PME55-T9	1	324215000
R3	RES MF 475K 1% 1/4W	19701	5043ED475K0F	1	341565000
R4	RES NETWORK 3.3K 2% 0.5W 6pin	71450	750-61-R3.3K	1	34504500A
R5	RES VAR 2K 10% 0.5W	73138	72XWR2K	1	311347000
R6	RES MF 1.00K 1% 1/4W	19701	5043ED1K000F	1	341300000
R7	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	1	341400000
R8	RES VAR 2K 10% 0.5W	73138	72XWR2K	1	311347000
R9	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	1	341400000
R10	RES VAR 2K 10% 0.5W	73138	72XWR2K	1	311347000
R11	RES MF 9.31K 1% 1/4W	19701	5043ED9K310F	1	341383000
R12	RES MF 15.0K 1% 1/4W	19701	5043ED15K00F	1	341417000
R13	RES VAR 2K 10% 0.5W	73138	72XWR2K	1	311347000
R14	RES MF 4.87K 1% 1/4W	19701	5043ED4K870F	1	341388000
R15	RES MF 4.02K 1% 1/4W	19701	5043ED4K020F	1	341358000
R16	RES MF 2.00K 1% 1/4W	19701	5043ED2K000F	1	341329000
R17	RES MF 9.09K 1% 1/4W	19701	5043ED9K090F	1	341392000
U1	IC 74HCT273	01295	SN74HCT273N	1	534377000
U2	IC PEEL PROG FILTER OPT '8220'	04901	53458700A	1	53458700A
U3	IC 6208 4 CHAN DIF MULTPXR	32293	IH6208CPE	1	534288000
U4	IC 356P OP AMP	04713	LF356N	1	535040000
XU1-2	SOCKET IC 20 PIN	06776	ICN-203-S3-G	2	473065000
XU3	SOCKET IC 16 PIN	06776	ICN-163-S3-G	1	473042000
XU4	SOCKET IC 8 PIN	06776	ICN-083-S3-G	1	473041000
97403101A REV: A- OPT AUDIO LOOP-THRU, -07 OPTION					
A15	PWA '8220' FILTER OPTION	04901	08262400A	1	08262400A
J11-12	CONN COAX BNC	54420	UG-625B/U	2	479123000
W16	CABLE COAXIAL ASSY (BLUE)	04901	57223616A	1	57223616A
W17	CABLE COAXIAL ASSY (YELLOW)	04901	57223617A	1	57223617A

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR PART NO.	QTY	BEC PART NO.
11204000A REV: AA PWA CCITT BANDPASS FILTER, -03 OPTION					
C1	CAP MPC 0.01uF 2% 50V	14752	652A-1A-103G	1	234142000
C2	CAP MICA 1000pF 5% 100V	14655	CD15FA102J	1	200506000
C3-4	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	2	224268000
C5-6	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	2	283336000
C7	CAP MPC 0.01uF 2% 50V	14752	652A-1A-103G	1	234142000
C8	CAP MPC 0.0047uF 2% 50V	14752	652A-1-A472G	1	23417300A
C9	CAP MPC 0.1uF 2% 50V	14752	652A-1-A-104G	1	234139000
C10	CAP MICA 560pF 1% 300V	14655	CD15FC561F	1	200091000
C11	CAP MPC 0.047uF 2% 50V	14752	652A-1-A473G	1	234144000
C12	CAP MPC 0.022uF 2% 50V	14752	652A-1-A223G	1	234168000
C13	CAP MPC 0.047uF 2% 50V	14752	652A-1-A473G	1	234144000
C14-16	CAP MPC 0.1uF 2% 50V	14752	652A-1-A-104G	3	234139000
J1-10	TERMINAL .040 OD .270 LG .062M	98291	229-1071-230	10	510038000
R1	RES MF 23.2K 1% 1/4W	19701	5043ED23K20F	1	34143500A
R2	RES MF 15.0K 1% 1/4W	19701	5043ED15K00F	1	341417000
R3	RES MF 1.15K 1% 1/4W	19701	5043ED1K150F	1	341306000
R4	RES MF 2.15K 1% 1/4W	19701	5043ED2K150F	1	341332000
R5	RES MF 26.1K 1% 1/4W	19701	5043ED26K10F	1	341440000
R6	RES MF 9.09K 1% 1/4W	19701	5043ED9K090F	1	341392000
R7	RES MF 6.04K 1% 1/4W	19701	5043ED6K040F	1	341375000
R8	RES MF 5.62K 1% 1/4W	19701	5043ED5K620F	1	341372000
R9	RES MF 6.04K 1% 1/4W	19701	5043ED6K040F	1	341375000
R10	RES MF 4.53K 1% 1/4W	19701	5043ED4K530F	1	341363000
R11	RES MF 100 OHM 1% 1/4W	19701	5043ED100R0F	1	341200000
R12	RES MF 26.1K 1% 1/4W	19701	5043ED26K10F	1	341440000
R13	RES MF 14.3K 1% 1/4W	19701	5043ED14K30F	1	341415000
R14	RES MF 1.10K 1% 1/4W	19701	5043ED1K100F	1	341304000
R15	RES MF 5.76K 1% 1/4W	19701	5043ED5K760F	1	341373000
U1-2	IC 5532A DUAL OP AMP 8 DIP	01206	NE5532AP	2	53512100A
XU1-2	SOCKET IC 8 PIN	06776	ICN-063-S3-G	2	473041000
11203700A REV: BA PWA CCIR WGHTING FILTER, -08 OPTION					
C1	CAP MICA 1500pF 1% 100V	57582	SD15-152F101	1	20013100A
C2	CAP MPC 0.0047uF 1% 50V	14752	652A-1A-472F	1	23418100A
C3	CAP MICA 1500pF 1% 100V	57582	SD15-152F101	1	20013100A
C4-5	CAP MPC 0.0047uF 1% 50V	14752	652A-1A-472F	2	23418100A
C6-8	CAP MICA 1500pF 1% 100V	57582	SD15-152F101	3	20013100A
C9-10	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	2	224268000
C11-12	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	2	283336000
J1-10	TERMINAL .040 OD .270 LG .062M	98291	229-1071-230	10	510038000
R1	RES MF 10.0K 1% 1/4W	19701	5043ED10K00F	1	341400000
R2	RES MF 5.62K 1% 1/4W	19701	5043ED5K620F	1	341372000
R3	RES MF 27.4K 1% 1/4W	19701	5043ED27K40F	1	341442000
R4-5	RES MF 5.62K 1% 1/4W	19701	5043ED5K620F	2	341372000

TABLE 7-2. Model 8201 Parts List Continued.

REFERENCE DESIGNATOR	DESCRIPTION	FED. CODE	MFGR PART NO.	QTY	BEC PART NO.
R6	RES MF 392 OHM 1% 1/4W	19701	5043ED392R0F	1	341257000
R7-9	RES MF 5.62K 1% 1/4W	19701	5043ED5K820F	3	341372000
R10	RES MF 20.0K 1% 1/4W	19701	5043ED20K00F	1	341429000
R11	RES VAR 2K 10% 0.5W	73138	72XWR2K	1	311347000
U1-2	IC 5532A DUAL OP AMP 8 DIP	01295	NE5532AP	2	53512100A
XU1-2	SOCKET IC 8 PIN	06776	ICN-083-S3-G	2	473041000
11207000A REV: BB PWA C-MSG FILTER, -09 OPTION					
C1-4	CAP MPC 0.022uF 2% 50V	14752	652A-1-A223G	4	234166000
C5-8	CAP MPC 0.0022uF 2% 50V	14752	653A-1-A222G	4	234165000
C9-10	CAP CER 0.1uF 20% 50V	04222	SR215E104MAA	2	224268000
C11-12	CAP EL 10uF 20% 25V	S4217	SM-25-VB-10-M	2	283336000
C13	CAP MPC 0.22uF 2% 50V	14752	652A-1-A224G	1	234167000
J1-10	TERMINAL .040 OD .270 LG .062M	98291	229-1071-230	10	510039000
R1	RES MF 20.0K 1% 1/4W	19701	5043ED20K00F	1	341429000
R2	RES MF 33.2K 1% 1/4W	19701	5043ED33K20F	1	341450000
R3	RES MF 3.32K 1% 1/4W	19701	5043ED3K320F	1	341350000
R4	RES MF 19.1K 1% 1/4W	19701	5043ED19K10F	1	341427000
R5	RES MF 8.25K 1% 1/4W	19701	5043ED8K250F	1	341388000
R6	RES MF 95.3K 1% 1/4W	19701	5043ED95K30F	1	341494000
R7	RES MF 3.85K 1% 1/4W	19701	5043ED3K850F	1	341354000
R8	RES MF 110K 1% 1/4W	19701	5043ED110K0F	1	341504000
R9	RES MF 13.3K 1% 1/4W	19701	5043ED13K30F	1	341412000
U1-2	IC 5532A DUAL OP AMP 8 DIP	01295	NE5532AP	2	53512100A
XU1-2	SOCKET IC 8 PIN	06776	ICN-083-S3-G	2	473041000

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SECTION VIII SCHEMATIC DIAGRAMS

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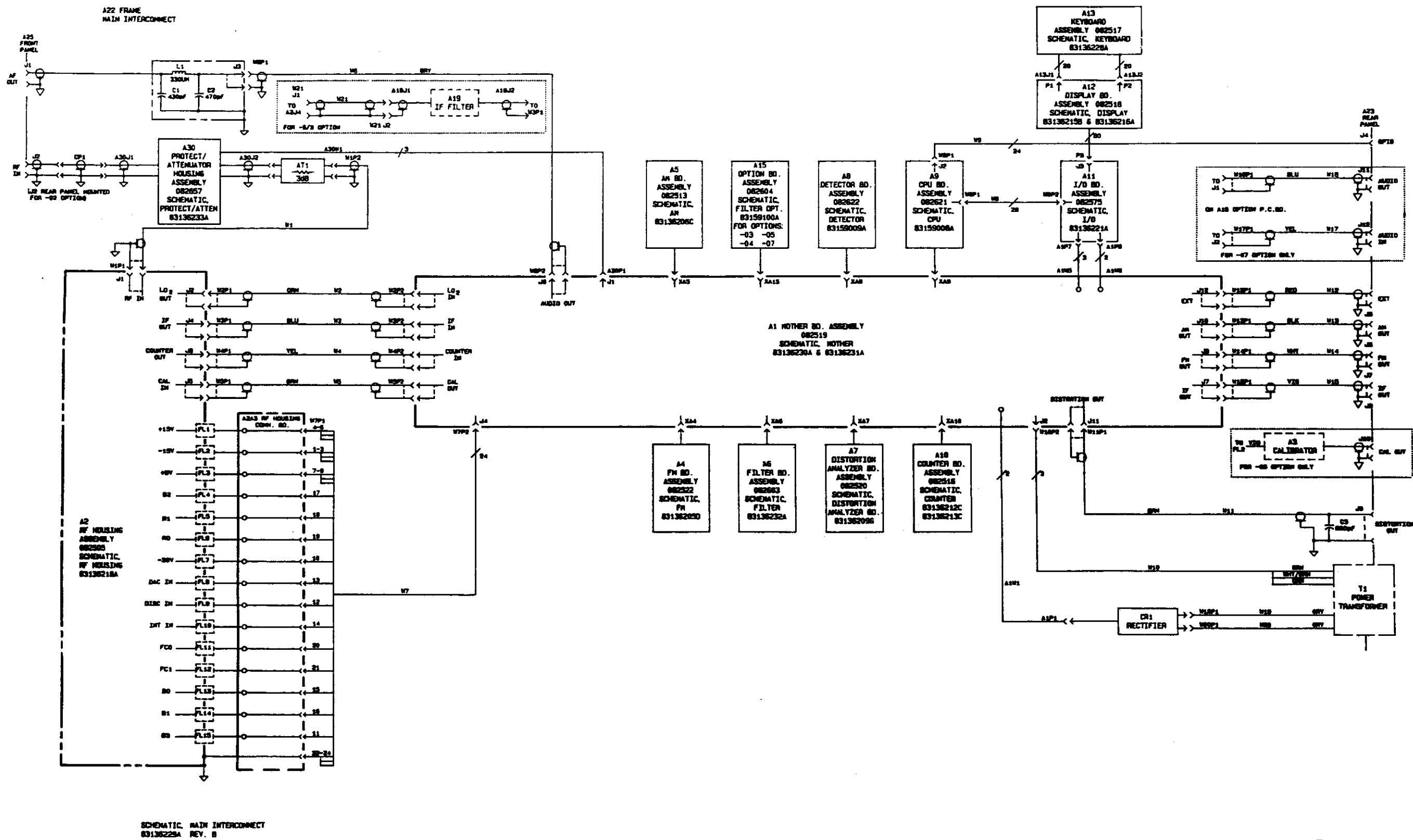
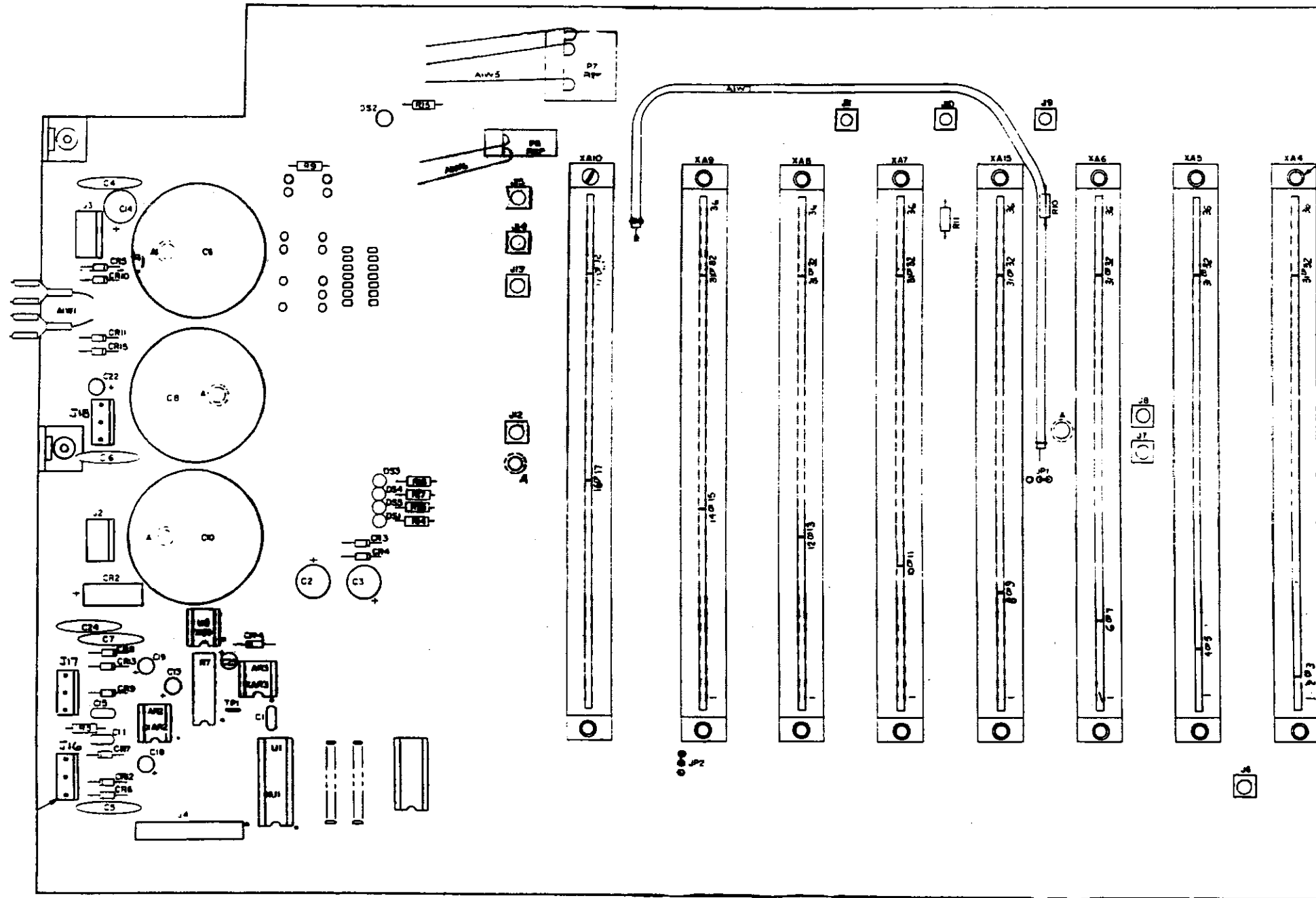


Figure 8-1. Main Frame Schematic.



082519A SHT. 3

Figure 8-2. Mother Board A1, Parts Location.

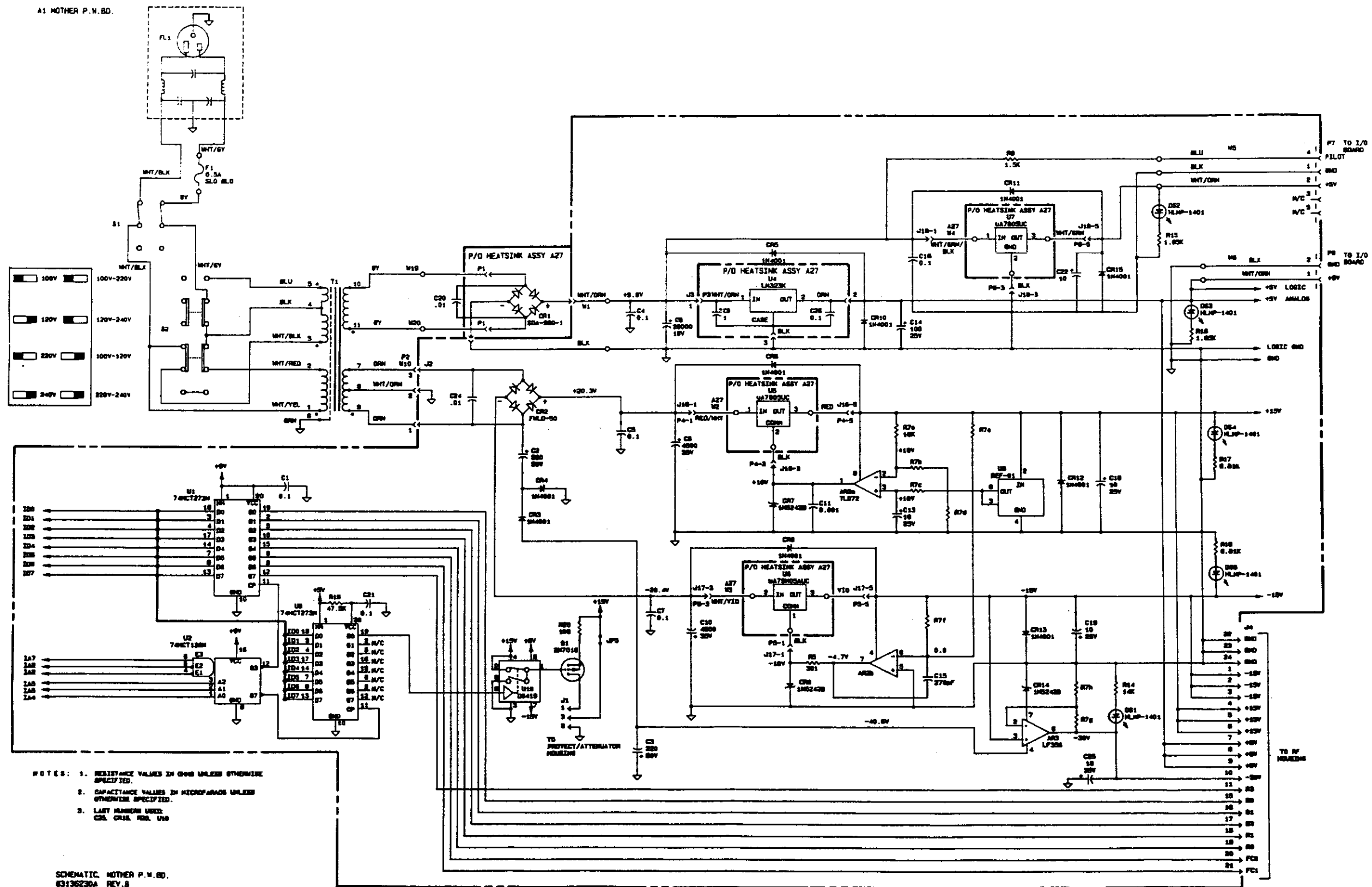


Figure 8-3. Motherboard A1, Schematic Diagram Sheet 1.

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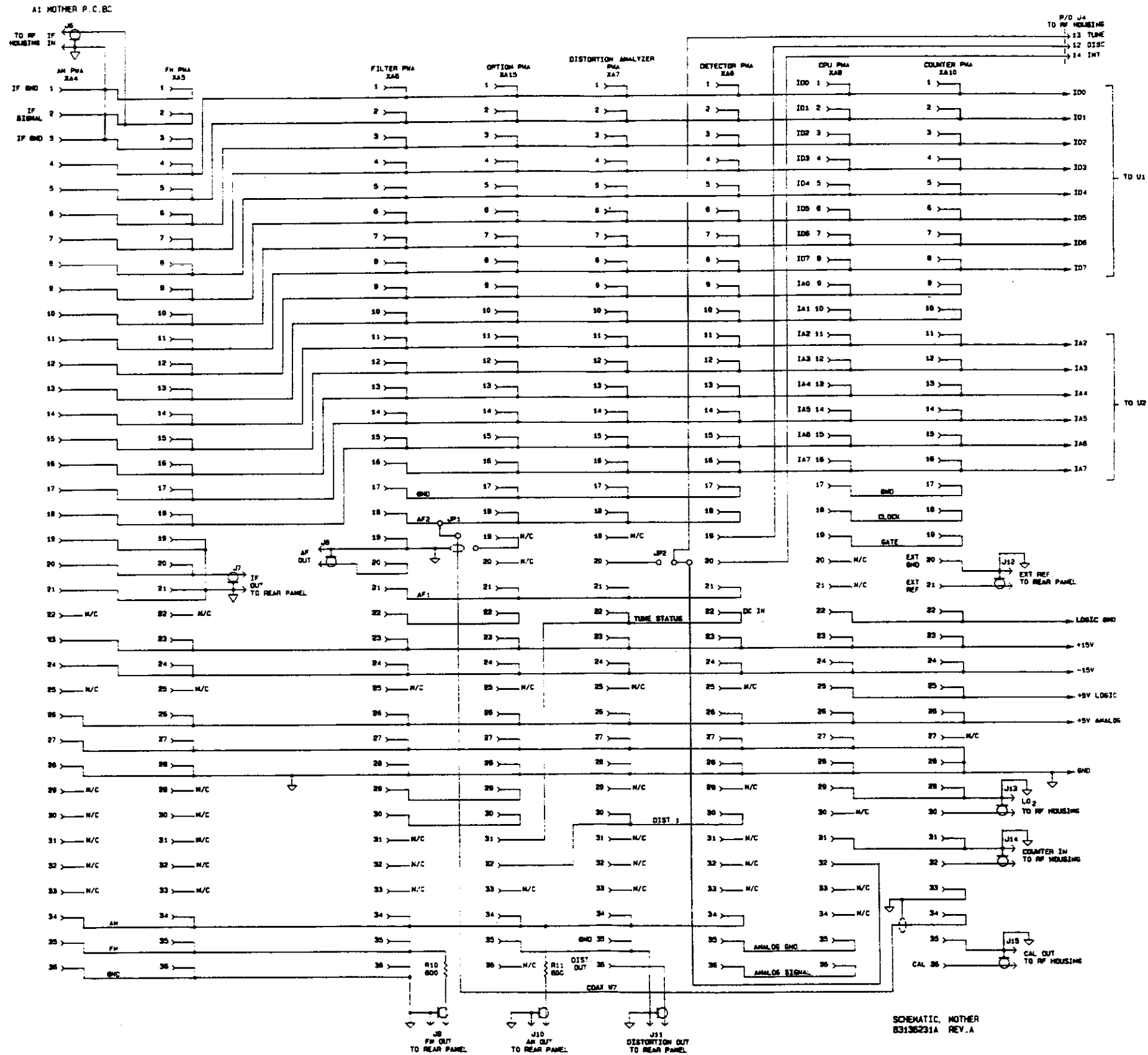


Figure 8-4. Motherboard A1, Schematic Diagram Sheet 2.

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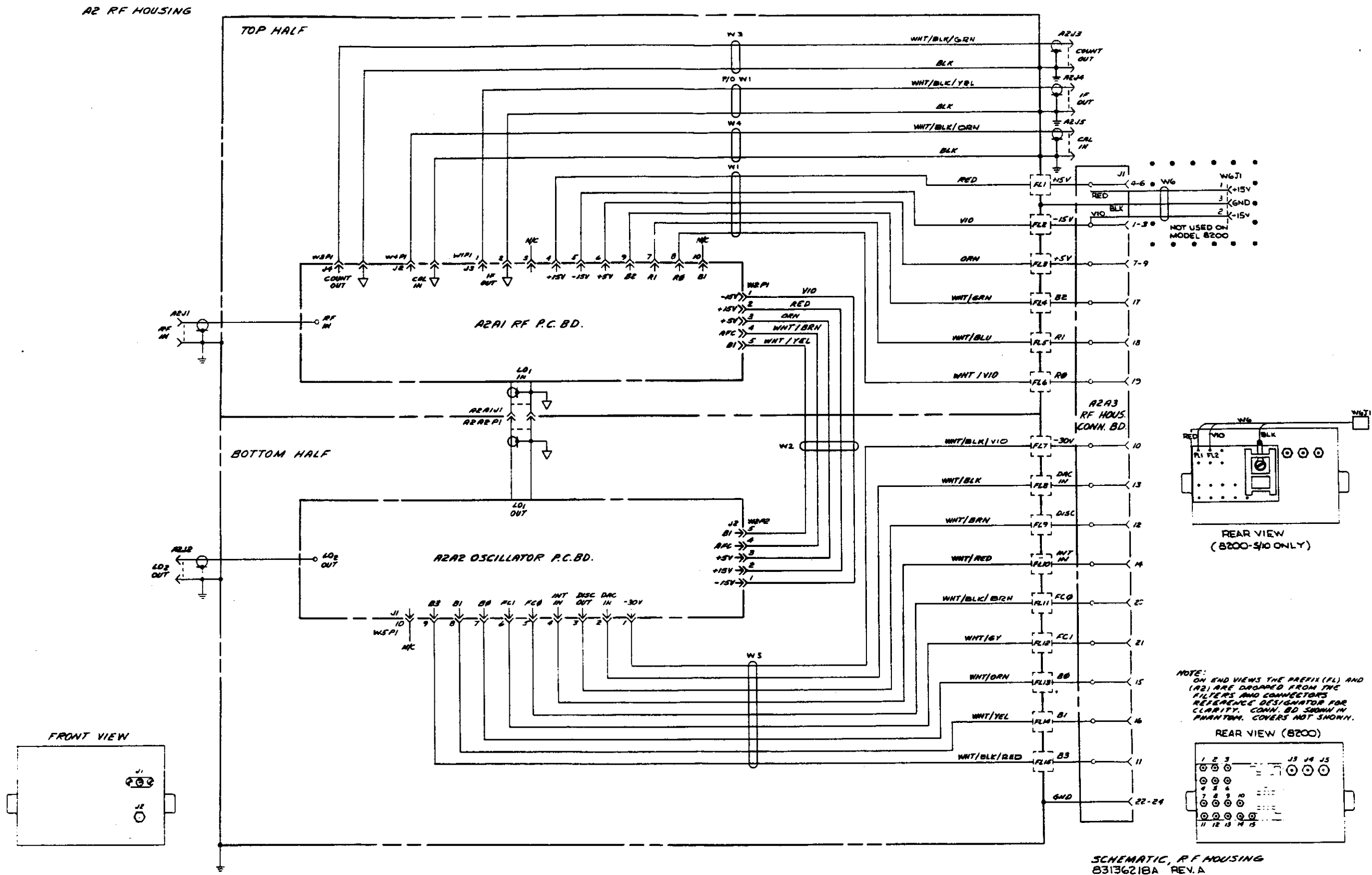
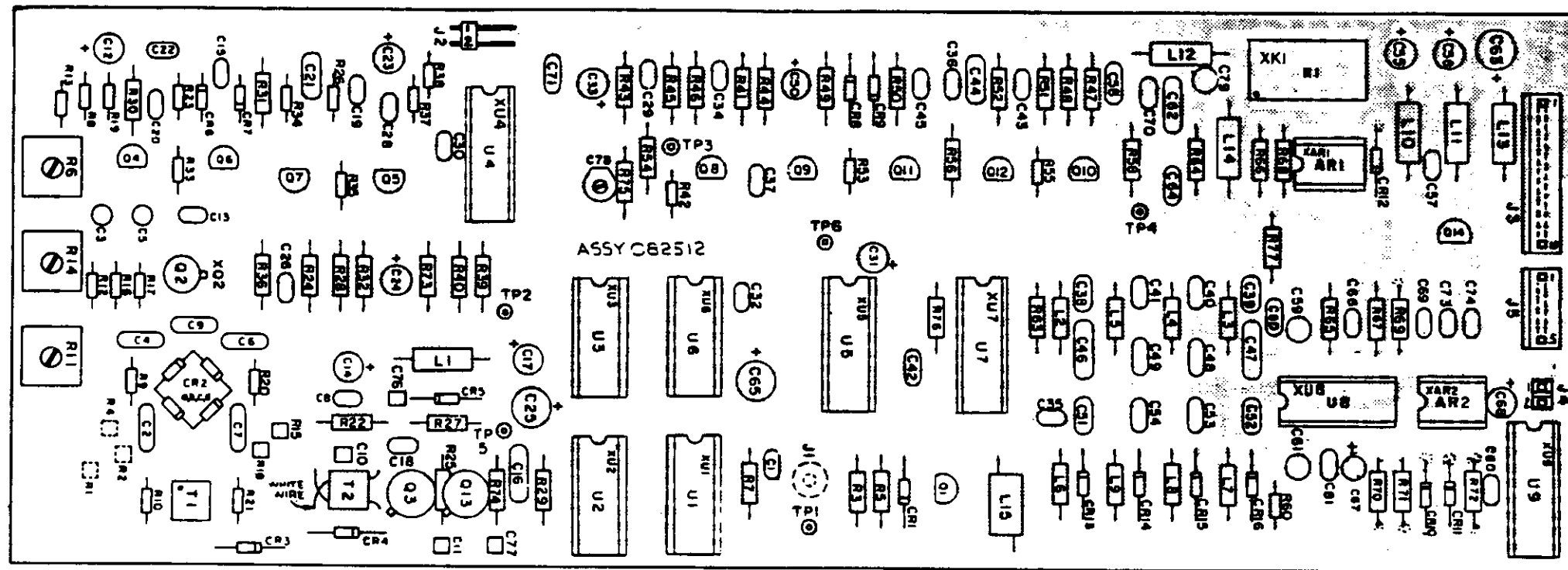


Figure 8-5. RF Housing A2, Schematic Diagram.



082512F

Figure 8-6. RF Board A2A1, Parts Location.

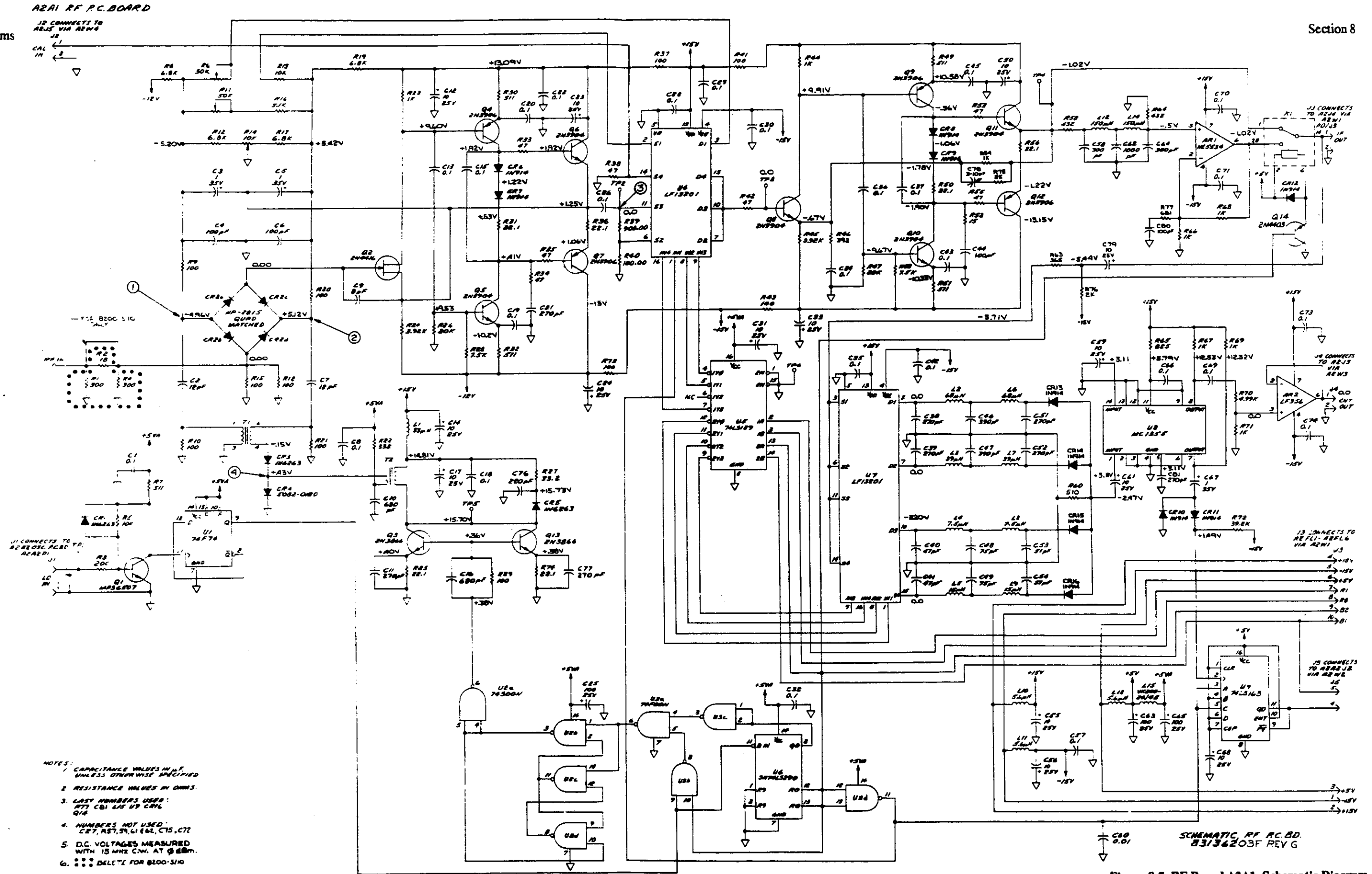
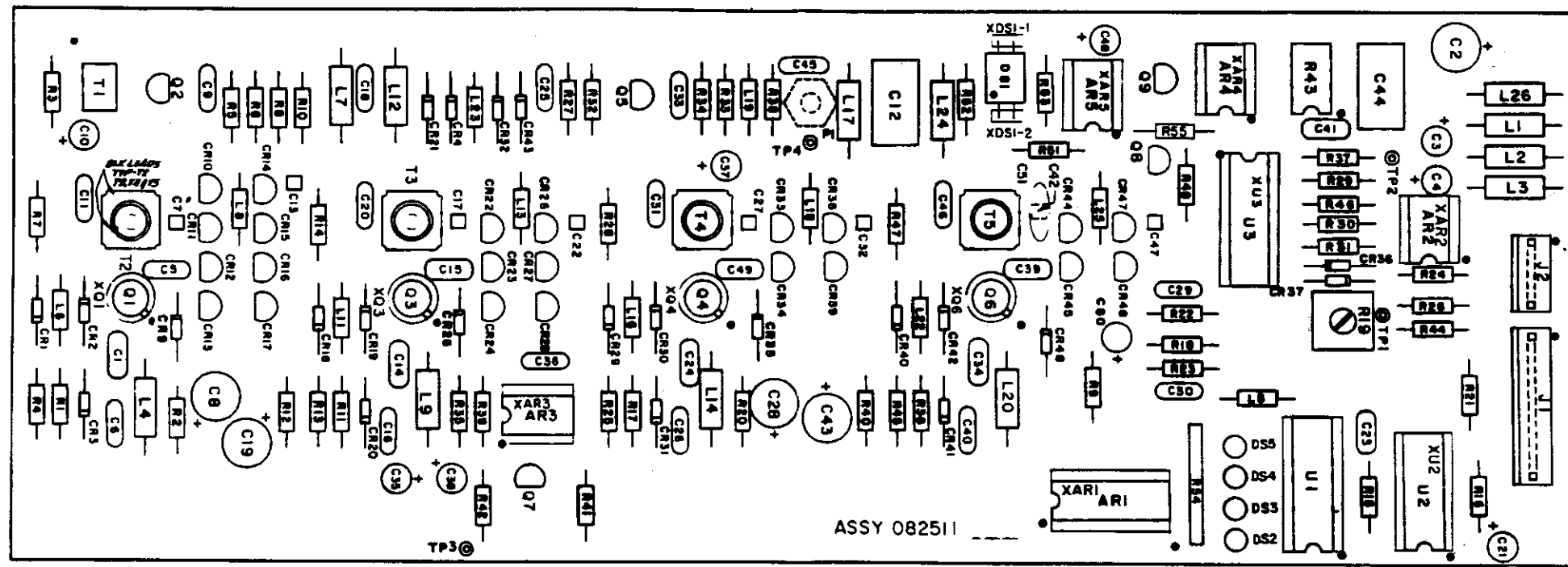


Figure 8-7. RF Board A2A1, Schematic Diagram.



082511C

Figure 8-8. Oscillator Board A2A2, Parts Location.

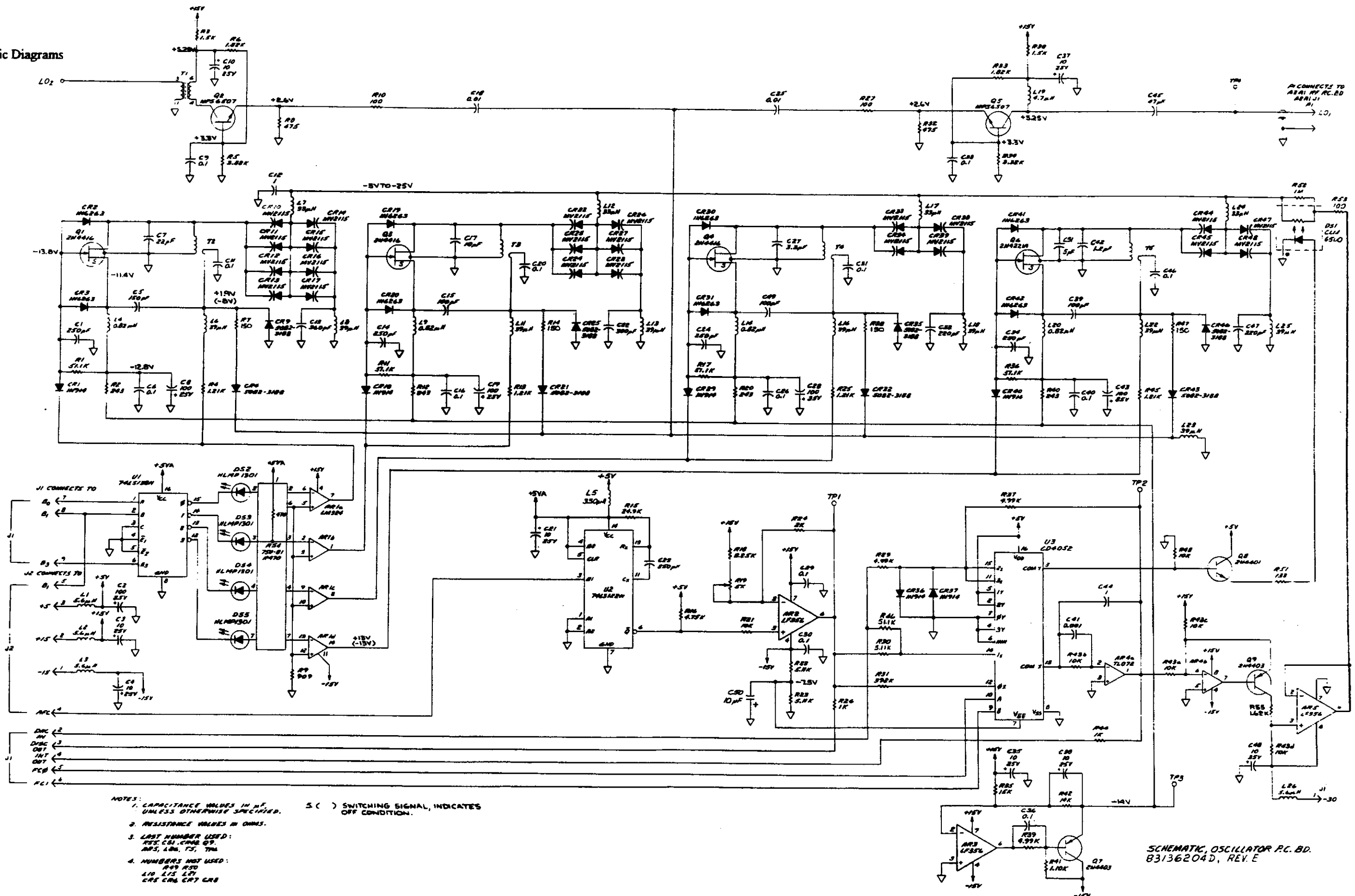


Figure 8-9. Oscillator Board A2A2, Schematic Diagram.

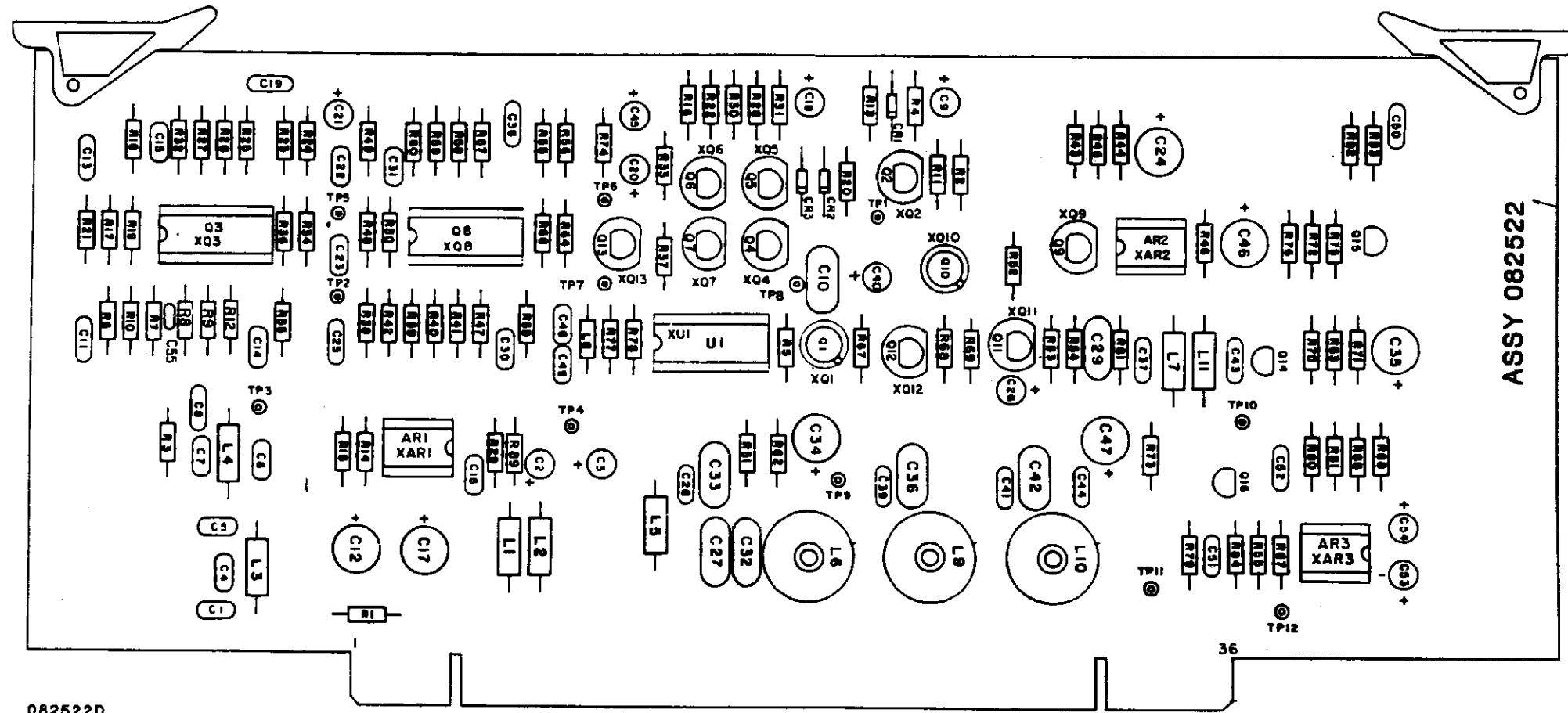
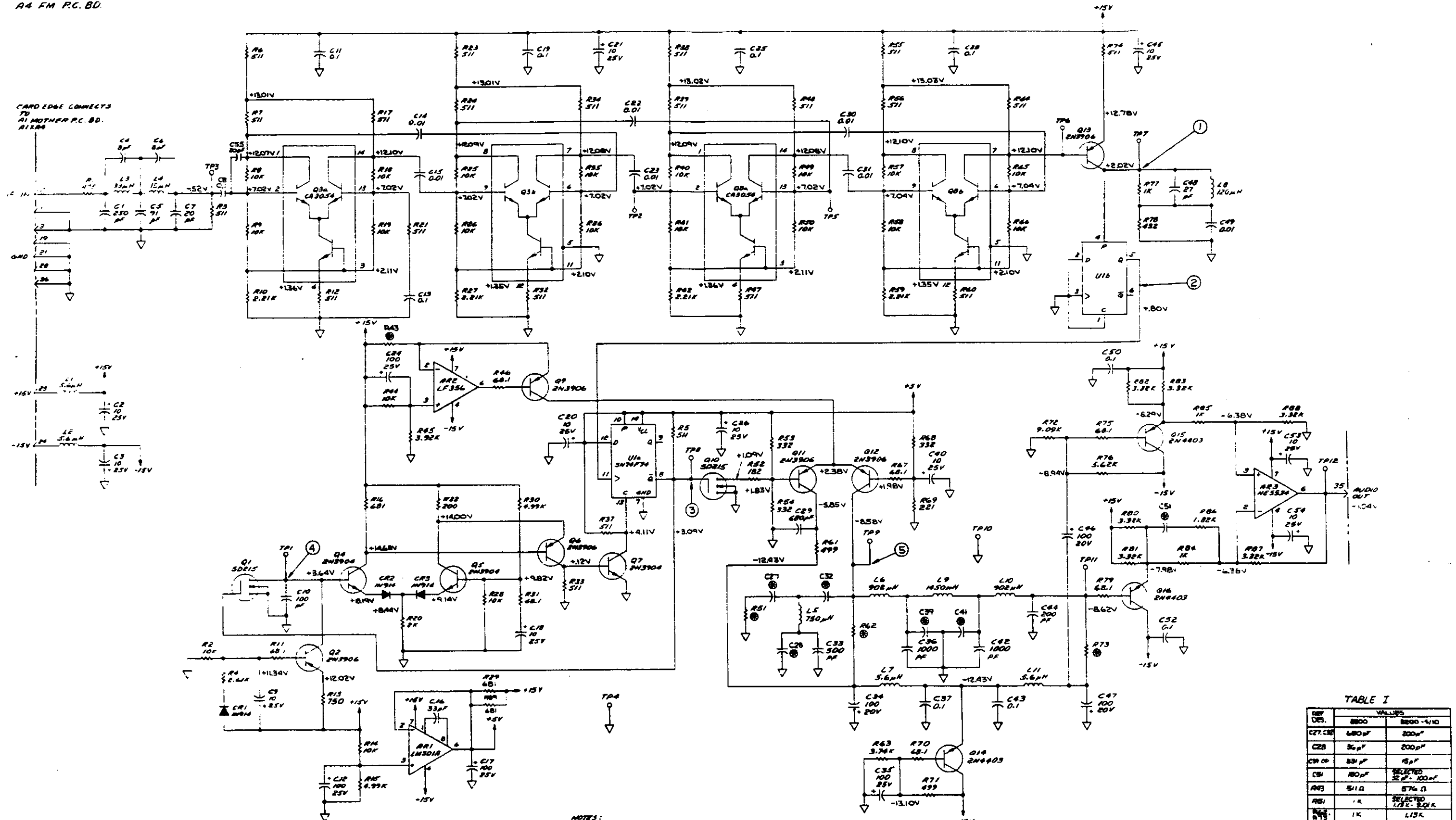


Figure 8-10. FM Board A4, Parts Location.

A4 FM P.C. BD.



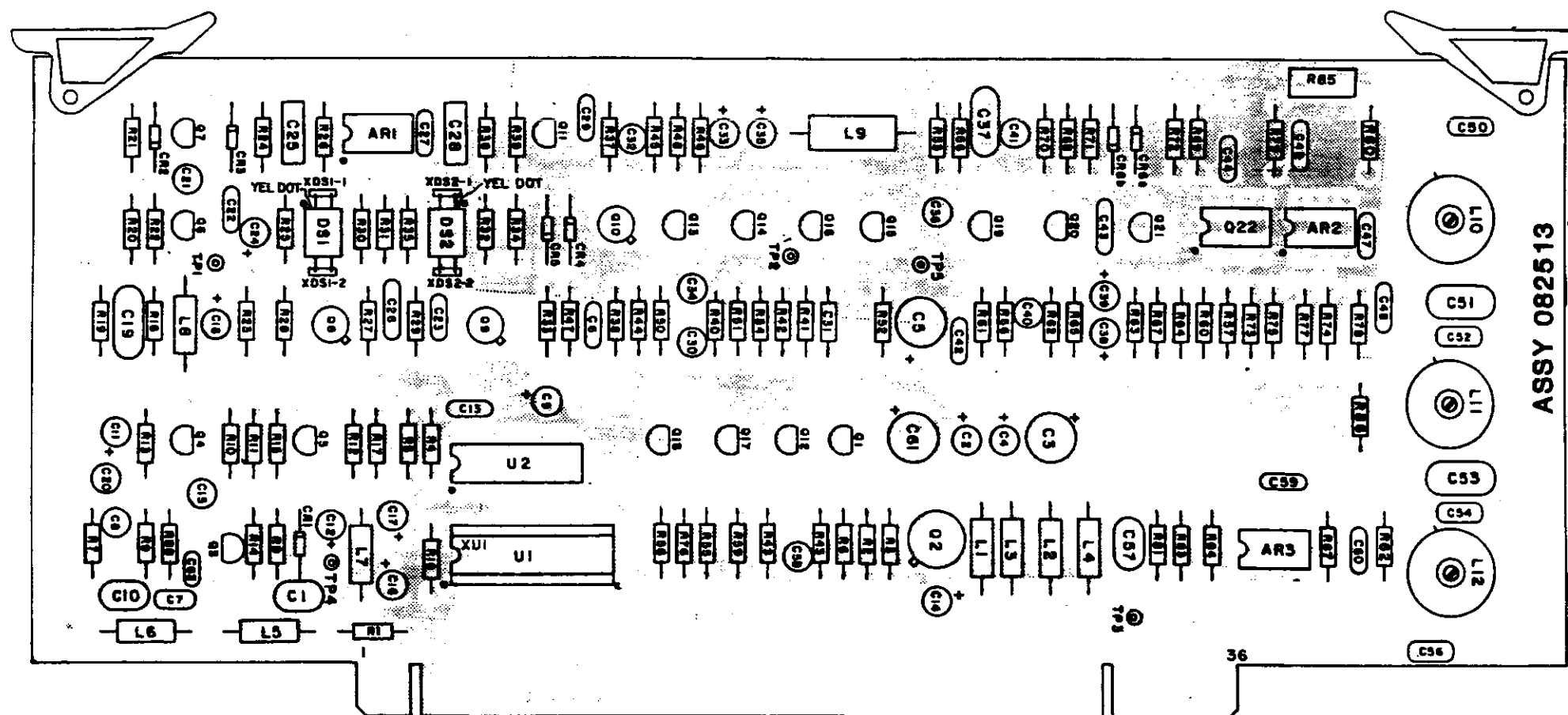
- NOTES:
1. CAPACITANCE VALUES IN μ F, UNLESS OTHERWISE SPECIFIED.
 2. RESISTANCE VALUES IN OHMS.
 3. LAST NUMBERS USED: R89, C50, Q16, TP18, L11
 4. D.C. MEASUREMENTS MADE WITH 15 MHz C.W. AT 0.48.50 MHz DEV. AT 1 kHz RATE.
 5. \odot SEE TABLE I FOR VALUES.

TABLE I

REF. DES.	VALUES	
C27, C36	680 pF	200 pF
C28	30 pF	200 pF
C39, C40	33 pF	45 pF
C51	100 pF	SELECTED 50 pF - 100 pF
R43	51 Ω	57 Ω
R41	1 K	SELECTED 1.15 K - 1.50 K
R42, R73	1 K	1.15 K

SCHEMATIC, FM P.C. 83136205D REV. F

Figure 8-11. FM Board A4, Schematic Diagram.

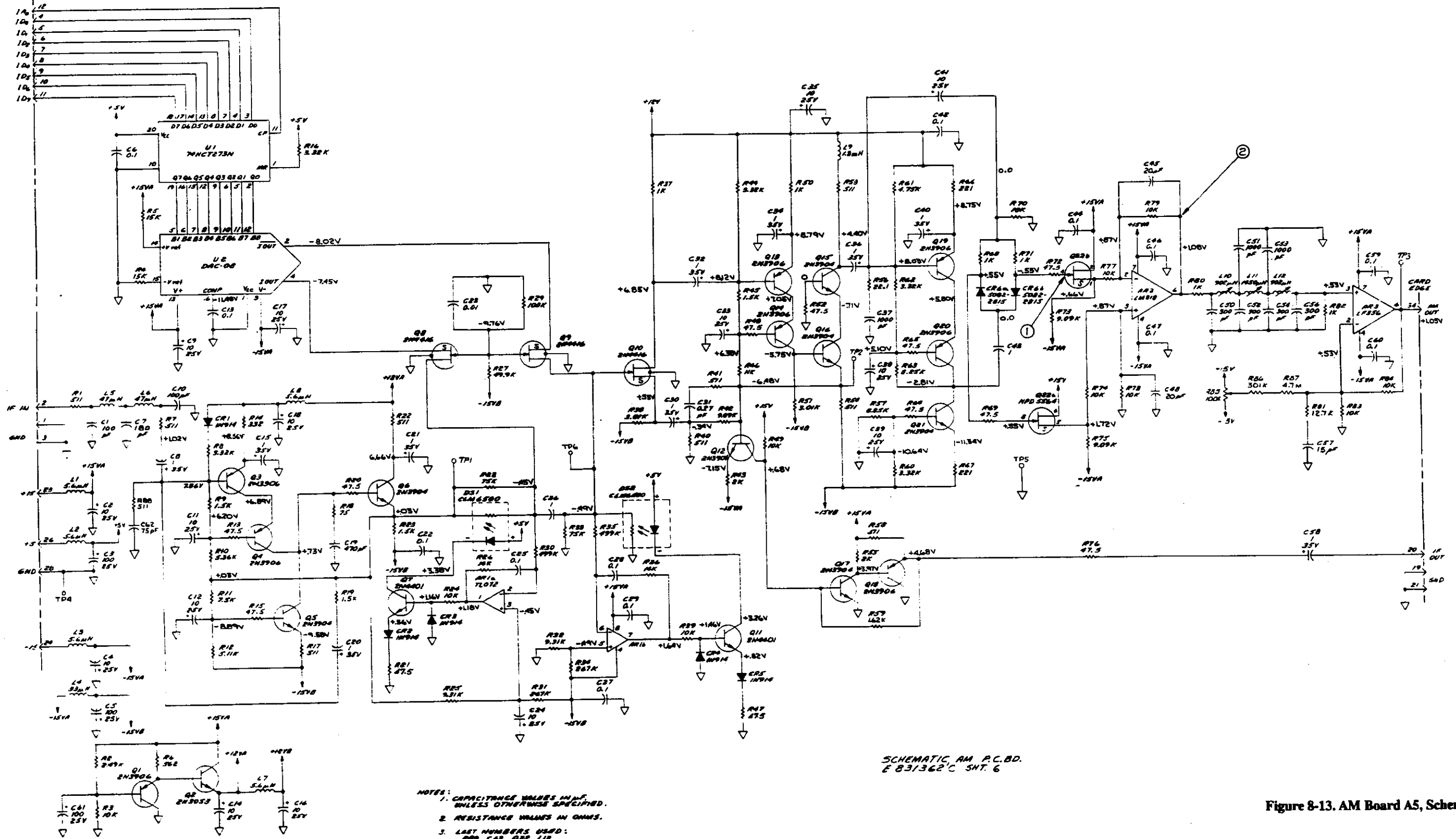


082513B

Figure 8-12. AM Board A5, Parts Location.

AS AM P.C. BD.

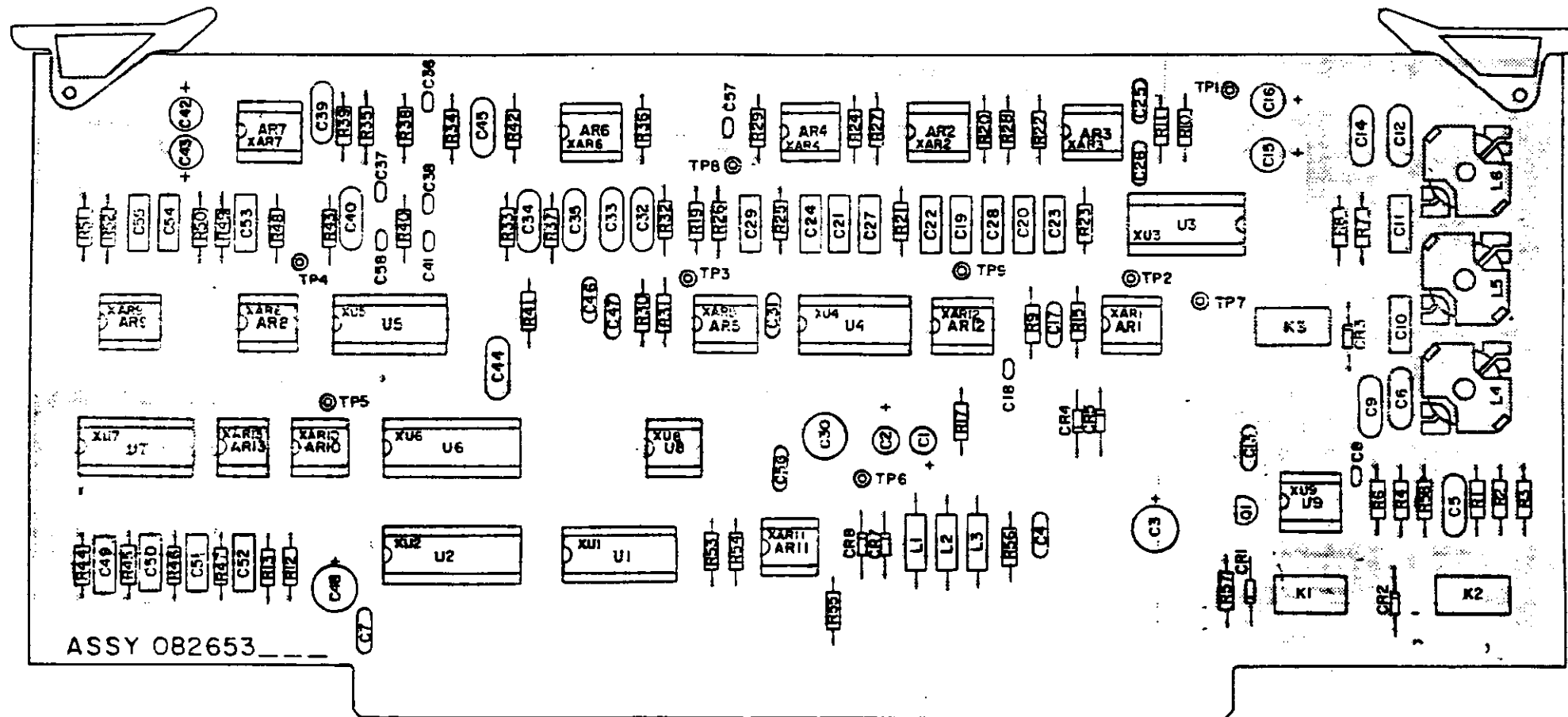
CARD EDGE CONNECTS TO ANOTHER P.C. BOARD



SCHMATIC AM P.C. BD.
E 831362 C SMT. 6

- NOTES:
1. CAPACITANCE VALUES IN P.F. UNLESS OTHERWISE SPECIFIED.
 2. RESISTANCE VALUES IN OHMS.
 3. LAST NUMBERS USED:
R85 C48 Q85 L18
 4. DC MEASUREMENTS MADE WITH 15 MHz C.M. AT 0.4B, 50% AM AT 1 MHz RATE

Figure 8-13. AM Board A5, Schematic Diagram.



082653 A

Figure 8-14. Filter Board A6, Parts Location.

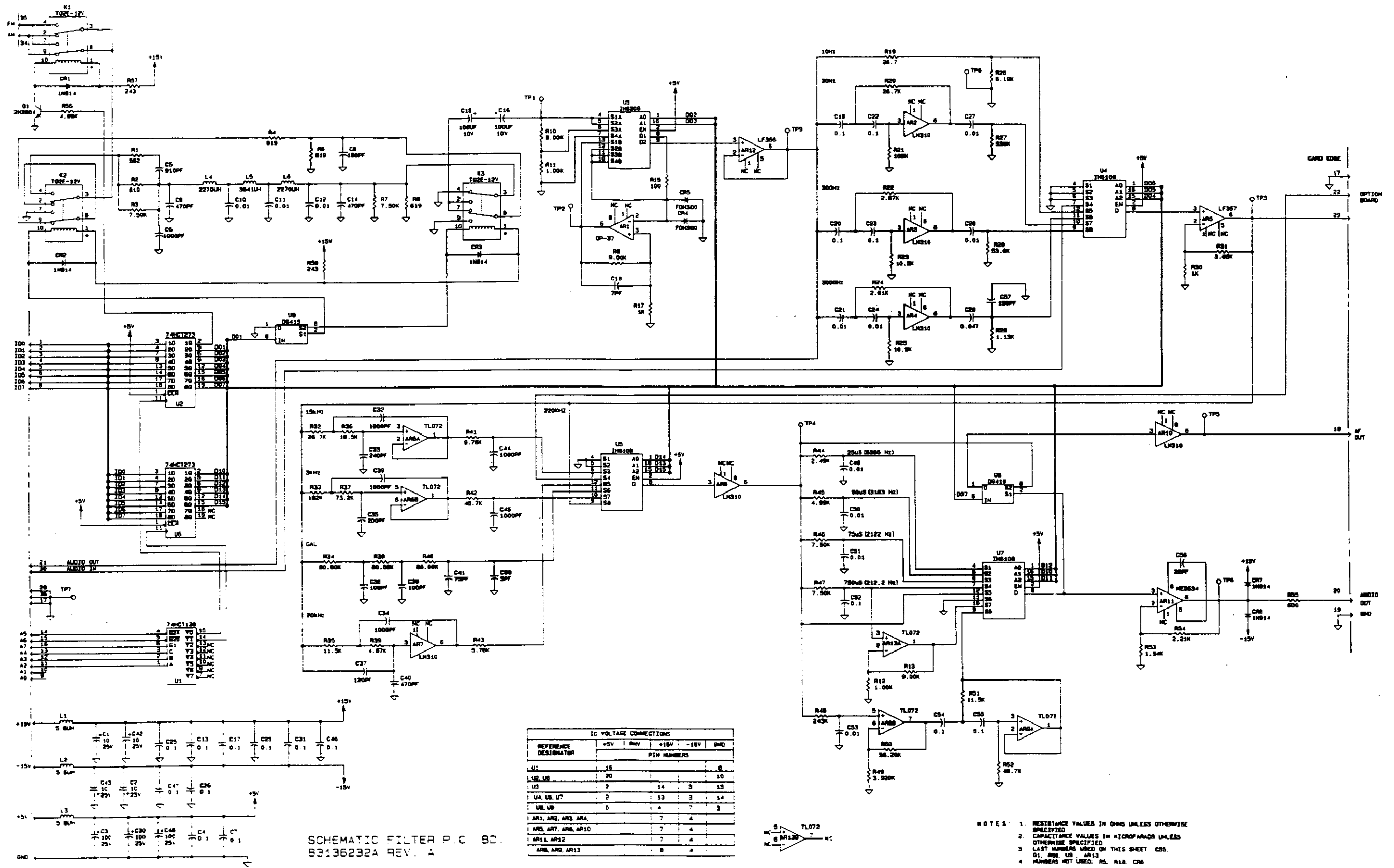
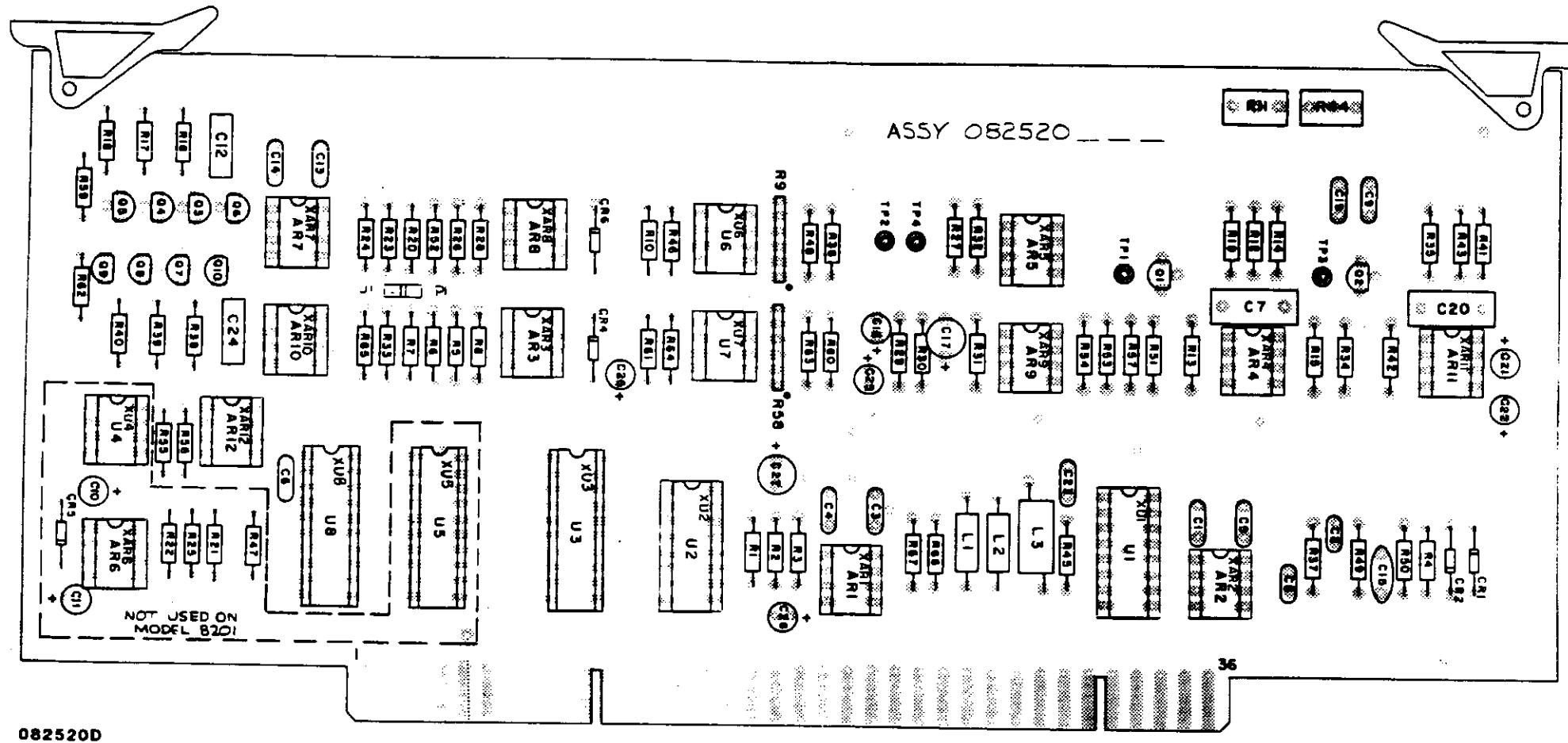
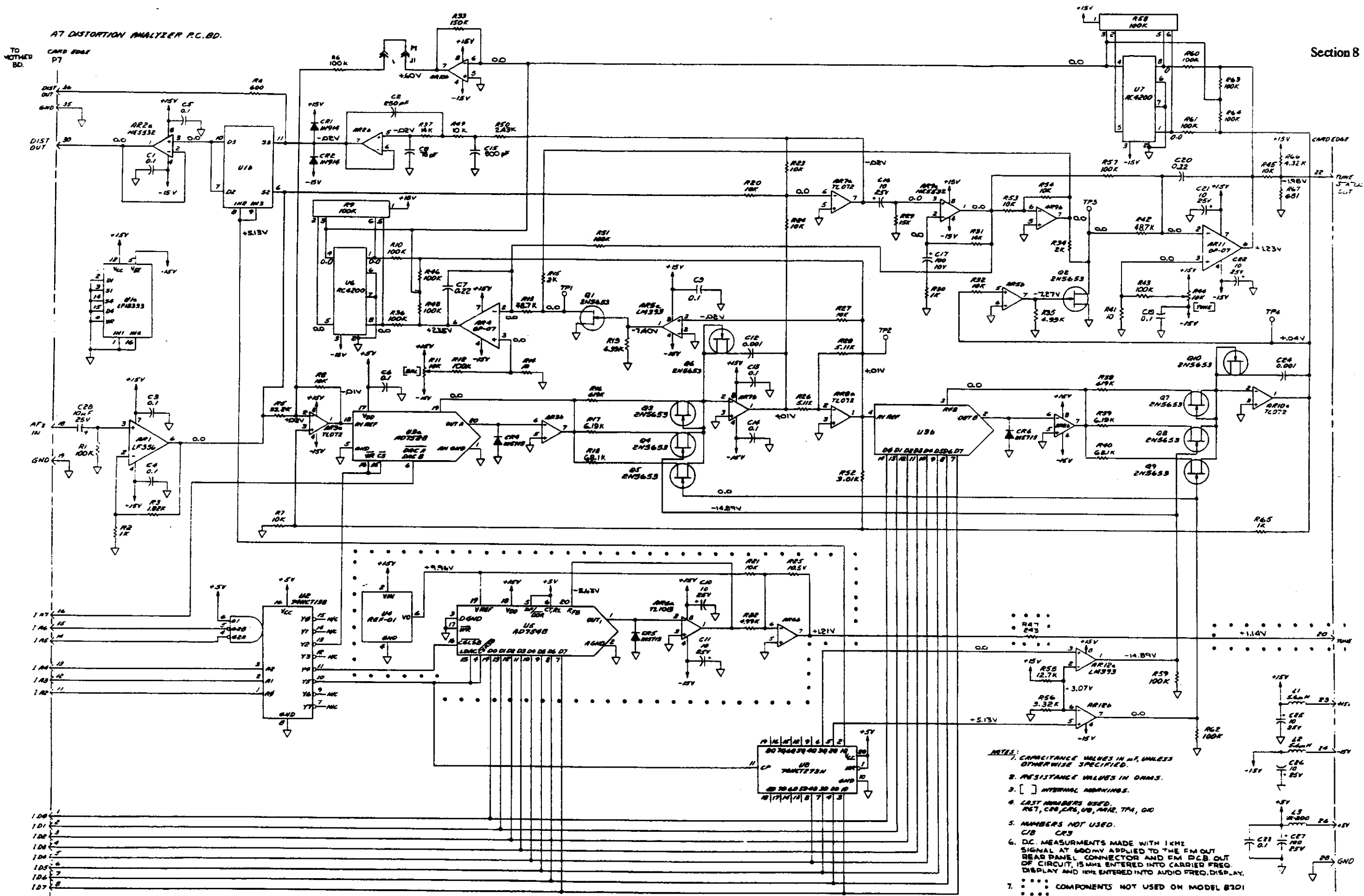


Figure 8-15. Filter Board A6, Schematic Diagram.



NOTE:
1. MARK FINAL ASSY PART NUMBER WITH 1/8 HIGH BLACK CHARACTERS.
REFER TO MANUFACTURING ORDER FOR COMPLETE PART NUMBER

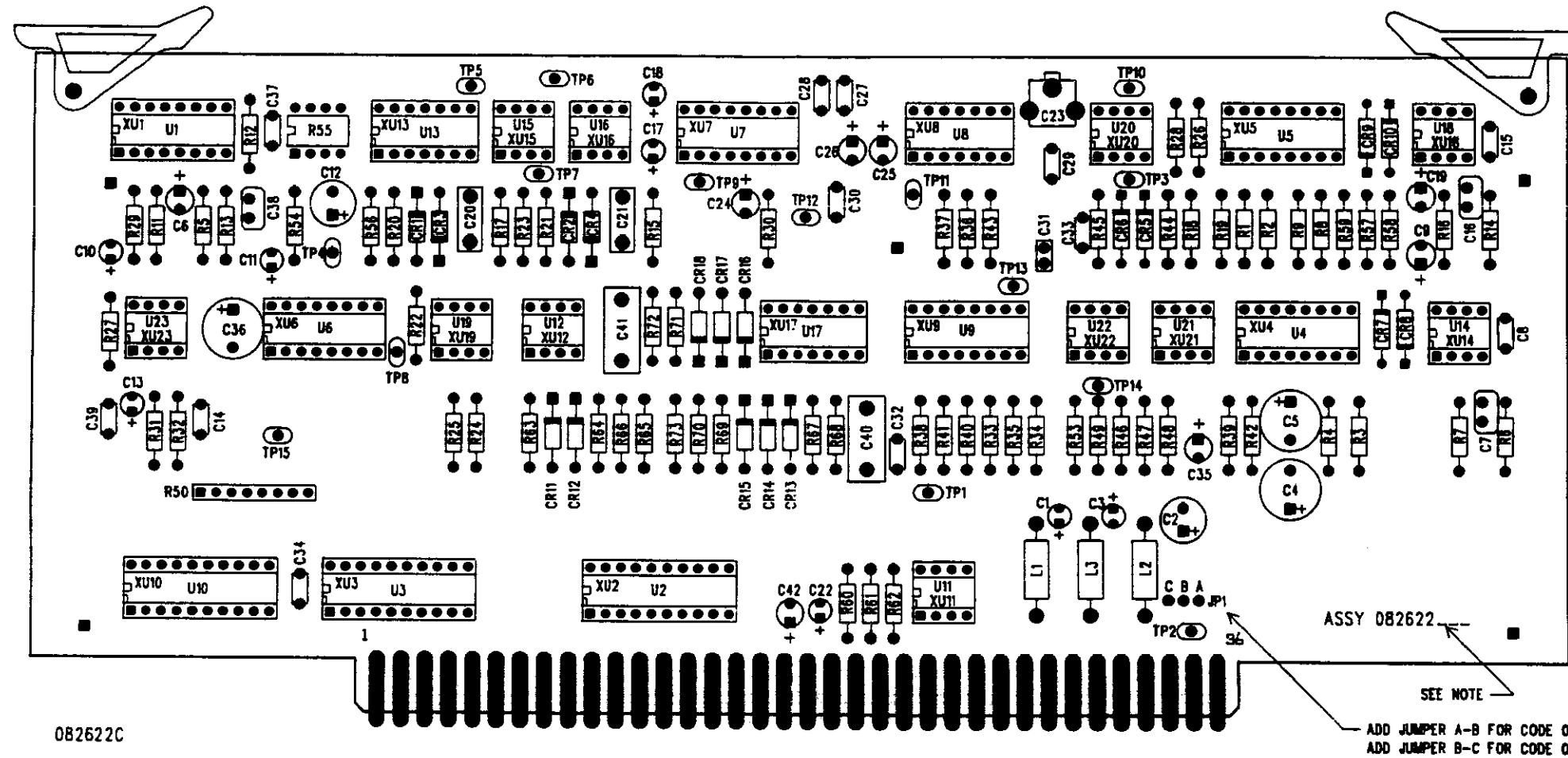
Figure 8-16. Distortion Analyzer, A7 Parts Location.



SCHEMATIC, DISTORTION ANALYZER P.C. BD.
83136209G REV. H1

- NOTES:
1. CAPACITANCE VALUES IN μ F, UNLESS OTHERWISE SPECIFIED.
 2. RESISTANCE VALUES IN OHMS.
 3. [] INTERNAL MARKINGS.
 4. PART NUMBERS USED: RET, C28, C25, U36, AR12, TP4, Q10
 5. NUMBERS NOT USED: C/B, C/S
 6. DC MEASUREMENTS MADE WITH 1KHZ SIGNAL AT 600MV APPLIED TO THE FM OUT REAR PANEL CONNECTOR AND FM PCB OUT OF CIRCUIT, 15KHZ ENTERED INTO CARRIER FREQ. DISPLAY AND 10KHZ ENTERED INTO AUDIO FREQ. DISPLAY.
 7. COMPONENTS NOT USED ON MODEL 8701

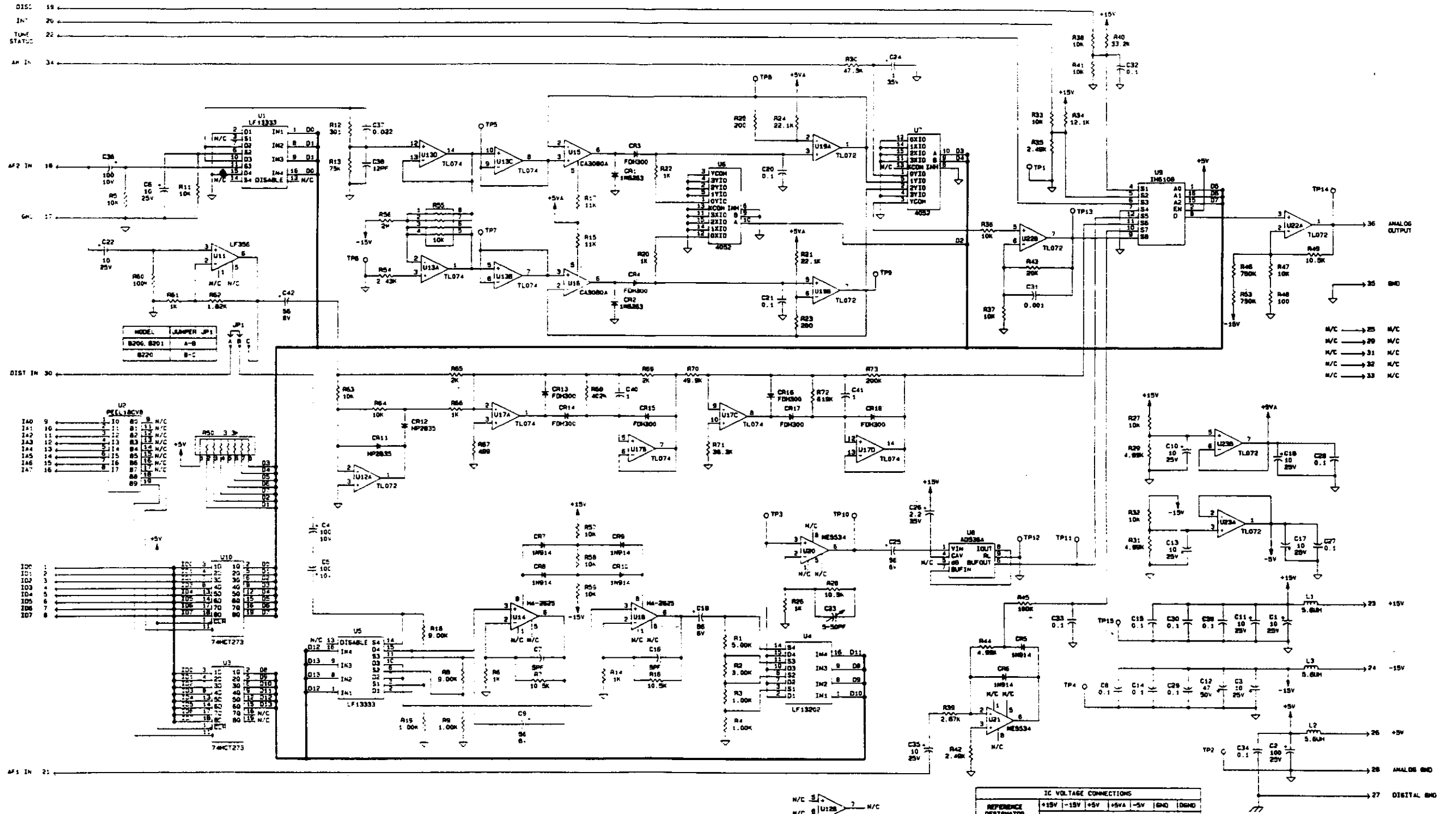
Figure 8-17. Distortion Analyzer, A7 Schematic Diagram.



082622C

BEC CODE	MODEL	REMARKS
00C	COMMON ASSY	
01A	B201	ADD APPROPRIATE JUMPER (JP1)
02A	B220	ADD APPROPRIATE JUMPER (JP1)

Figure 8-18. Detector Board A8, Parts Location.

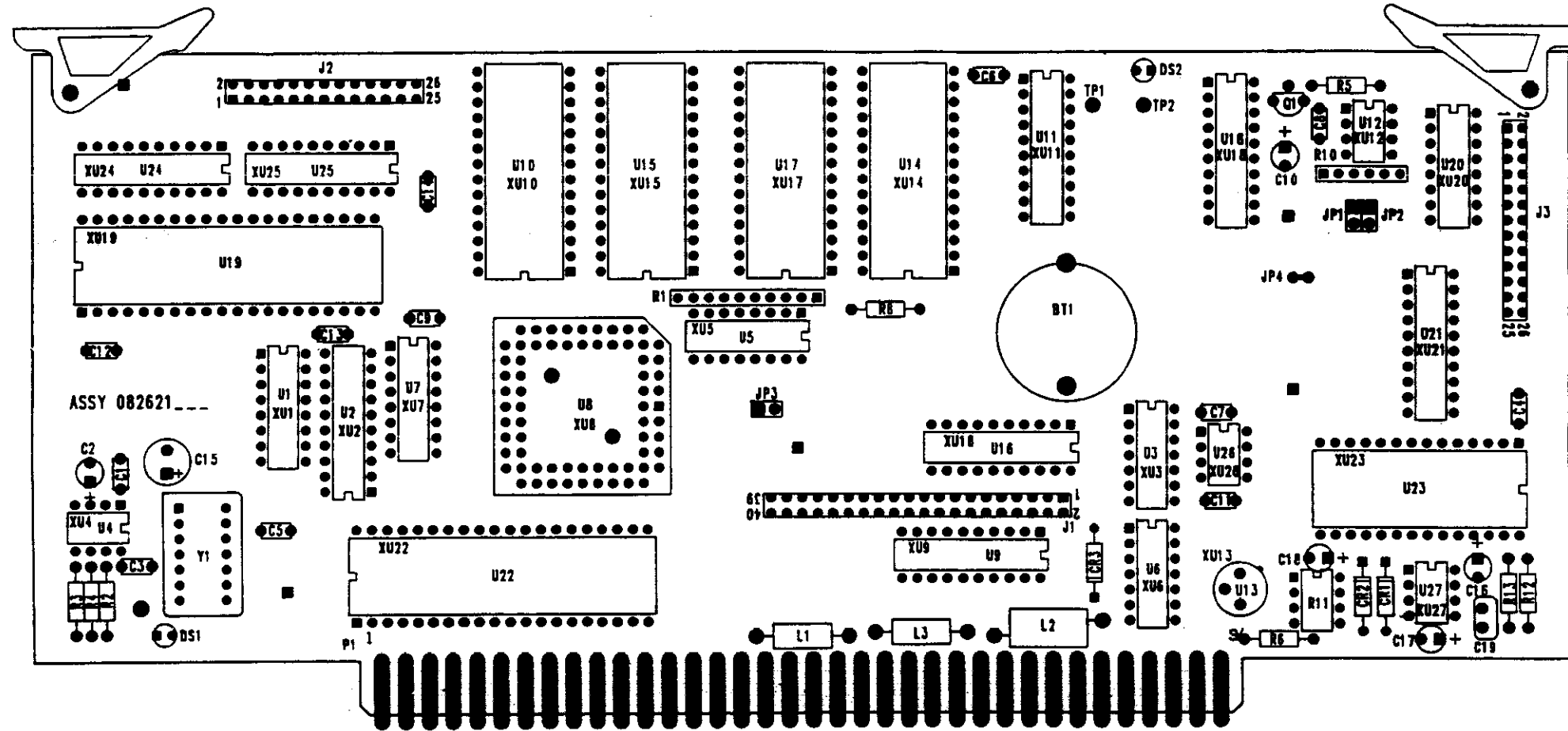


SCHEMATIC: 8220 DETECTOR PWB
83159009A REV C

- NOTES
1. ALL RESISTOR VALUES IN OHMS
 2. ALL CAPACITOR VALUES IN UF UNLESS OTHERWISE SPECIFIED
 3. LAST NUMBERS USED: C42 CR18 JP1 L3 R73 U23 TP15
 4. NUMBERS NOT USED: R10 R31 R32

REFERENCE DESIGNATOR	+15V	-15V	+5V	+5VA	-5V	GND	DEMO
PIN NUMBERS							
U1, 5	12	5				4	
U11, 14, 18, 20, 21	7	4					
U13, 17	4	11					
U15, 18			7	4			
U16, 7			16	7	8		
U19			8	4			
U19	13	3			14		
U12, 22, 23	8	4					
U2, 3, 10					20		10
U19	14	3			10		
U4	13	4			5		

Figure 8-19. Detector Board A8, Schematic Diagram.



082621B

PART NUMBER	MODEL	REMARKS
08262100A	8220	U10 & U14 ARE VARIABLE
08262101A	8201	

Figure 8-20. CPU Board A9, Parts Location.

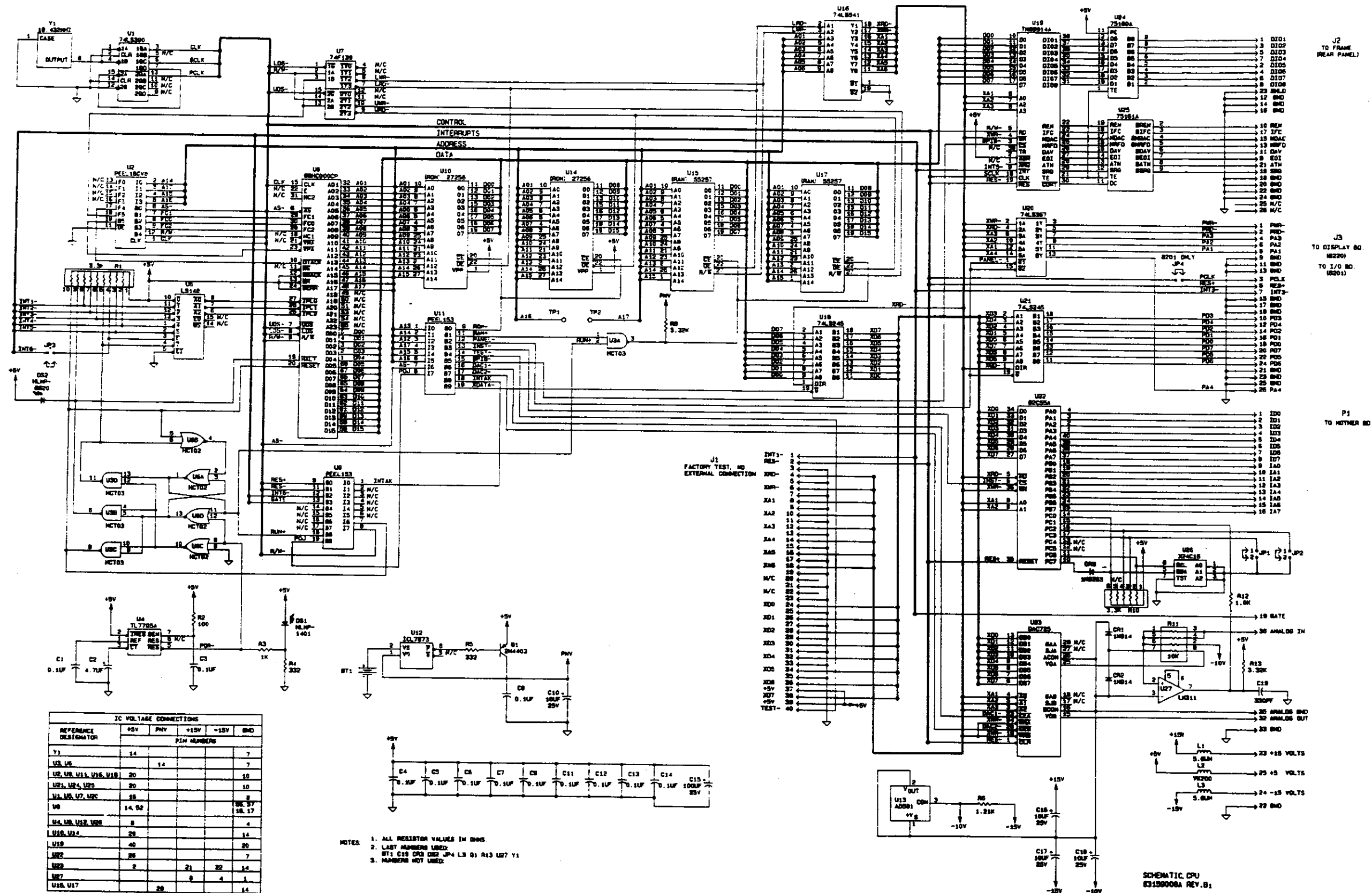
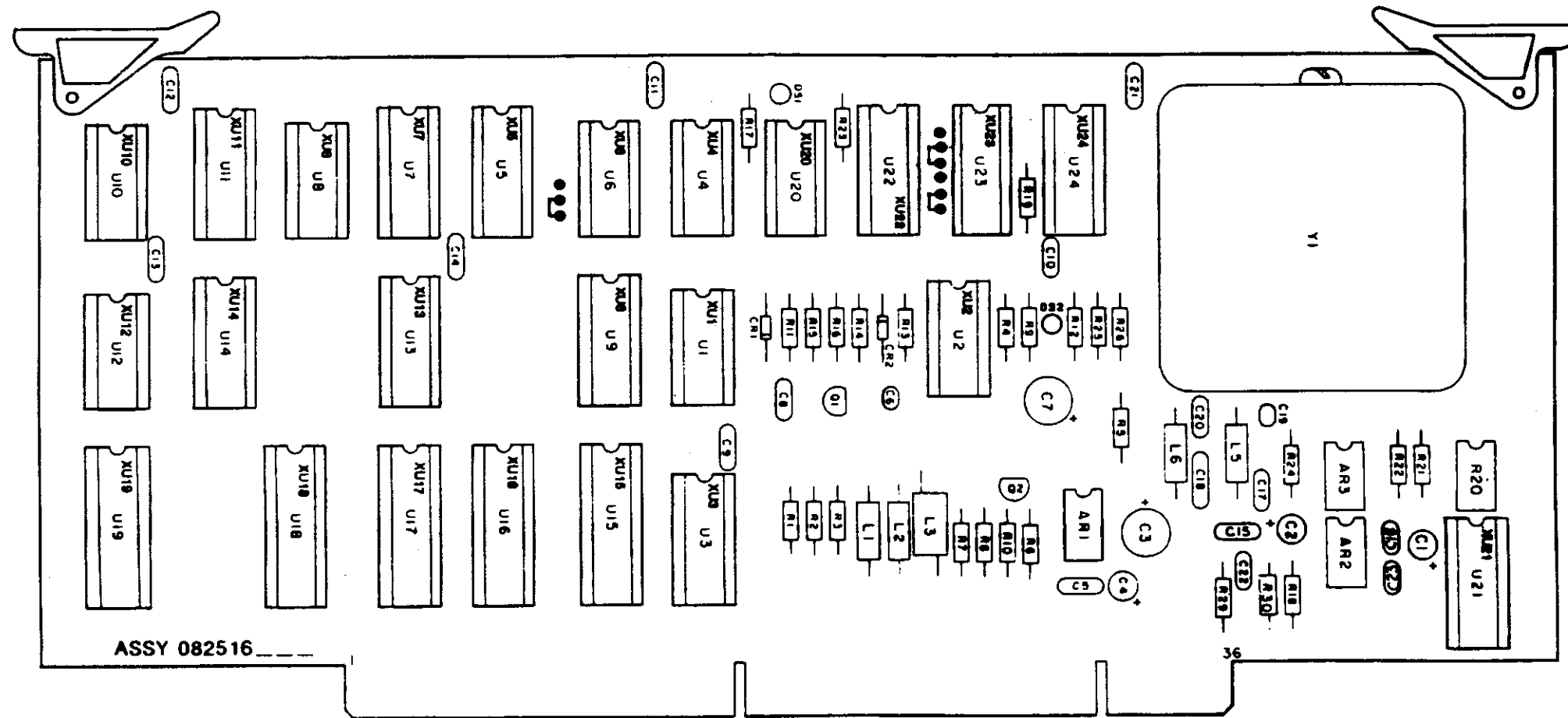


Figure 8-21. CPU Board A9, Schematic Diagram.



082516D1

Figure 8-22. Counter Board A10, Parts Location.

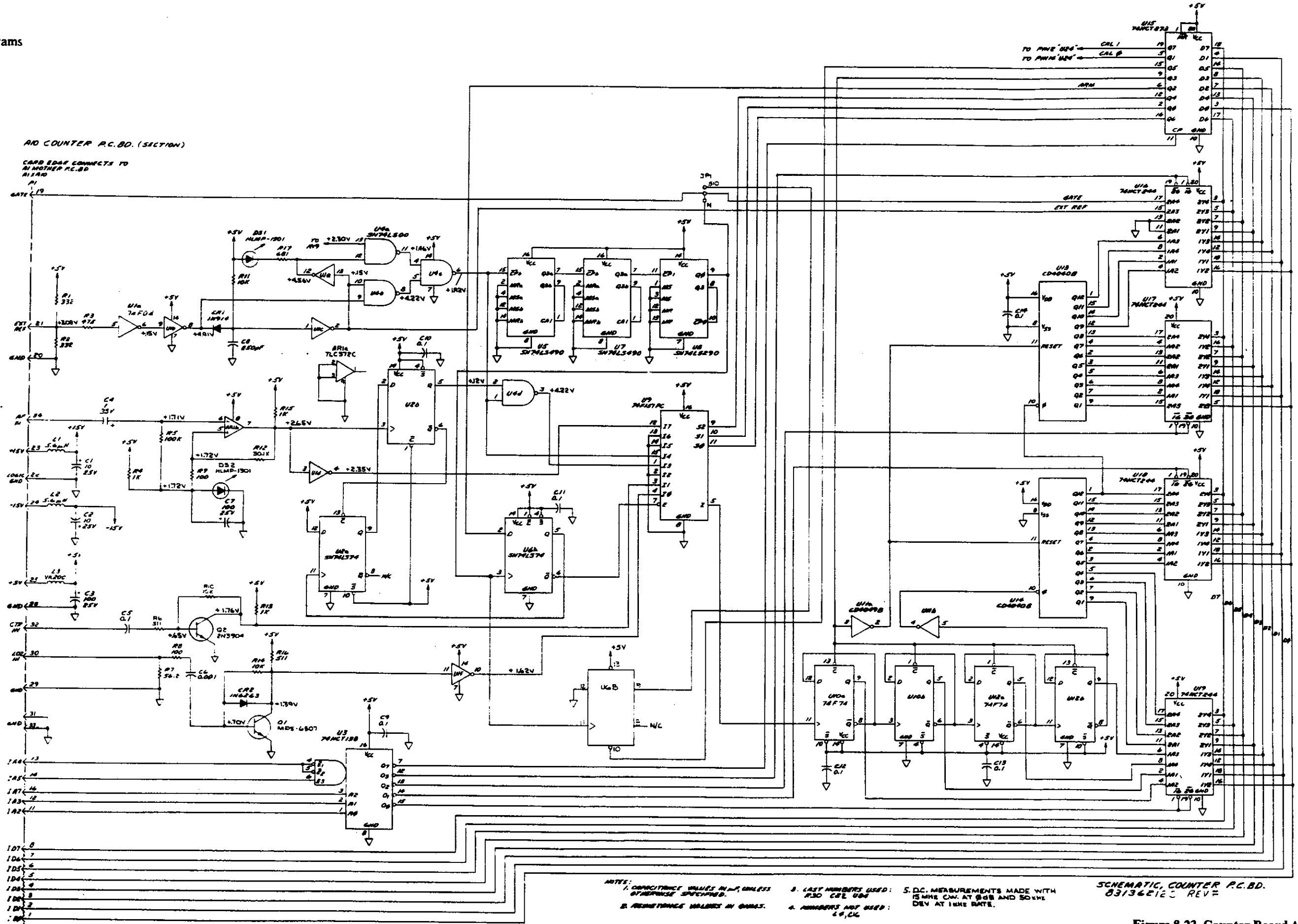
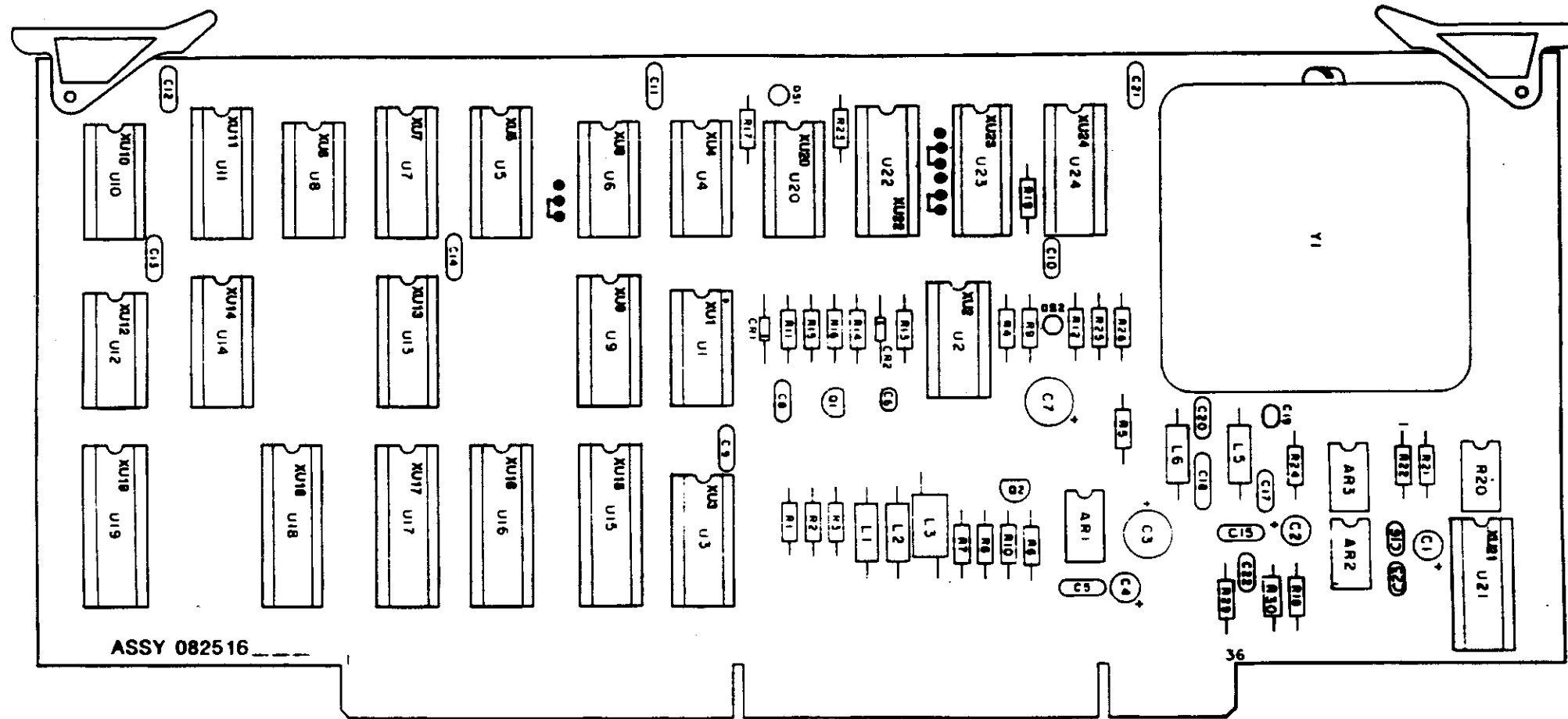
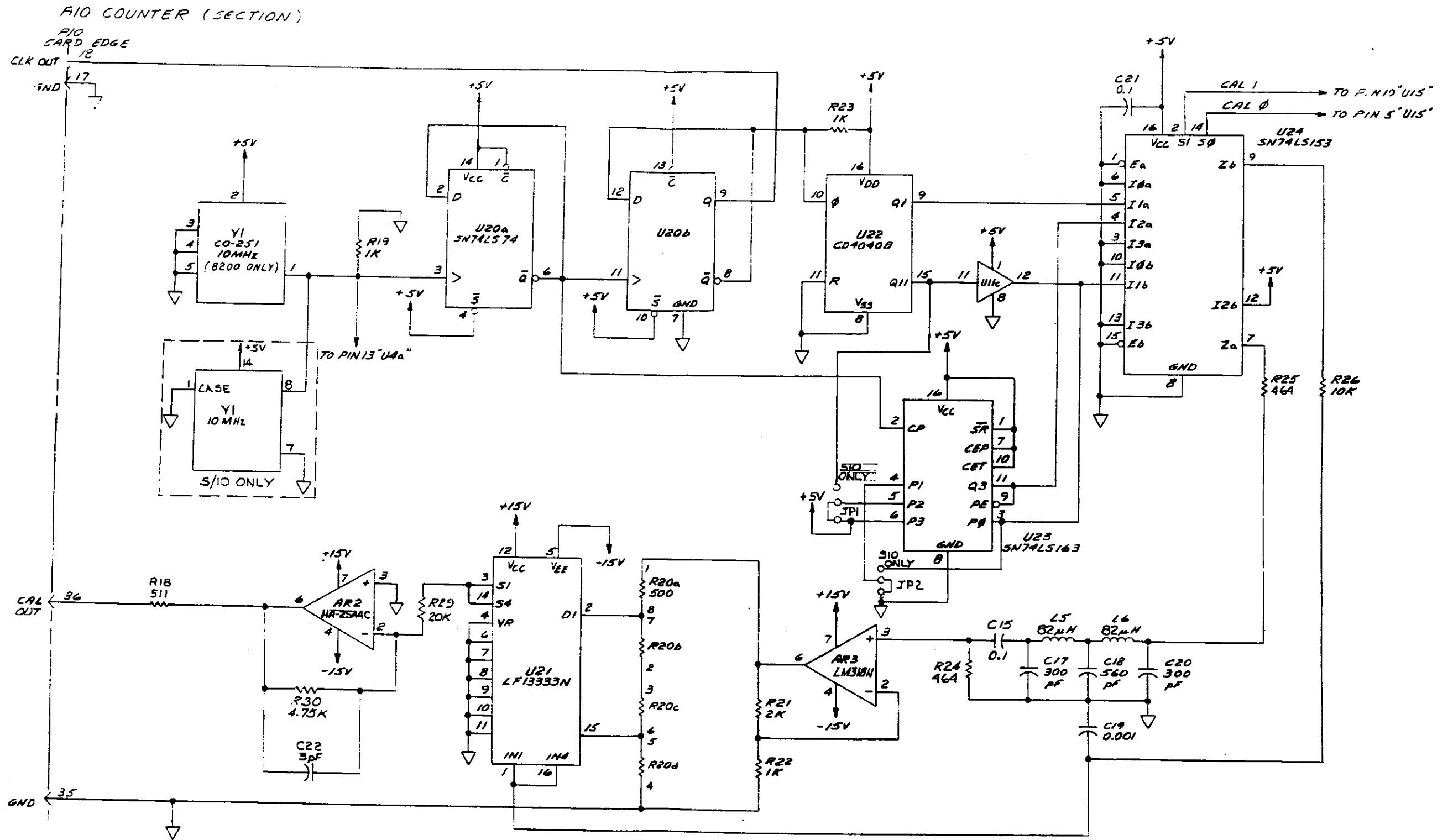


Figure 8-23. Counter Board A10 Schematic, Sheet 1.



082516D,

Figure 8-24. Counter Board A10, Parts Location.



SCHEMATIC, COUNTER P.C. BD.
D83136213C REV D

Figure 8-25. Counter Board A10 Schematic, Sheet 2.

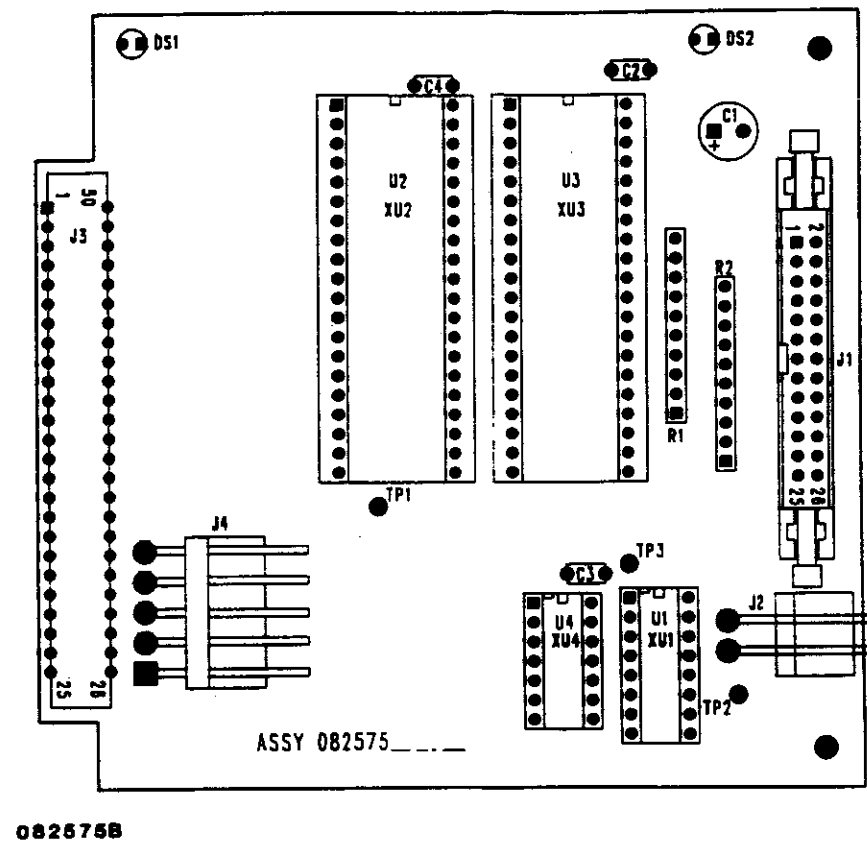
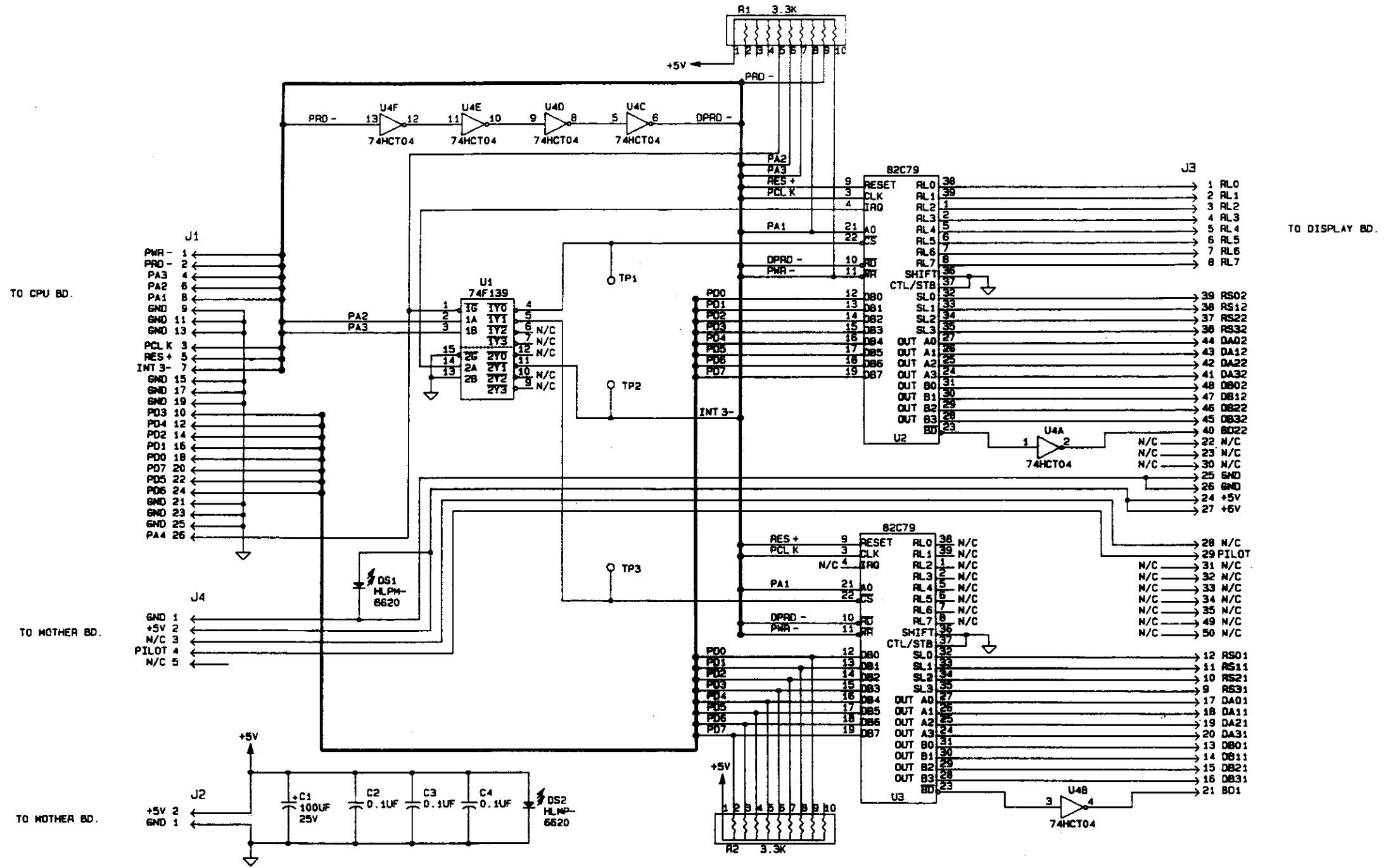


Figure 8-26. I/O Board A11, Parts Location.

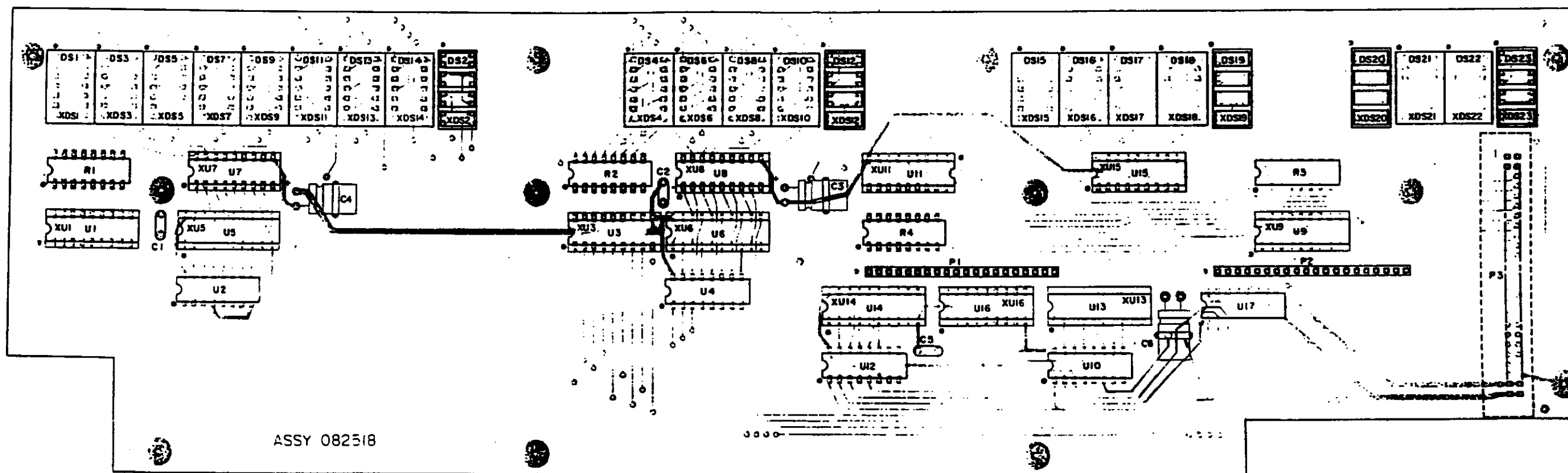


SCHEMATIC, I/O
83136221A REV C₁

REFERENCE DESIGNATOR	IC VOLTAGE CONNECTIONS				
	+5V	-5V	+15V	-15V	GND
U1	16				8
U2, U3	40				20
U4	14				7

- NOTES:
1. ALL RESISTOR VALUES IN OHMS.
 2. LAST NUMBERS USED:
C4 DS2 R2 U4
 3. NUMBERS NOT USED:

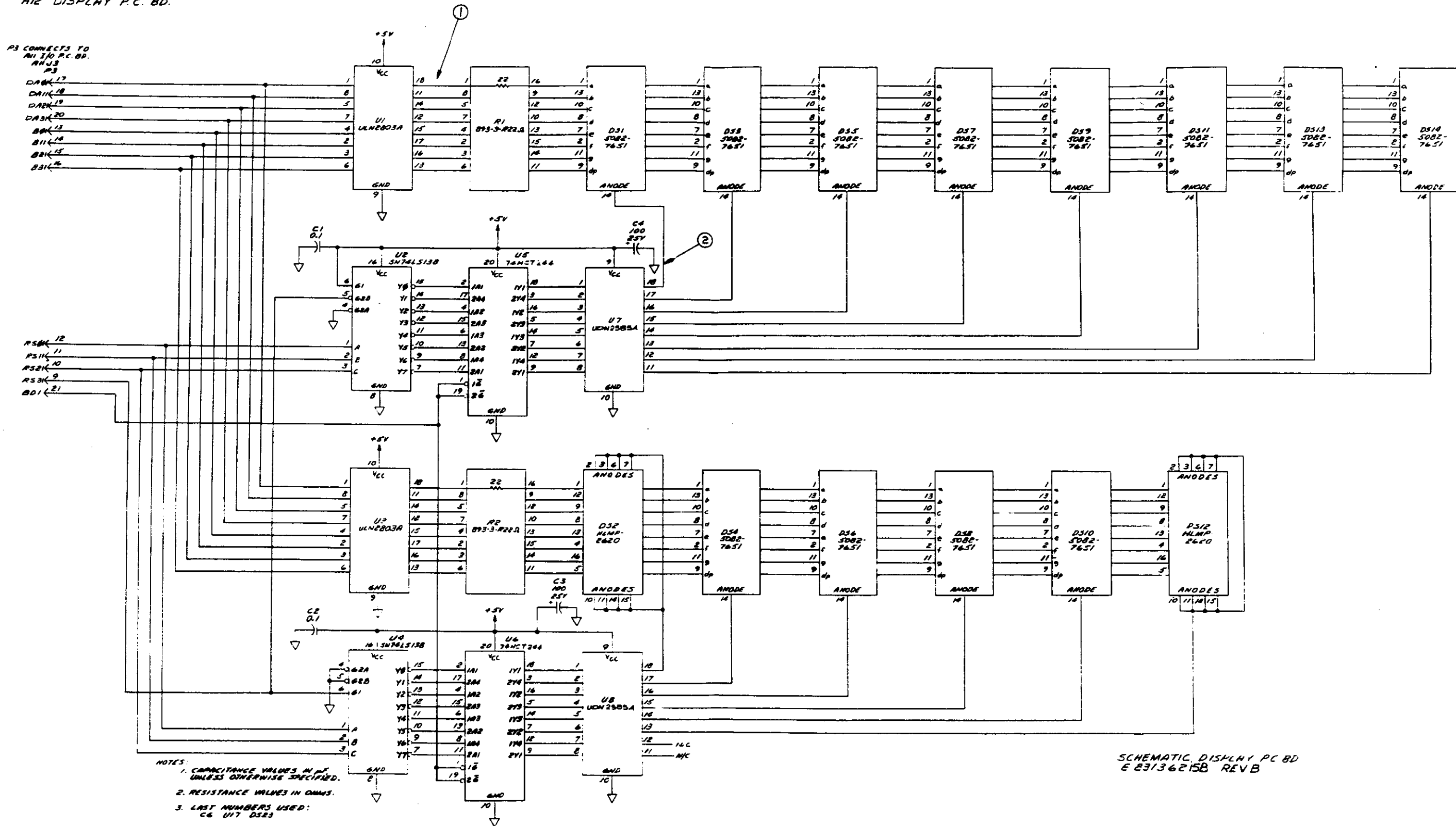
Figure 8-27. I/O Board A11, Schematic Diagram.



082518B

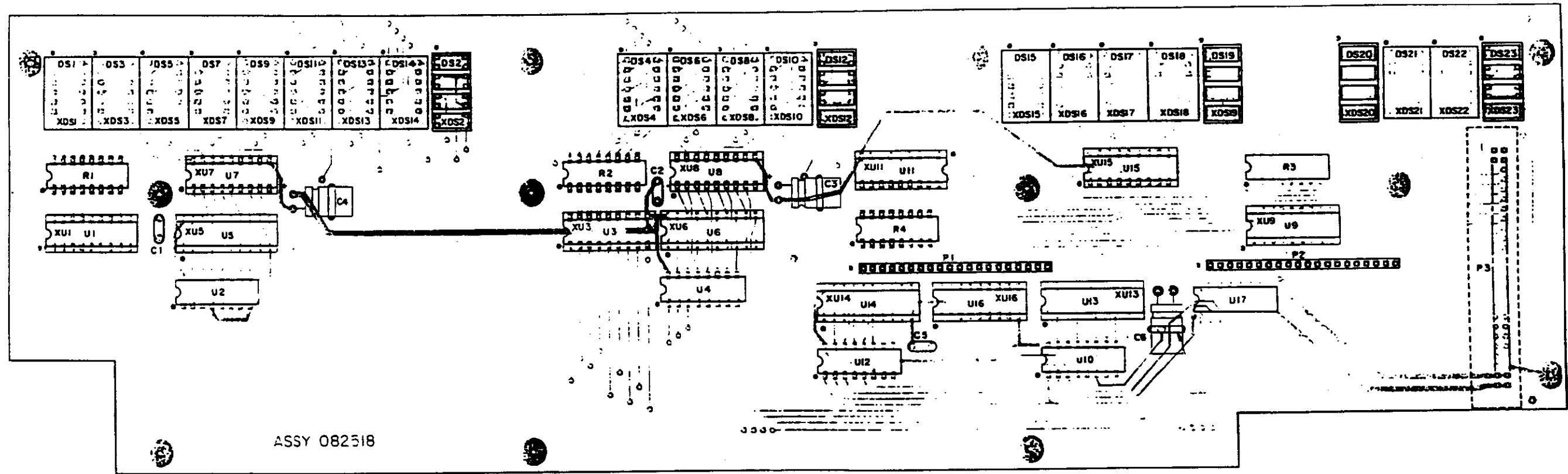
Figure 8-28. Display Board A12, Parts Location.

A12 DISPLAY P.C. BD.



SCHEMATIC, DISPLAY P.C. BD
E 83136215B REV B

Figure 8-29. Display Board A12 Schematic, Sheet 1.



082518B

Figure 8-30. Display Board A12, Parts Location.

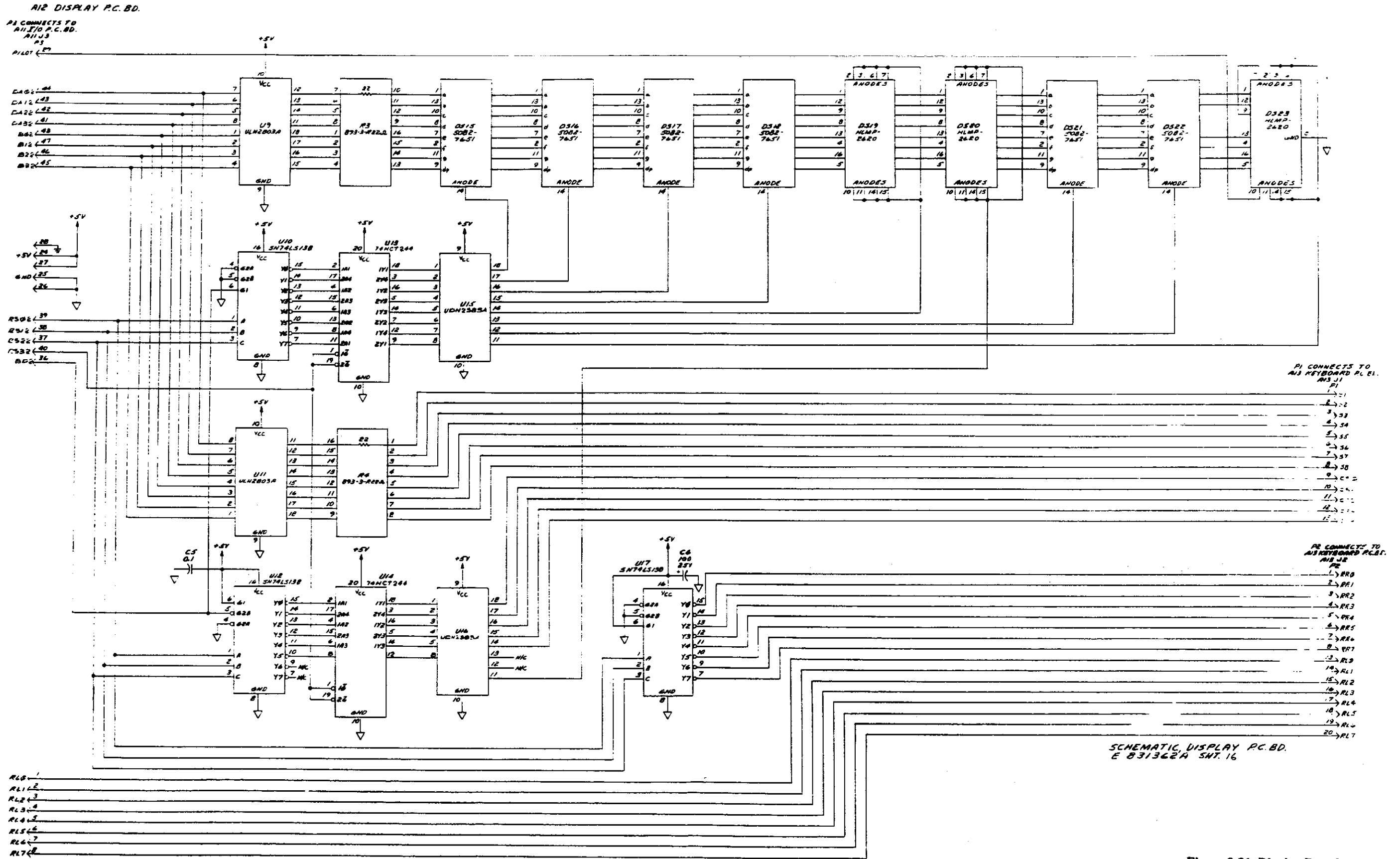
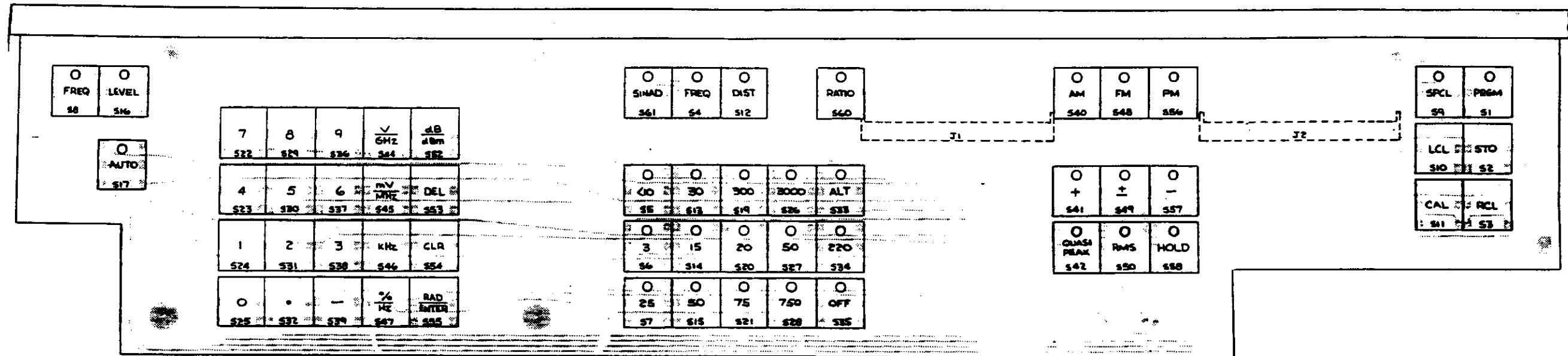


Figure 8-31. Display Board A12 Schematic, Sheet 2.



082517A SHT.3

Figure 8-32. Keyboard A13, Parts Location.

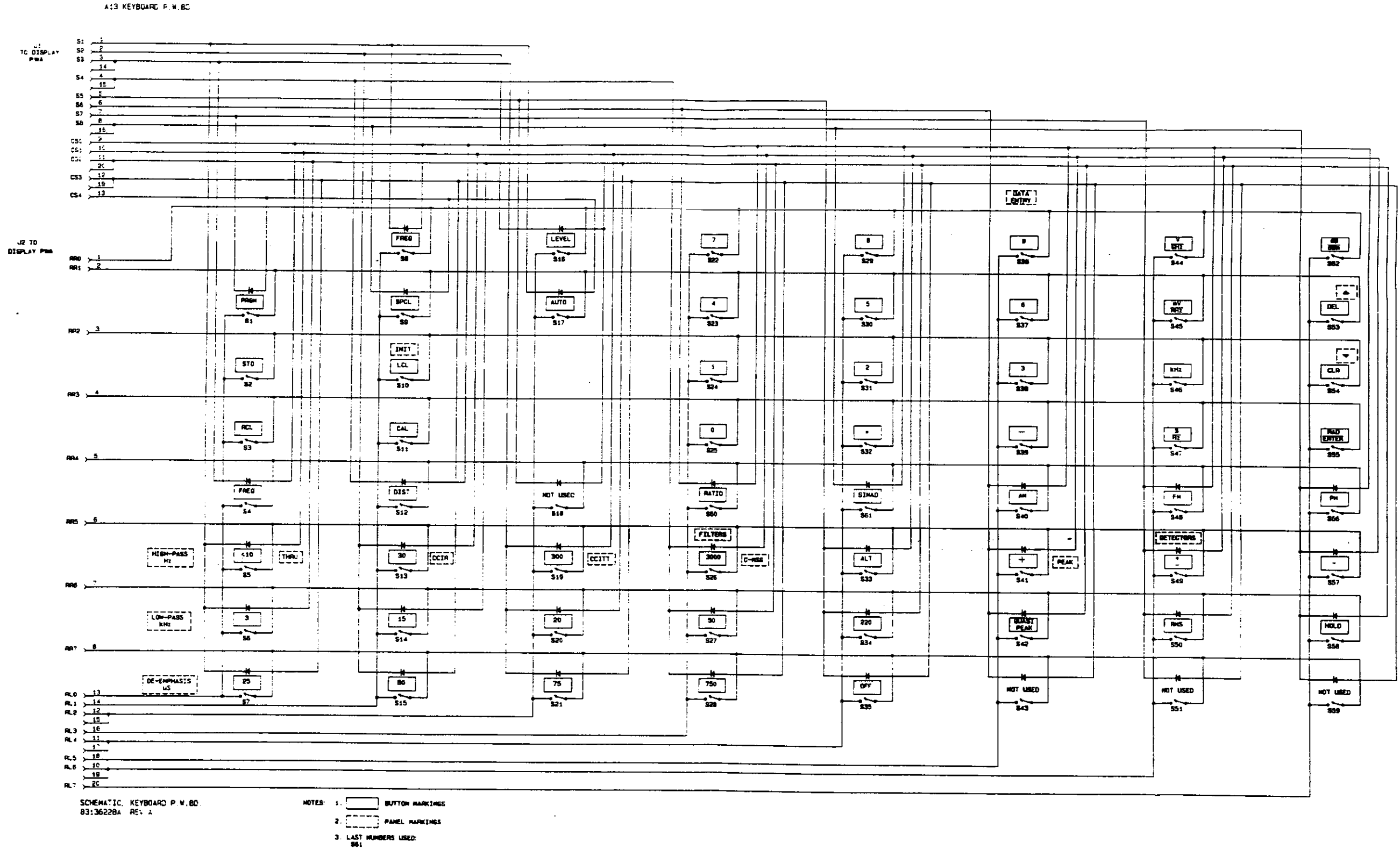
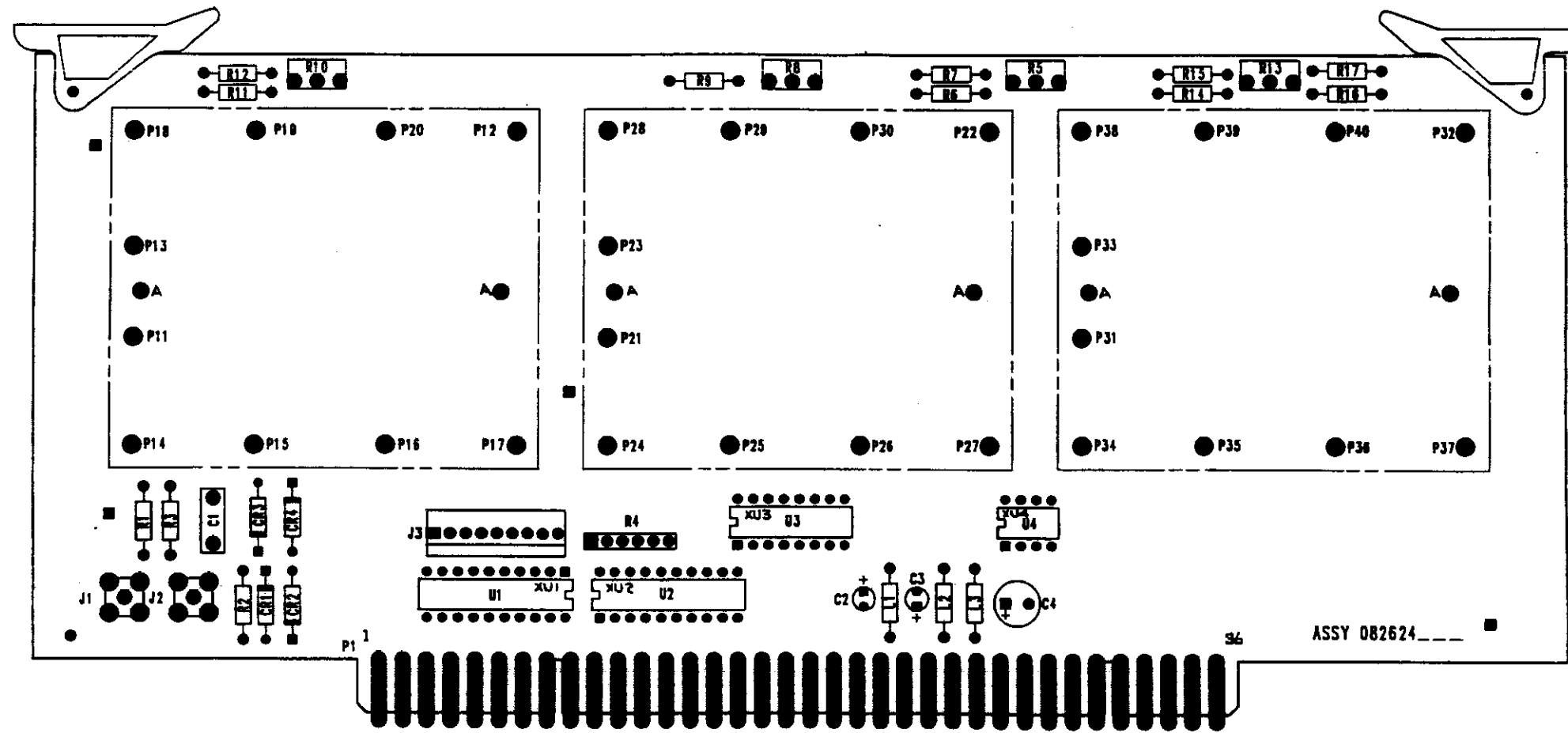


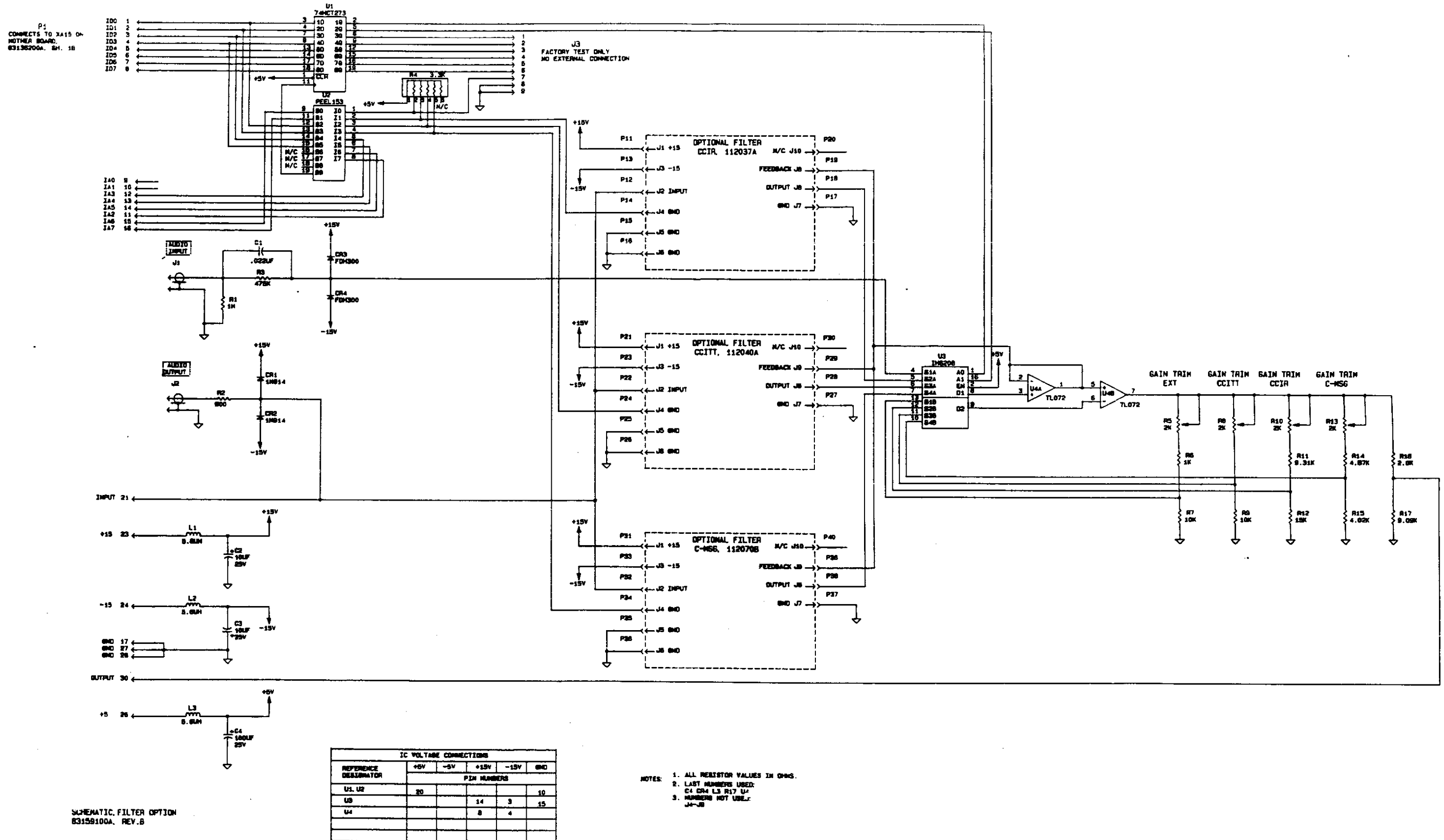
Figure 8-33. Keyboard A13, Schematic Diagram.



082624B

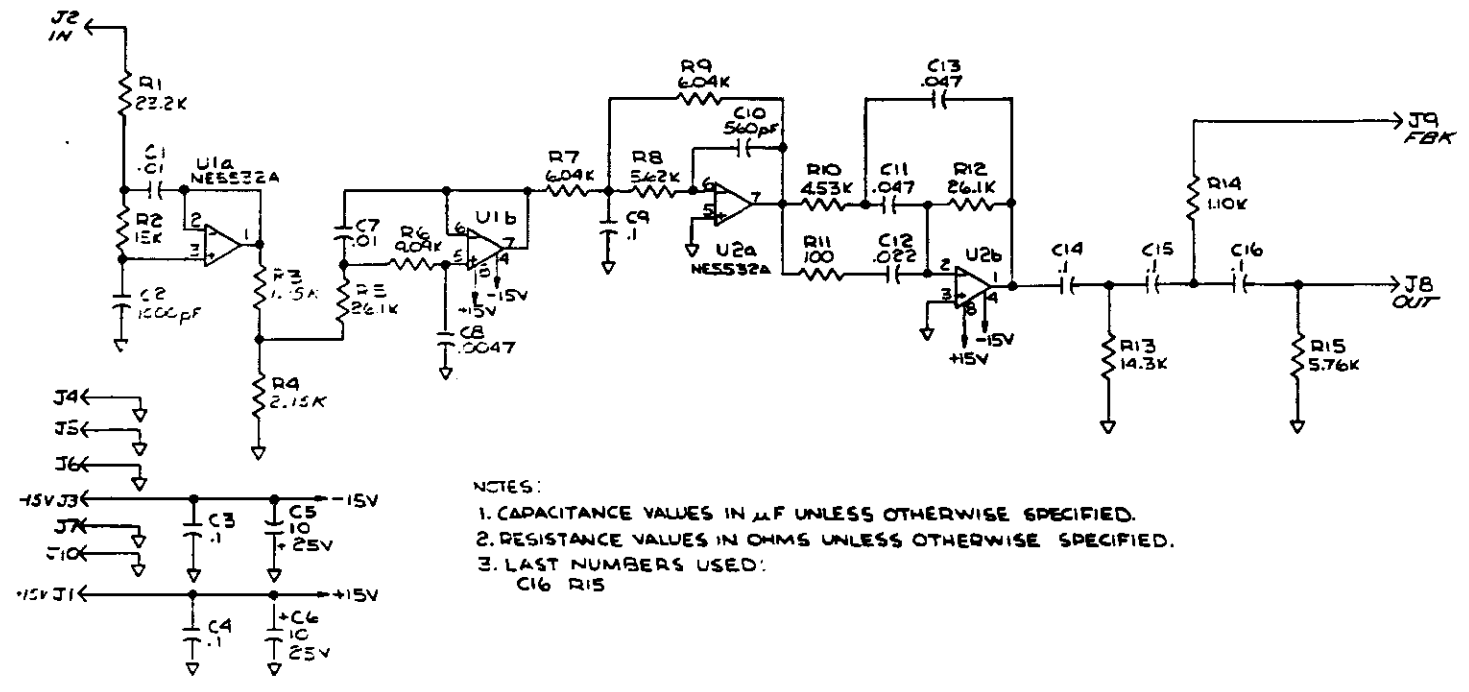
Figure 8-34. Option Board A15, Parts Location.

Schematic Diagrams

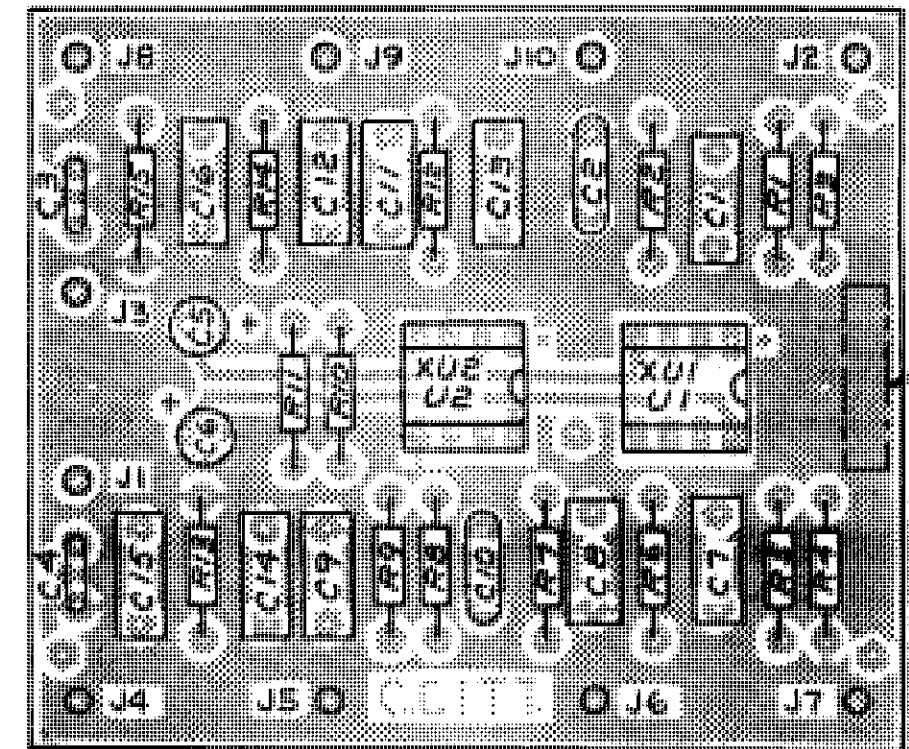


SCHEMATIC, FILTER OPTION
8315B100A, REV. B

Figure 8-35. Option Board A15, Schematic Diagram.

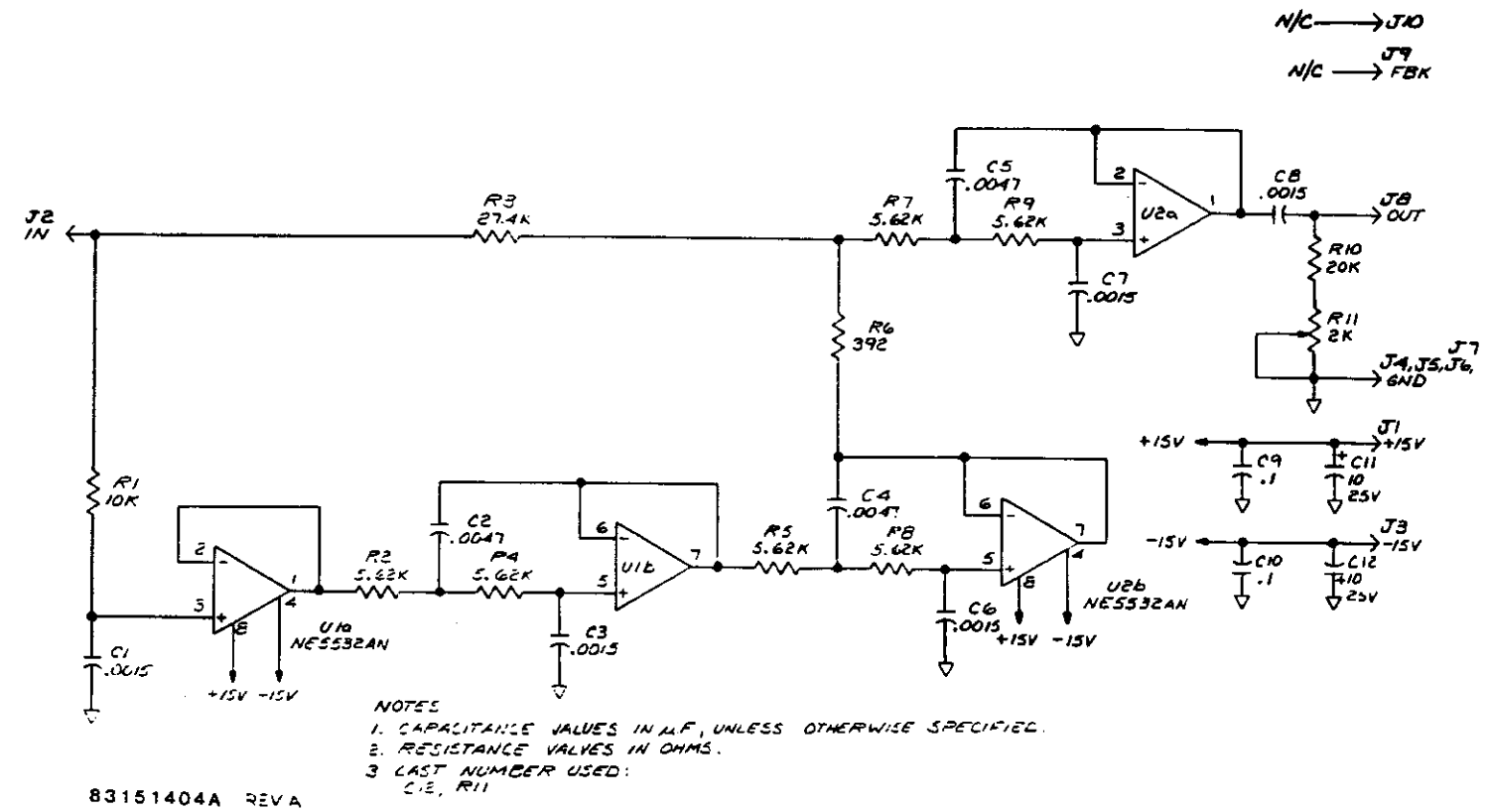
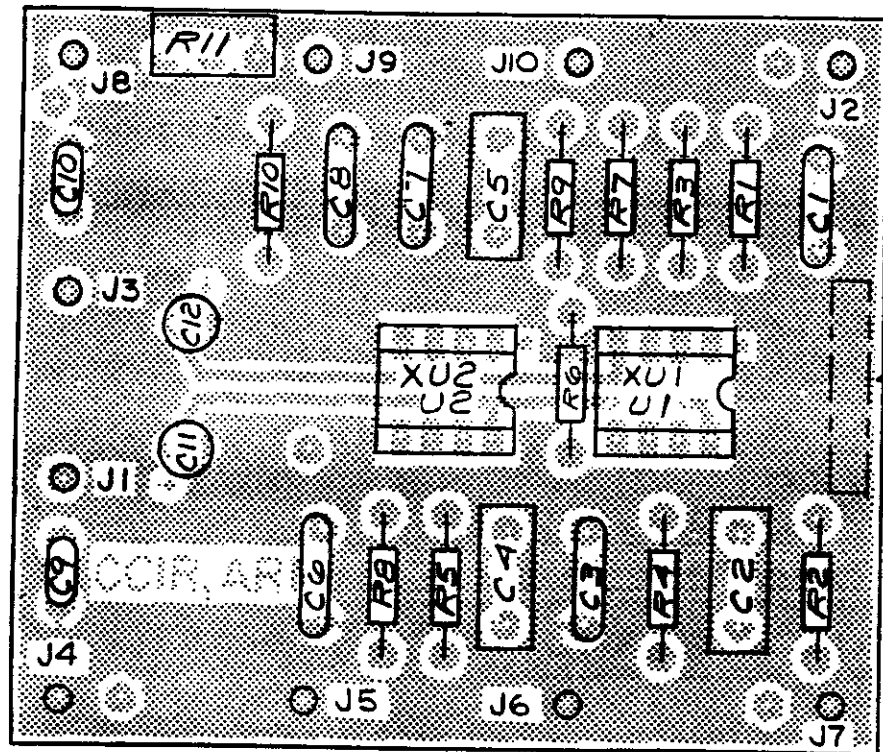


83151403A REV A



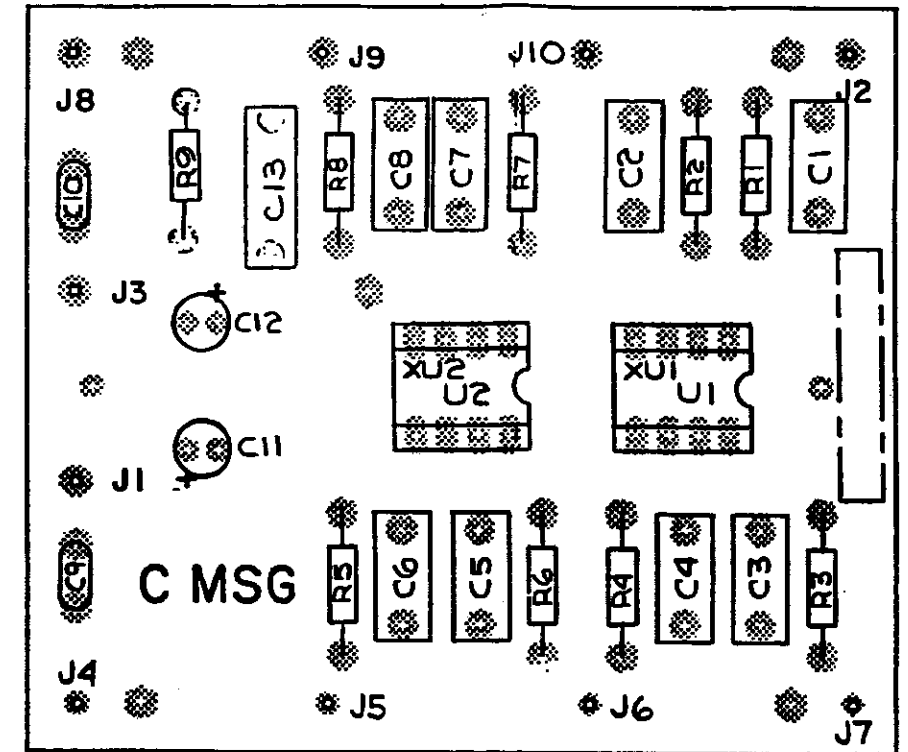
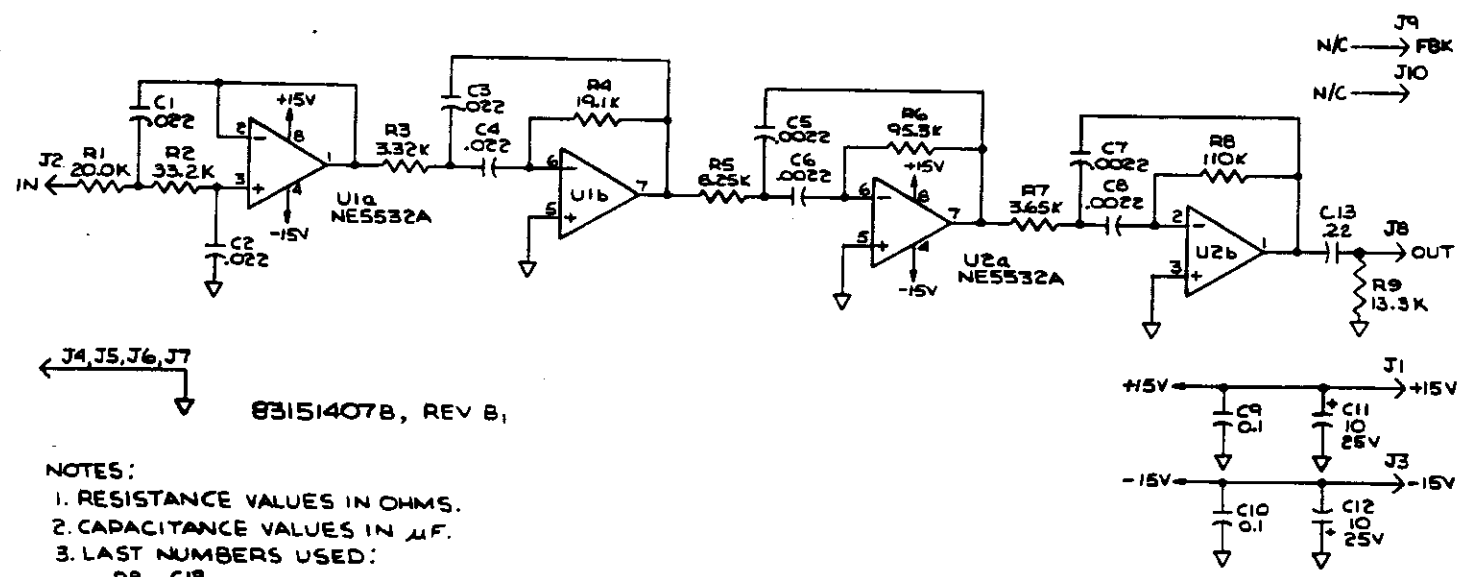
112040A

Figure 8-36. CCITT Filter, Parts Location/Schematic.



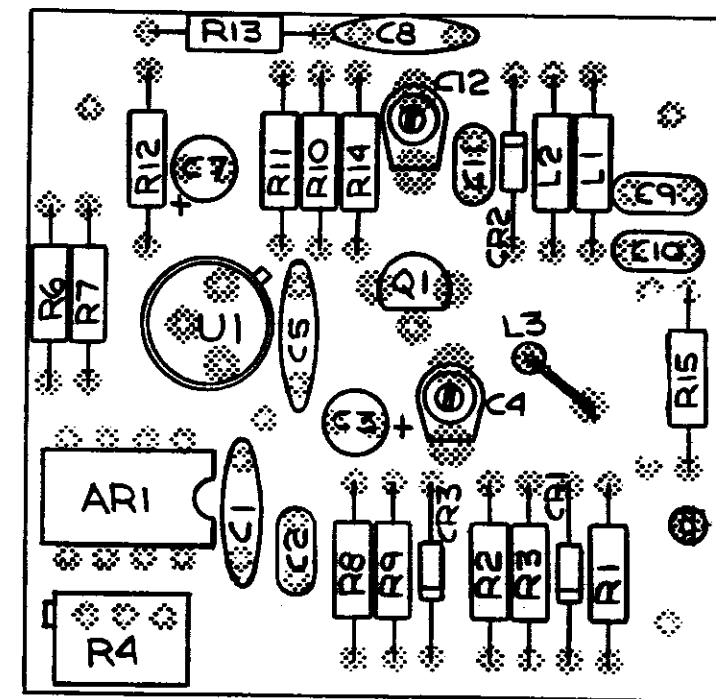
112037A

Figure 8-37. CCIR Filter, Parts Location/Schematic.



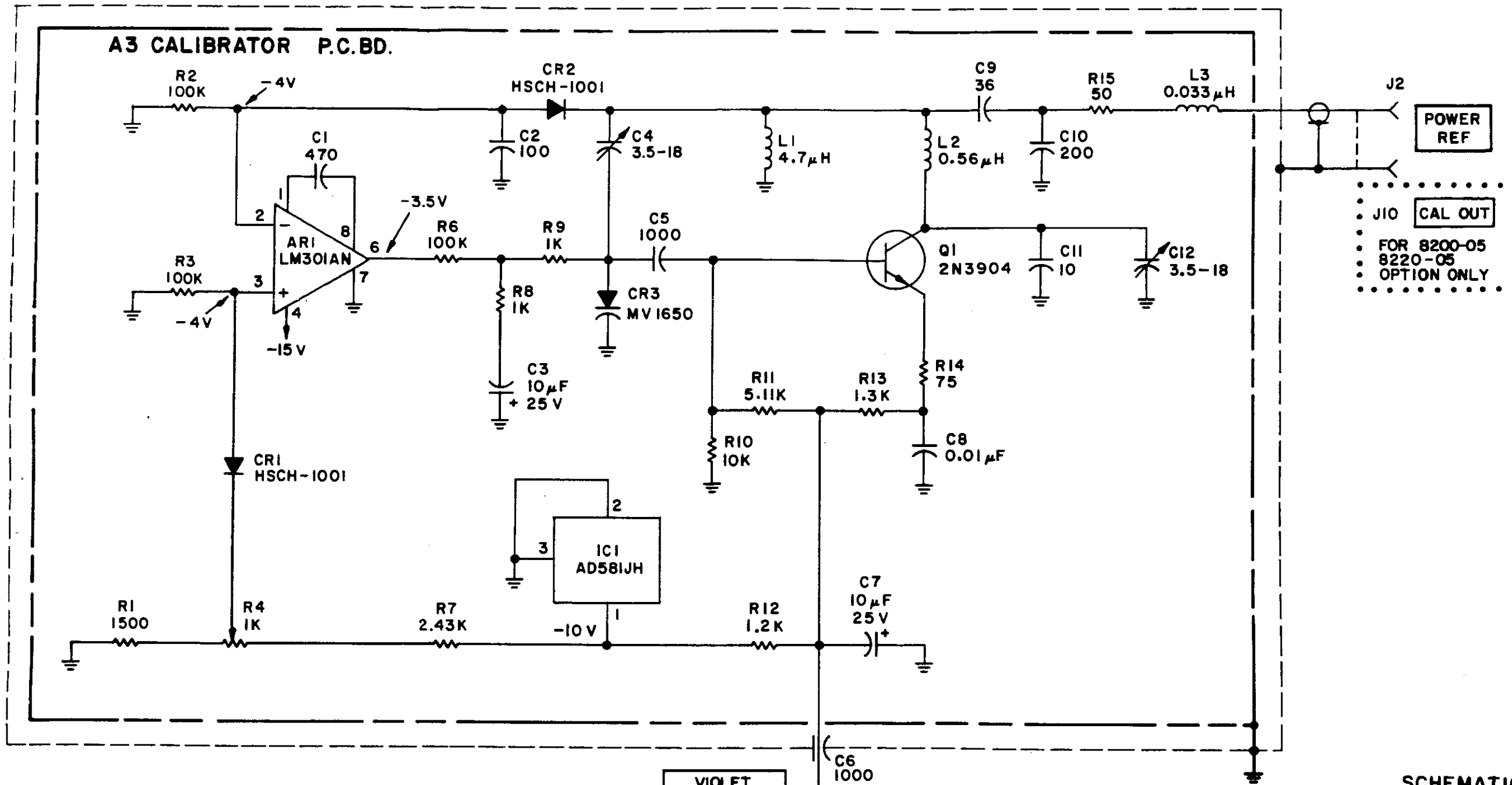
112070B

Figure 8-38. C-Message Filter Parts Location/Schematic



043131A

Figure 8-39. 50 MHz Calibrator A3, Parts Location.



NOTES:

1. CAPACITANCE VALUES IN μF , UNLESS OTHERWISE SPECIFIED.
2. RESISTANCE VALUES IN OHMS.
3. EXTERNAL MARKINGS.
4. LAST NUMBERS USED:
C12 R15
5. NUMBERS NOT USED:
R5 J1(26) (8200-05 & 8220-05 ONLY)

VIOLET
FOR 8200-05
& 8220-05
OPTION ONLY

TO FL2
83136219 C
(FOR 8200-05 ONLY)
83159002A
(FOR 8220-05 ONLY)

J1(26)
CONNECTS TO
A2 P2(26)
ON FRAME SCHEMATIC
831271
SHT. 1 OF 9

SCHEMATIC, CALIBRATOR P.C. BD.
83127103A REV. A5

Figure 8-40. 50 MHz Calibrator A3, Schematic Diagram

WARRANTY

Boonton Electronics Corporation (BEC) warrants its products to the original Purchaser to be free from defects in material and workmanship for a period of one year from date of shipment for instrument, and for one year from date of shipment for probes, power sensors and accessories. BEC further warrants that its instruments will perform within all current specifications under normal use and service for one year from date of shipment. These warranties do not cover active devices that have given normal service, sealed assemblies which have been opened or any item which has been repaired or altered without BEC's authorization.

BEC's warranties are limited to either the repair or replacement, at BEC's option, of any product found to be defective under the terms of these warranties.

There will be no charge for parts and labor during the warranty period. The Purchaser shall prepay shipping charges to BEC or its designated service facility and shall return the product in its original or an equivalent shipping container. BEC or its designated service facility shall pay shipping charges to return the product to the Purchaser. The Purchaser shall pay all shipping charges, duties and taxes if a product is returned to BEC from outside of the United States.

THE FOREGOING WARRANTIES ARE IN LIEU OF ALL OTHER WARRANTIES, EXPRESSED OR IMPLIED, INCLUDING, BUT NOT LIMITED TO, THE IMPLIED WARRANTIES OF MERCHANTABILITY AND FITNESS FOR A PARTICULAR PURPOSE. BEC shall not be liable to any incidental or consequential damages, as defined in Section 2-715 of the Uniform Commercial Code, in connection with the products covered by the foregoing warranties.

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